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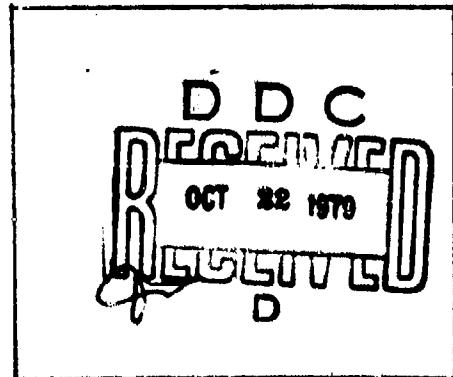
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COMPENDIUM OF SHOCK WAVE DATA

SECTIONS A2-B

H. van Thiel

June 1977



LAWRENCE LIVERMORE LABORATORY
University of California Livermore, California 94550

UCRL-50108 Vol. 2 Rev. 1

COMPENDIUM OF SHOCK WAVE DATA

Section A2 - Inorganic Compounds
Section B - Hydrocarbons

General Editor: M. van Thiel
Assistant Editors: J. Shaner
E. Salinas
Programmer: T. Michels
Secretarial: C. MacNaughton

MS. date: June 1977

Notice

The completeness of this compilation depends upon its users. To assure its continued usefulness, users are urged to send any missing or new shock wave data and corrections to the Editor, M. van Thiel, Lawrence Livermore Laboratory, P.O. Box 808, Livermore, California, U.S.A., 94550.

New and revised pages will be distributed as necessary.



LAWRENCE LIVERMORE LABORATORY
University of California Livermore, California 94550

UCP

1. 2 Rev. 1

COMPEND'

ROCK WAVE DATA

Compounds

477

79 10 19 093

88

SECTION A2

INORGANIC COMPOUNDS

U06/14/77

2-1---0
WATER SUMMARY

H2-O

 $T = 20 \text{ DEG. C}$
 $V_0 = 1.0018 \text{ CC/O}$ $C_0 = 1.483 \text{ KM/SEC}$ THE TABLE LISTS HUGONIOT POINTS CALCULATED FROM THE FITS GIVEN BELOW.
UNITS ARE: G/CC., KM/SEC., KBARS AND KBAR.CC/O FOR THE ENERGY DIFFERENCE.

TABLE

FIT	RHO0	US	UP	P	V/V0	E-EO
1	0.9982	3.316	.9	29.8	0.729	4.05
-	-	4.106	1.4	57.4	0.659	9.80
-	-	4.997	1.9	92.9	0.612	18.0
-	-	5.887	2.4	136.	0.578	26.0
2	-	6.591	3.0	197	0.545	45.0
-	-	7.751	4.0	309	0.484	80.
-	-	8.911	5.0	445	0.439	125.
-	-	11.231	7.0	785	0.377	245.
-	-	13.551	9.0	1217	0.336	405.

 $US = 1.893 + 1.581 \cdot UP, \quad \text{SIG.US} = 0.03 \text{ KM/SEC}$ FIT 1
FOR UP BETWEEN 0.9 AND 2.4 KM/SEC $US = 3.111 + 1.160 \cdot UP, \quad \text{SIG.US} = 0.16 \text{ KM/SEC}$ FIT 2
FOR UP BETWEEN 3.3 AND 8.7 KM/SEC.

COMMENTS:

- 1) SOURCE: COMPILER
DATA OF 2-1---1 AND 3 WERE USED FOR THIS SUMMARY.
- 2) THE TWO-Straight-LINE CHARACTER OF THE US UP DATA MAY BE ASSOCIATED WITH A PHASE TRANSFORMATION:
L. V. AL'TSHULER, A. A. BAKANOVA AND R. F. TRUNIN
DOKLADY AKAD. NAUK SSSR. VOL. 121, P. 67, (1958) RUSS.
SOVIET PHYS. DOKLADY VOL. 3, P. 761, (1958) ENGL.
- 3) DATA OF 2-1---4 AGREE WITH THIS FIT BUT ARE LESS PRECISE.
- 4) C0 IS HIGHLY TEMPERATURE DEPENDENT: $C_0(10 \text{ DEG. C.}) = 1.448 \text{ KM/SEC}$
 $C_0(30 \text{ DEG. C.}) = 1.309 \text{ KM/SEC}$
L. BEPMANN, DER ULTRASCHALL (S. HIRZEL VERLAG, STUTTGART 1954)
6TH ED. P. 410

2-1---0
WATER SUMMARY

H2-O

T = 20 DEG. C
V0 = 1.0018 CC/G

C0 = 1.483 KM/SEC

THE TABLE LISTS HUGONIOT POINTS CALCULATED FROM THE FITS GIVEN BELOW.
UNITS ARE: G/CC, KM/SEC, KBARS AND KBAR.CC/G FOR THE ENERGY DIFFERENCE.

TABLE

FIT	RHO0	US	UP	P	V/V0	E-E0
1	0.9982	3.316	.9	29.8	0.728	4.05
-	-	4.106	1.4	57.4	0.659	9.80
-	-	4.897	1.9	92.8	0.612	18.0
-	-	5.687	2.4	136.	0.578	28.8
2	-	6.591	3.0	197	0.545	45.0
-	-	7.751	4.0	309	0.484	80.
-	-	8.911	5.0	445	0.439	125.
-	-	11.231	7.0	785	0.377	245.
-	-	13.551	9.0	1217	0.336	405.

US = 1.893 + 1.581*UP, SIG.US = 0.03 KM/SEC FIT 1

FOR UP BETWEEN 0.9 AND 2.4 KM/SEC

US = 3.111 + 1.160*UP, SIG.US = 0.16 KM/SEC FIT 2

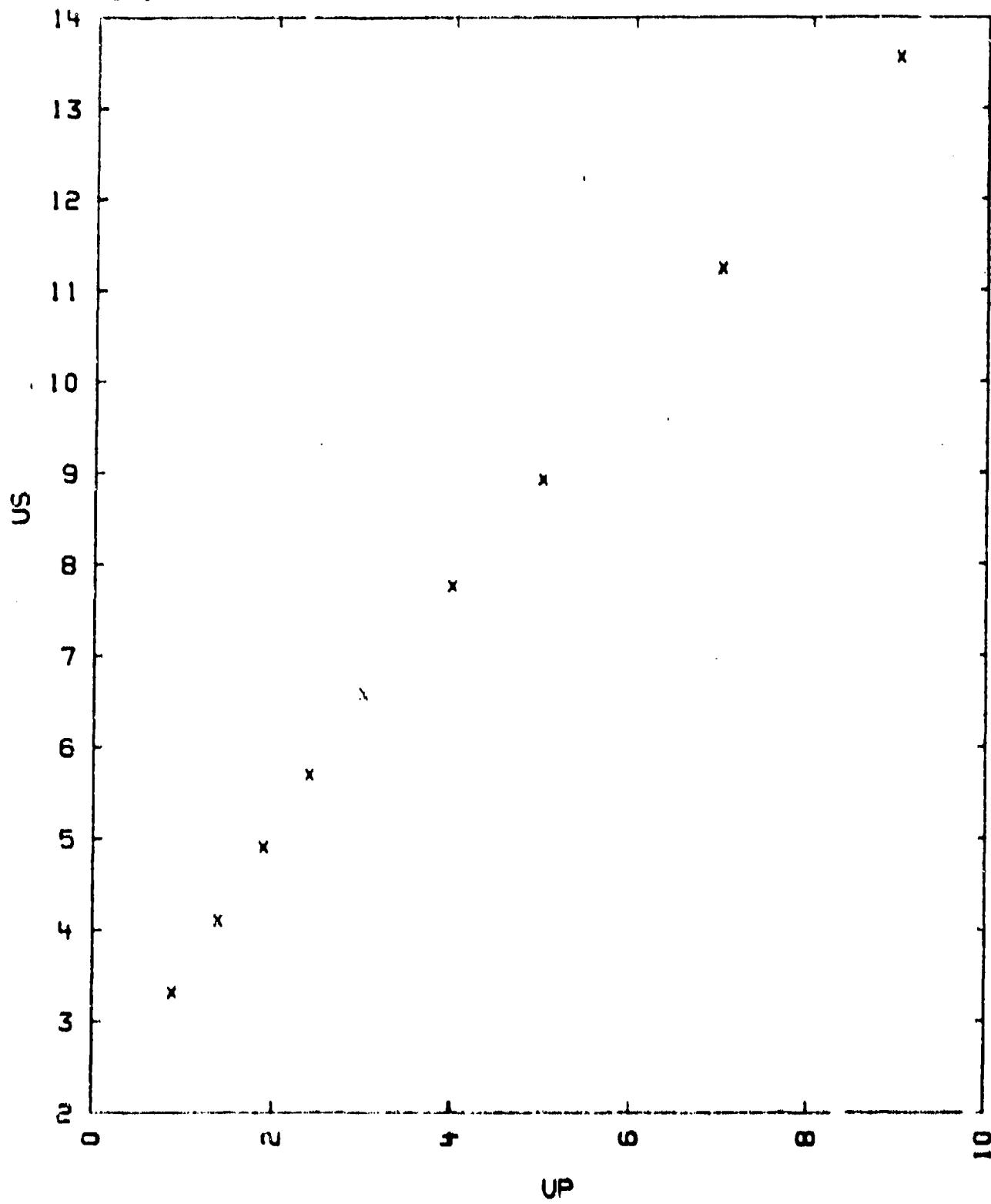
FOR UP BETWEEN 3.3 AND 8.7 KM/SEC.

COMMENTS:

- 1) SOURCE: COMPILER
DATA OF 2-1---1 AND 3 WERE USED FOR THIS SUMMARY.
- 2) THE TWO-Straight-line CHARACTER OF THE US UP DATA MAY BE ASSOCIATED WITH A PHASE TRANSFORMATION:
L. V. AL'TSIKLER, A. A. BAKANOVA AND R. F. TRUNIN
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SOVIET PHYS. DOKLADY VOL. 3, P. 761, (1958) ENGL.
- 3) DATA OF 2-1---4 AGREE WITH THIS FIT BUT ARE LESS PRECISE.
- 4) C0 IS HIGHLY TEMPERATURE DEPENDENT: C0(10 DEG. C.) = 1.448 KM/SEC
C0(30 DEG. C.) = 1.309 KM/SEC
L. BERGMANN, DER ULTRASCHALL. (S. HIRZEL VERLAG, STUTTGART 1954)
6TH ED. P. 410.

TABLE 1

WATER SUMMARY
2-1---0



2-1---1
WATER (HYDROGEN OXIDE)

H₂O GREATER THAN 99.9 PER CENT

$$V_0 = 1.002 \text{ CC}/\text{O}$$

$$C_0 = 1.5 \text{ KM}/\text{SEC}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN MM/MICRO-SEC., AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UP	P	V/V0
1.00	7.06	3.32	235	.530
	7.05	3.39	240	.491
	6.89	3.44	240	.498
	8.26	4.53	378	.447
	12.05	8.03	1040	.370
	12.69	8.43	1070	.336
	13.09	8.71	1140	.335

US = 3.09 + 1.164UP - .1138(UP - 3.76) MM/MICROSEC FOR UP LESS THAN 3.76
 US = 3.09 + 1.164UP MM/MICROSEC FOR UP GREATER THAN 3.76

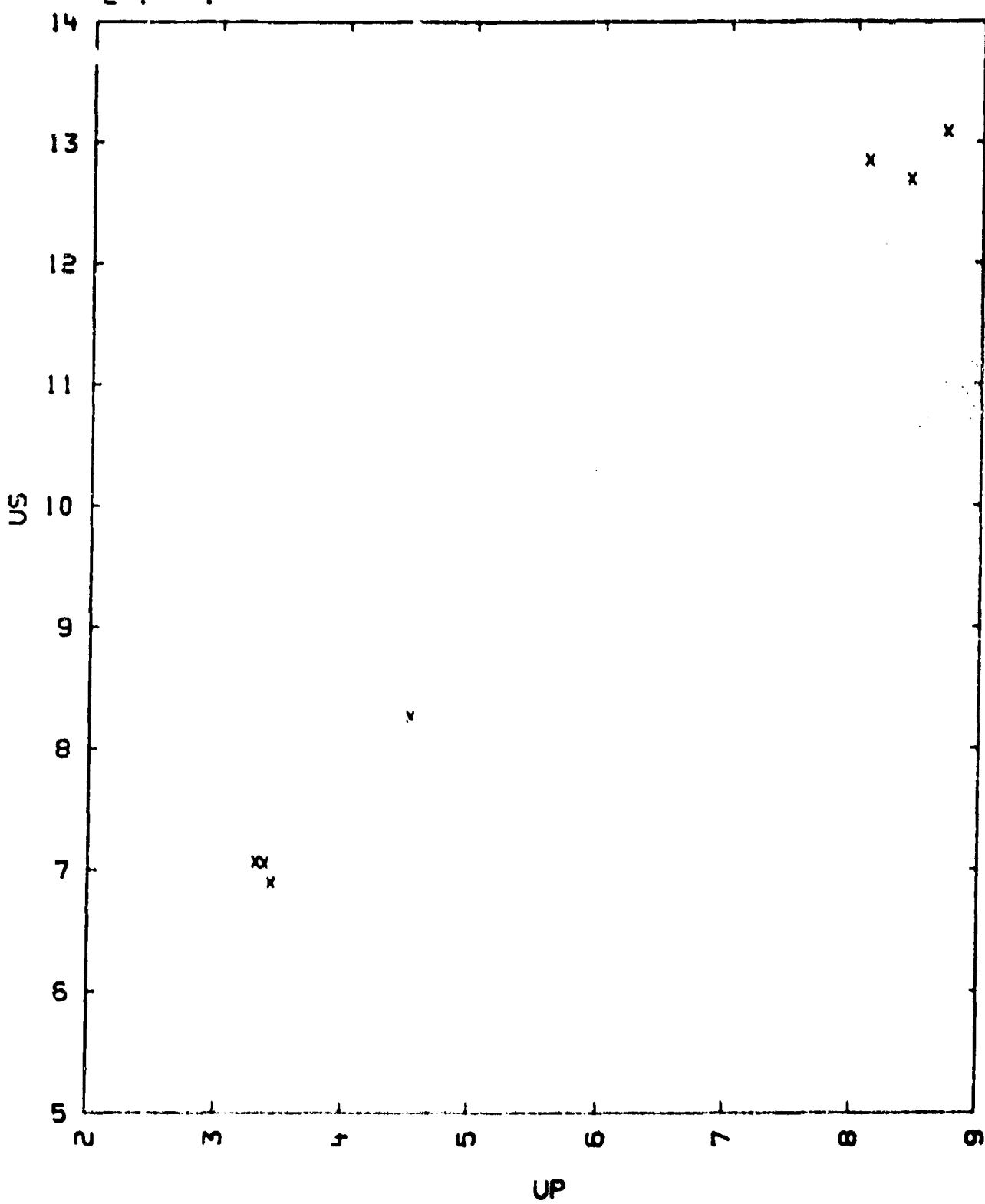
COMMENTS:

- 1) SOURCE: SKIDMORE, I.C. AND MORRIS, E.
THERMODYNAMICS OF NUCLEAR MATERIALS, P. 172 FF. (1962)
INTERN. AT. ENERGY AGENCY, VIENNA
ATOMIC WEAPONS RESEARCH ESTABLISHMENT, ALDERMaston, ENGLAND
- 2) EXPERIMENTAL TECHNIQUE A
DATA REDUCTION TECHNIQUE B
THE SHOCK WAS PRODUCED BY AN EXPLOSIVELY ACCELERATED EN3 STEEL PLATE.
THE SHOCK WAS TRANSMITTED THROUGH A STEEL PLATE INTO THE SAMPLE.
- 3) THE VELOCITY OF THE FLYING PLATE AND THE SHOCK AND SURFACE VELOCITY OF THE TARGET PLATE WERE MEASURED AS WELL AS THE SAMPLE SURFACE AND SHOCK VELOCITIES.
- 4) DATA SCATTER WAS ABOUT 0.03 MICROSEC.
- 5) CORRECTIONS WERE MADE FOR FLYING PLATE CURVATURE OF UP TO 1 MICROSEC.
- 6) THE HIGHER PRESSURES WERE OBTAINED BY A SPHERICALLY CONVERGING SYSTEM.
- 7) ALL PELLETS WERE SURROUNDED BY LEAD TO REDUCE LATERAL RAREFACTION.

TABLE I

WATER (HYDROGEN OXIDE)

2-1---1



2-1---2
WATER (HYDROGEN OXIDE)

H₂O

VOL = 1.00 CC/G

THE TABLE BELOW GIVES THE VELOCITY OF RELAXATION WAVE, C, AT THE GIVEN PRESSURE. THE HUGONIOT STATE THE RELAXATION WAVE TRAVELS THROUGH IS GIVEN BY US, U, P AND V/V₀. VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBARS AND DENSITY IN G/CC.

TABLE

SOUND VELOCITY
PERPENDICULAR TO SHOCK DIRECTION

RHO0	US	UP	P	V/V ₀	C
1.00	4.42	1.52	67.2	0.656	5.60
US =					

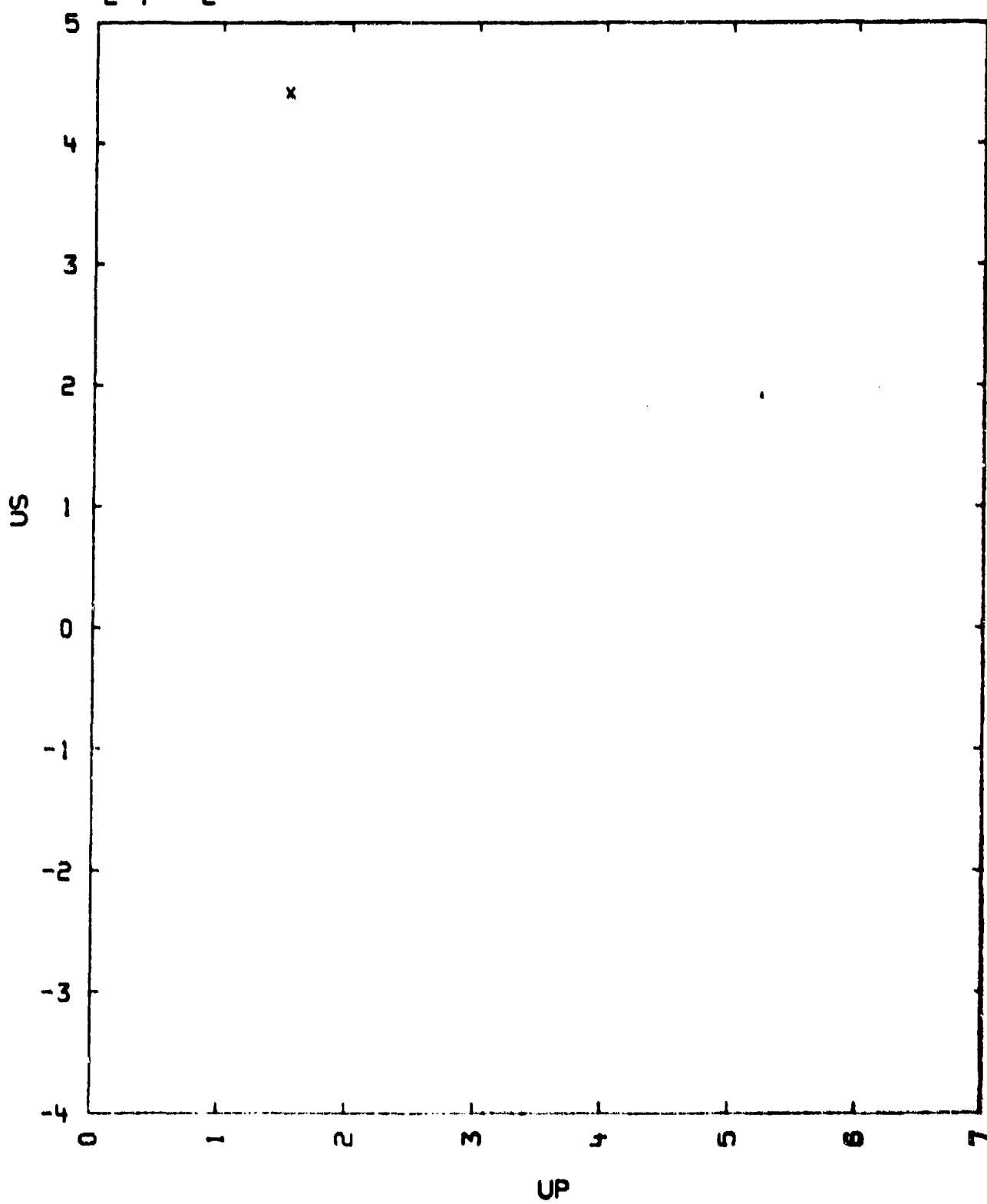
COMMENTS:

- 1) SOURCE: AL'TSHULER, L. V., KORMER, S. B., BRAZHNIK, M. I., VLADIMIROV, L. A. AND FUNTIKOV, A. I.
SOVIET PHYS.-JETP, VOL. 11, P. 766 (1960)
- 2) EXPERIMENTAL TECHNIQUE B
- 3) THE SOUND VELOCITIES WERE DETERMINED FROM THE CONTOUR OF THE FREE SURFACE AFTER IT HAD MOVED SOME DISTANCE.
- 4) THE MEASURED SOUND VELOCITY IS SLIGHTLY SMALLER THAN THE VELOCITY $(\partial P / \partial \rho_0)^{1/2} / P = 5.85$ KM/SEC., WHERE THE DERIVATIVE IS TAKEN ALONG THE HUGONIOT.
- 5) VOL WAS OBTAINED FROM THE HANDBOOK OF CHEMISTRY AND PHYSICS (THE CHEMICAL RUBBER PUBLISHING CO., CLEVELAND, OHIO, 1962-1963) 44TH ED.

TABLE I

WATER (HYDROGEN OXIDE)

2-1---2



2-1---3
WATER (HYDROGEN OXIDE)

H₂O

T₀ = 20 DEG. CENTIGRADE
V₀ = 1.0018 CC/0

C₀ = 1.4829 KM/SEC.

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBARS AND DENSITY IN G/CC.

TABLE

P(KB)	U _S	U _P	P	V/V ₀
0.9982	3.354	0.952	31.8	0.716
-	4.093	1.392	56.8	0.660
-	4.126	1.411	58.2	0.658
-	4.536	1.655	74.9	0.635
-	4.813	1.828	87.8	0.620
-	4.777	1.806	86.1	0.622
-	4.757	1.788	85.4	0.622
-	5.626	2.385	133.9	0.576
-	5.604	2.370	132.5	0.577
-	5.601	2.335	130.5	0.583
-	8.07	4.13	335.0	0.488
-	8.07	4.24	342.0	0.475
-	8.45	4.60	386.0	0.456
-	8.48	4.72	400.0	0.444
-	8.59	4.72	405.0	0.450
-	8.74	4.81	419.0	0.450

U_S = 1.57 + 1.946•U_P - 0.097•U_P•² KM/SEC. SIG U_S = 0.05 KM/SEC
BUT A LINEAR FIT IS ADEQUATE FOR U_P BELOW 4. KM/SEC.
U_S = 1.89 + 1.58•U_P KM/SEC. SIG U_S = 0.03 KM/SEC.

COMMENTS:

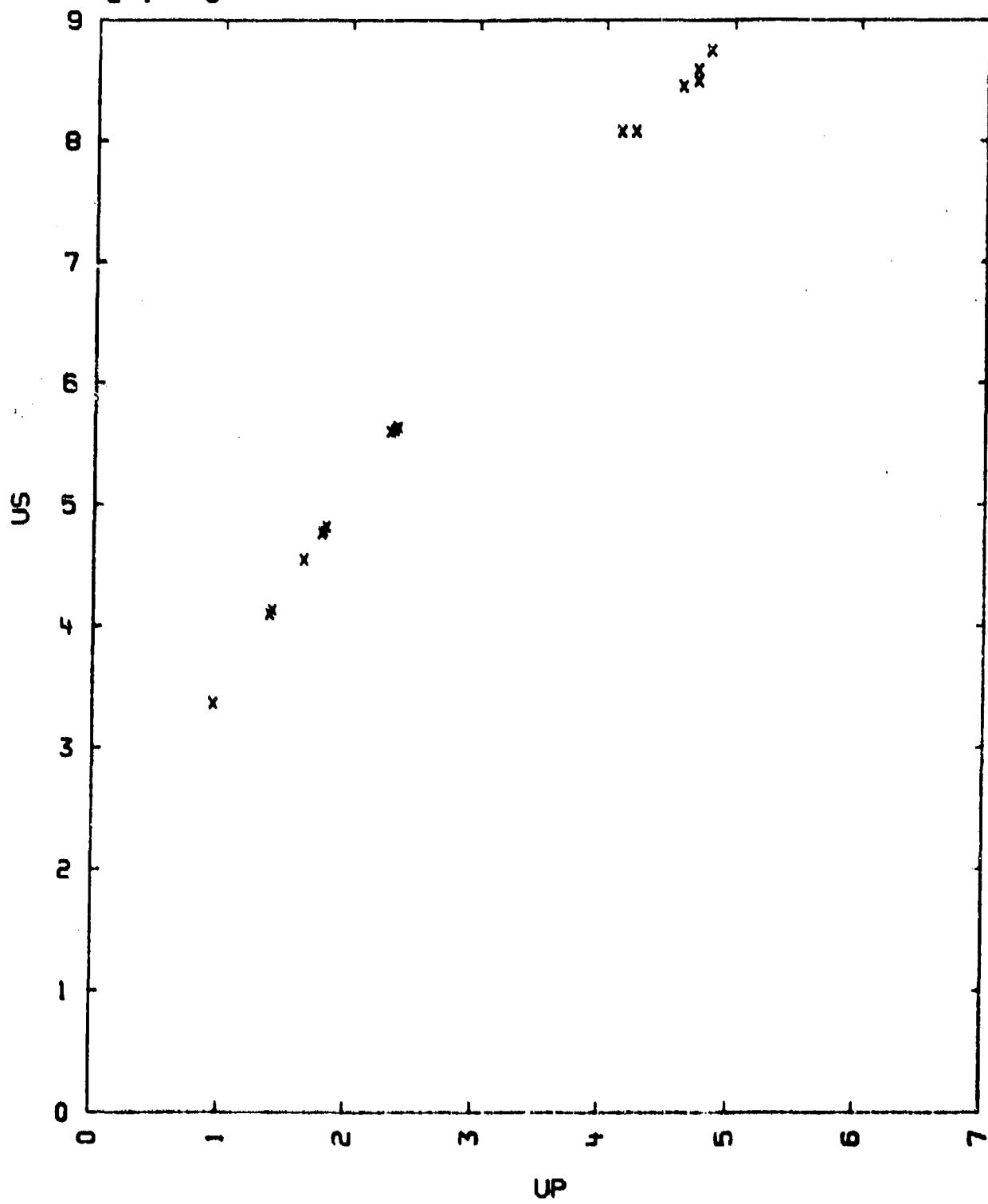
- 1) SOURCE: WALSH J. M. AND RICE H. H.
JOURNAL OF CHEMICAL PHYSICS, VOL. 26, P. 815 (1957)
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION TECHNIQUE B
STANDARD MATERIAL 24ST ALUMINUM
- 3) THE TOTAL SCATTER IN U_S IS TYPICALLY 3 TO 4 PERCENT, AND THE AVERAGE VALUE OF U_S HAS A PROBABLE ERROR OF ABOUT 0.5 PERCENT.
THE UNCERTAINTY IN U_P IS COMPARABLE TO THIS AVERAGE VALUE.
- 4) C₀ WAS OBTAINED FROM THE AMERICAN INSTITUTE OF PHYSICS HANDBOOK,
(MCGRAW-HILL BOOK CO., N. Y. 1963) 2ND ED.

UDG/14/77

TABLE I

WATER (HYDROGEN OXIDE)

2-1---3



2-1---4
WATERH₂OV₀ = 1.00

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBARS AND DENSITY IN G/CC.

TABLE

RH ₀₀	SAMPLE					STANDARD	
	US	UP	P	V/V ₀		UFS (ALUMINUM)	UFS (PLEXIGLASS)
1.00	5.835	2.365	138	0.595		4.740	
-	5.900	2.270	134	0.615		4.580	
-	5.725	2.140	122.5	0.626		4.310	
-	5.625	2.115	119	0.624		4.230	
-	5.555	2.125	118	0.617		4.220	
-	5.545	2.110	117	0.619		4.190	
-	5.460	2.180	119	0.601	2.890		
-	5.395	2.120	114.5	0.607	2.785		
-	5.260	2.165	115	0.585	2.860		
-	5.235	2.140	112	0.591	2.775		
-	5.160	2.005	103.5	0.611	2.630		
-	5.225	1.980	103.5	0.621	2.625		
-	5.185	1.975	102.5	0.619	2.640		
-	4.830	1.915	92.5	0.604	2.460		
-	4.730	1.840	87	0.611	2.360		
-	4.570	1.675	76.5	0.633	2.145		
-	4.165	1.465	61	0.648	1.840		
-	4.280	1.390	59.5	0.675	1.770		
-	4.075	1.340	54.5	0.671	1.695		
-	3.885	1.300	50.5	0.665	1.615		
-	3.635	1.100	40	0.697	1.375		
-	3.465	1.110	38.5	0.680	1.360		
-	3.625	1.060	38.5	0.708	1.300		
-	3.480	1.080	37.5	0.690	1.325		
-	3.240	0.970	31.5	0.697	1.170		
-	3.205	0.970	31	0.697	1.145		

US = 1.51 + 1.85 UP KM/SEC. 510.US + 0.15 KM/SEC.

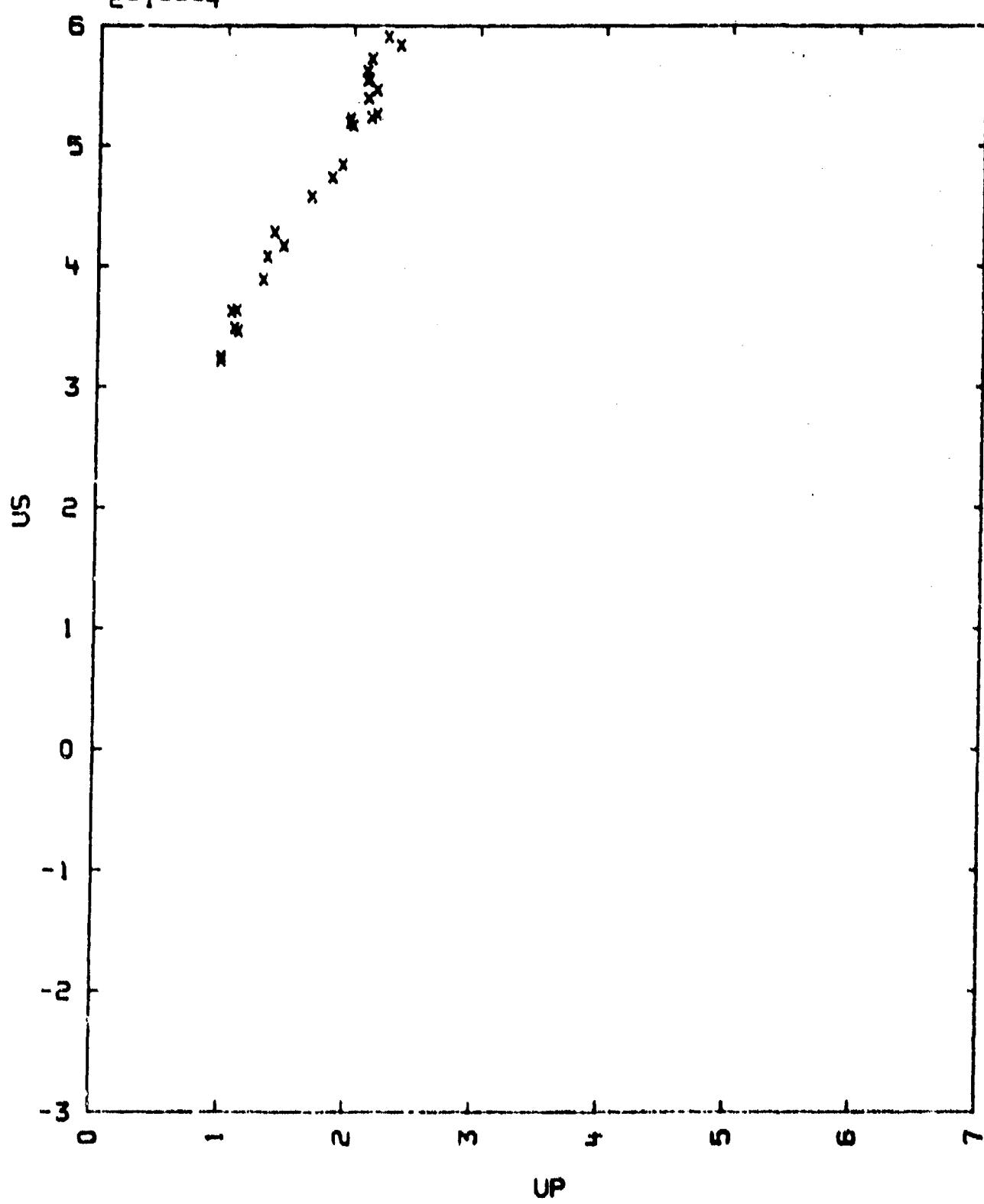
COMMENTS:

- 1) SOURCE: BERGER J. AND FAQUIGNON C.
 PRIVATE COMMUNICATION (1964), B.P. NO. 7, SEVRAN, FRANCE
- 2) EXPERIMENTAL TECHNIQUE B
 DATA REDUCTION TECHNIQUE B
 STANDARD MATERIALS PLEXIGLASS AND ALUMINUM ALMg ALLOY

TABLE I

WATER

2-1---4



2-1---5
WATER

H2-O

TC= 28 DEG C.
VOL=1.0037 CC/O

THE TABLE LISTS T IN DEG.C., RHO0 IN G/CC. VELOCITIES IN KM/SEC AND P IN KBARS. RI IS REFRACTIVE INDEX. AL IS 2024 ALUMINUM

TABLE

SAMPLE							STANDARD	
T0	RHO0	US	UP	P	V/V0	RI	UFS	MAT
28.	0.9983	3.87	1.245	48.0	0.6783	1.474	1.55	AL
28.	0.9983	4.09	1.40	57.0	0.6577	1.482	1.78	AL
20.	0.9942			0.	1.00	1.333		

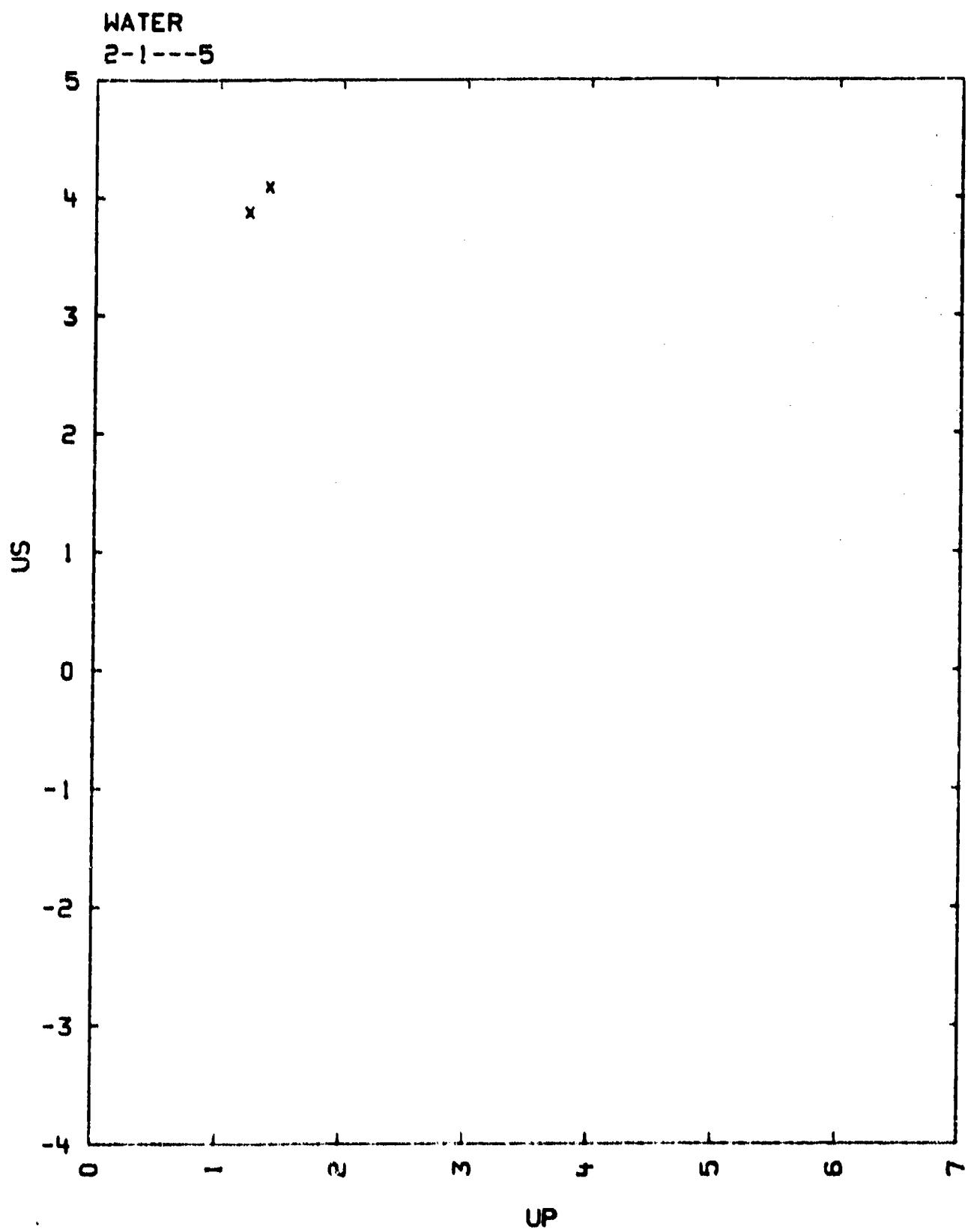
US *

COMMENTS:

- 1) SOURCE: AHRENS T.J. AND RUDERMAN M.H.
J. APPL. PHYS., V.37 P 4758 (1966)
- 2) EXPERIMENTAL TECHNIQUE: D AND C1
DATA REDUCTION METHOD : B
- 3) VOL AND RHO0 FROM THE AMERICAN INST. OF PHYS. HANDBOOK. D.E. GRAY EDITOR (MCGRAW HILL BOOK CO. 1972) 3RD ED.
- 4) UNCERTAINTY: DEL US=1-1.5 PERCENT
DEL UP=2.5 - MAXIMUM
DEL RI=1.3 -

UOB/14/77

TABLE I



10-9---1
CHLORINE TRIFLUORIDE

CL-F3

$$T_0 = 0.0 + 0.7 \text{ DEG. C.}$$

$$V_0 = 0.5305 + 0.5 \text{ CC/0}$$

$$C_0 = 0.904 \text{ KM/SEC.}$$

THE TABLE LISTS DENSITY IN G/CC., VELOCITIES IN KM/SEC., AND PRESSURE IN KBAR.

TABLE

RHOD	SAMPLE				STANDARD	
	US	UP	P	V/V0	UP(ST1)	P(ST1)
1.885	3.24	1.17	72.	0.64	0.80	144.
-	3.94	1.61	120.	0.592	1.14	220.
-	4.56	1.96	158.	0.57	1.43	291.
-	4.86	2.17	199.	0.554	1.61	336.
-	6.09	3.09	353.	0.49	2.37	563.

$$US = 1.318 + 1.64 \cdot UP \text{ FOR UP LESS THAN } 2.17 \text{ KM/SEC.}$$

$$US = 2.147 + 1.26 \cdot UP \text{ FOR UP GREATER THAN } 2.17 \text{ KM/SEC., OR}$$

$$US = 0.947 + 2.12 \cdot UP^{+2.1} \text{ KM/SEC OVER THE TOTAL RANGE}$$

$$\pm 10 \cdot US + 0.034 \text{ KM/SEC.}$$

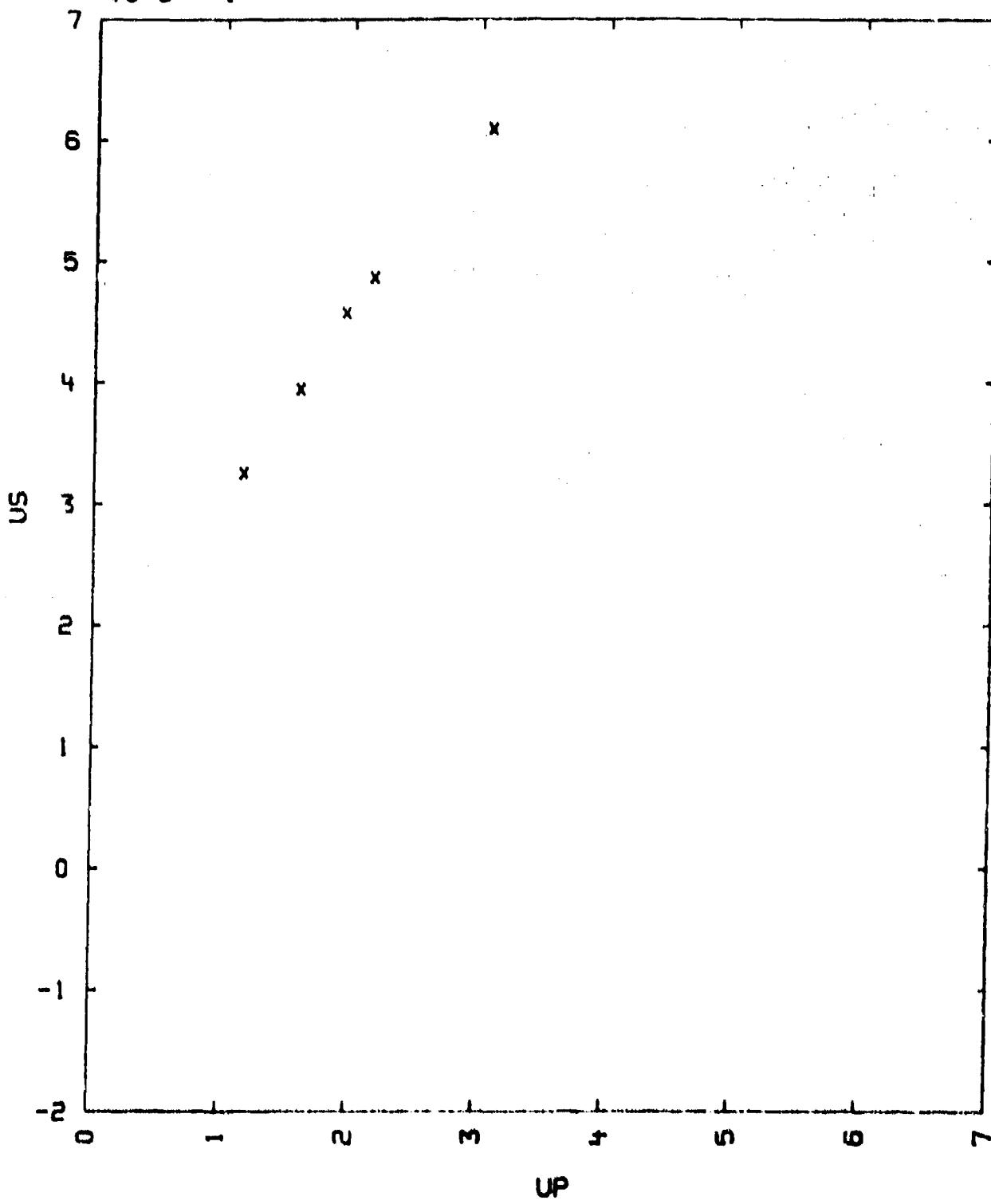
COMMENTS:

- 1) SOURCE: JEFFRIES, R. A. AND HACKERLE J.
LOS ALAMOS REPORT: LA-3453 (1966)
LOS ALAMOS SCIENTIFIC LAB., BOX 1663, LOS ALAMOS, N. M. 87544
- 2) EXPERIMENTAL TECHNIQUE: B
DATA REDUCTION TECHNIQUE: B (STANDARD MATERIAL: 2024 AL. ALLOY)
- 3) ERROR ESTIMATES FOR US ARE: .02 .01 .02 .01 .10 KM/SEC.
ERROR ESTIMATES FOR UP ARE: .02 .01 .02 .01 .10 KM/SEC.
IN THE ORDER OF THE TABLE LISTING.
- 4) MEASUREMENTS OF CO AS A FUNCTION OF TEMPERATURE (T) YIELDED:
 $C_0 = 0.904(1.0 - 0.0038 \cdot T + 0.00000 \cdot T^{+2.1}) \text{ KM/SEC.}, \text{ BETWEEN } T = -60$
AND +20 DEG. C.

UOB/14/77

TABLE 1

CHLORINE TRIFLUORIDE
10-9---1



18-14-2-1---1
AMMONIUM SULFATE

(N-H4)2-S-O4 + N2-S-MB-O4
SPECIFIC SURFACE AREA IN (CM⁻²)/G.: 540 AND 1800 FOR THE LAST FIVE
ENTRIES IN TABLE III.

$$V_0 = 0.368 - 0.769 \text{ CC/G.}$$

$$V_{01} = 0.3653 \text{ CC/G.}$$

THE TABLES BELOW GIVE DENSITY IN G/CC., VELOCITIES IN KM/SEC AND
PRESSURE IN KBARS. P(STD) IS THE PRESSURE IN THE STANDARD.

TABLE I

SAMPLE						STANDARD	
RHO0	US	UP	UFS	P	V/V0	P(STD)	
1.73	3.92	0.20	0.45	14.	0.949	10.	
-	4.50	0.55	1.21	43.	0.878	31.	
-	4.80	0.85	1.69	77.	0.806	59.	
-	5.81	1.46	3.0	147.	0.749	111.	
-	6.16	1.87		200	0.696	161.	

$$US = 3.71 + 1.34 \cdot UP \text{ KM/SEC.}$$

$$\Sigma \text{SIGMA US} = 0.13 \text{ KM/SEC}$$

TABLE II

SAMPLE						STANDARD	
RHO0	US	UP	UFS	P	V/V0	P(STD)	
1.6	2.43	0.28	0.44	11.	0.987	10.	
-	3.24	0.61	1.13	32.	0.814	28.	
-	3.53	0.68	1.21	38.	0.808	30.	
-	3.93	1.02	2.84	64.	0.742	57.	
-	4.20	0.99	1.87	66.	0.764	57.	
-	4.34	1.13	2.57	78.	0.746	63.	
-	5.18	1.57	3.65	130.	0.697	112.	
-	5.78	1.83	4.88	170.	0.685	138.	

$$US = 2.29 + 1.91 \cdot UP - 0.107 / UP \text{ KM/SEC.}$$

$$\Sigma \text{SIGMA US} = 0.12 \text{ KM/SEC.}$$

TABLE III

SAMPLE						STANDARD	
--------	--	--	--	--	--	----------	--

UOB/14/77

RHO0	US	UP	UFS	P	V/V0	P(ST)
-	5.26	2.31	5.60	158.	0.561	162.
-	4.74	1.79		110.	0.622	114.
-	3.51	1.21	2.98	55.	0.655	60.
-	2.65	0.81	1.83	28.	0.694	32.
-	1.57	0.36	0.56	7.	0.771	10.
-	5.50	2.50		178.	0.545	185.
-	5.35	2.29		159.	0.572	184.
-	4.84	1.83		115.	0.622	116.
-	4.04	1.80		113.	0.628	114.
-	4.40	1.78		102.	0.593	108.
-	3.56	1.15		53.	0.677	55.
-	2.76	0.78	0.84	28.	0.717	31.
-	5.40	2.26	5.6	158.	0.581	182.
-	4.54	1.77	4.2	104.	0.610	109.
-	3.38	1.12		49.	0.669	54.
-	2.67	0.96		33.	0.640	40.
-	1.78	0.41		9.	0.770	13.

$$US = 0.55 + 2.94 \cdot UP - 0.37 \cdot UP^2, \text{ KM/SEC.}$$

$$S10.US = 0.15 \text{ KM/SEC.}$$

COMMENTS:

- 1) SOURCE: JOHNSON J. O. AND HACKERLE J.
HIGH DYNAMIC PRESSURE SYMPOSIUM, I.U.T.A.M., SEPT. 11-15 1967
PARIS, FRANCE.
- 2) EXPERIMENTAL TECHNIQUE D.
DATA REDUCTION TECHNIQUE: D. STANDARD MATERIAL - LUCITE, WITH
 $US = 2.75 + 1.49 \cdot UP$ AND $UP = 0.5 \cdot UFS$
- 3) THE SAMPLES WERE ANALYTICAL REAGENT GRADE AMMONIUM SULFATE WHICH
WAS PRESSED INTO 2.54 CM DIAMETER BY 0.203 CM THICK WAFERS.
- 4) VOL WAS CALCULATED USING THE LATTICE CONSTANTS A = 7.782,
B. = 5.993, AND C. = 10.636 ANGSTOMS FOR A ORTHORHOMBIC CELL.
WYCKOFF, CRYSTAL STRUCTURES VOL. 3 (JOHN WILEY AND SONS, NEW YORK,
1963) 2ND. ED.
- 5) ESTIMATED PERCENT UNCERTAINTIES ARE 3.5 IN P(ST), 2.6 IN UP, 2.1 IN US
2.3 IN P AND 3.1 IN V/V0

008/14/77

TABLE I

AMMONIUM SULFATE
18-14-2-1---1

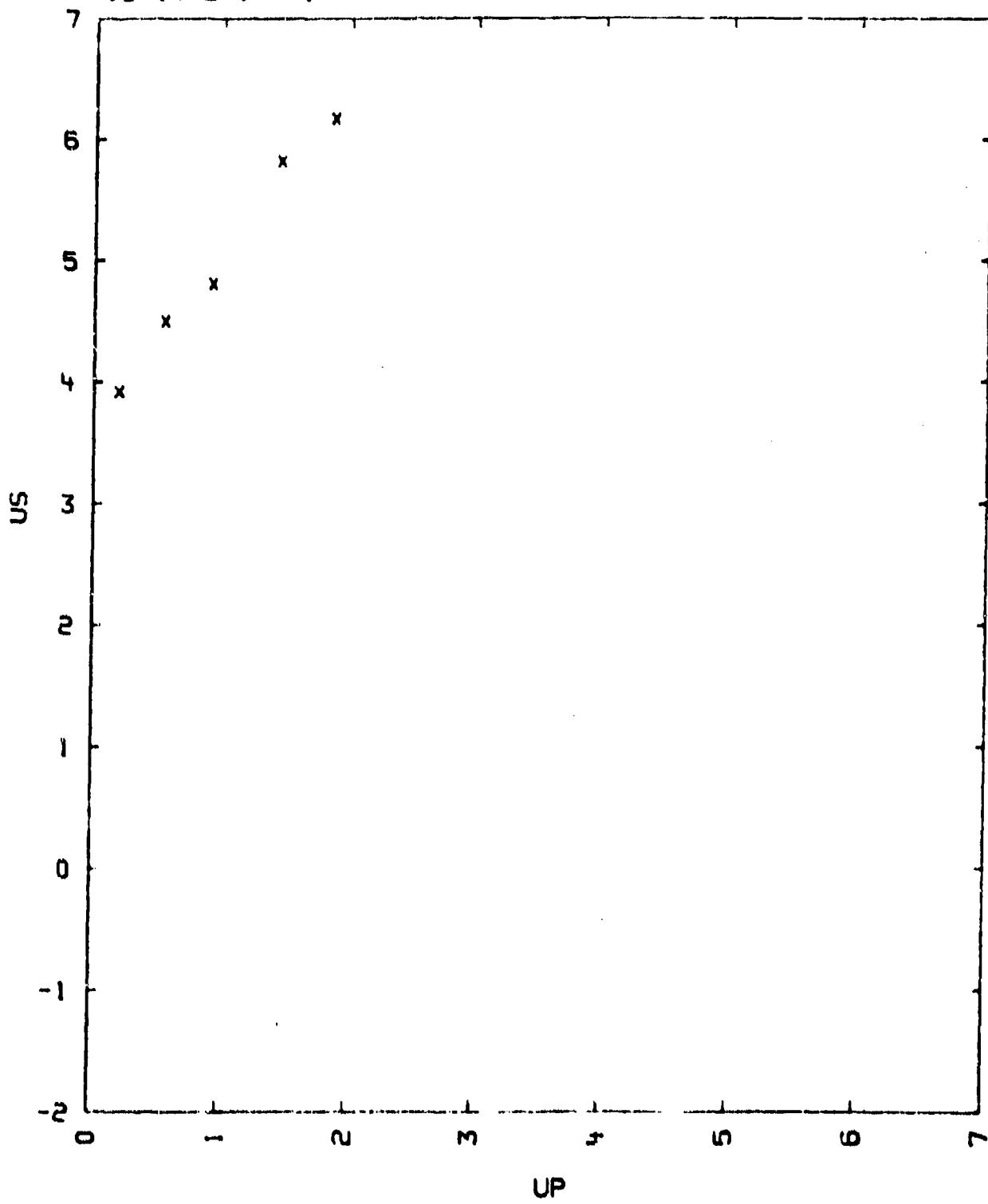


TABLE II

AMMONIUM SULFATE

18-14-2-1---1

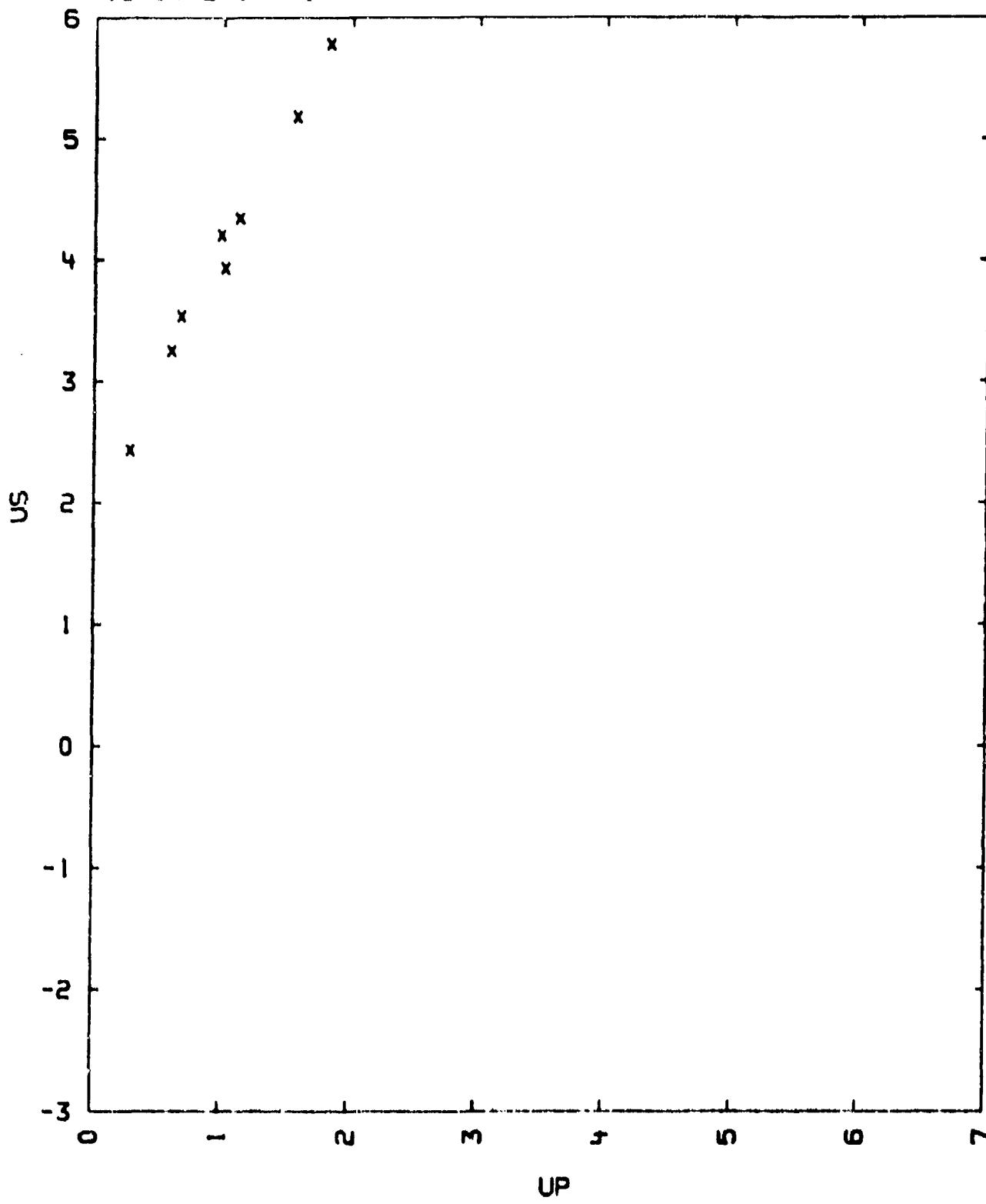
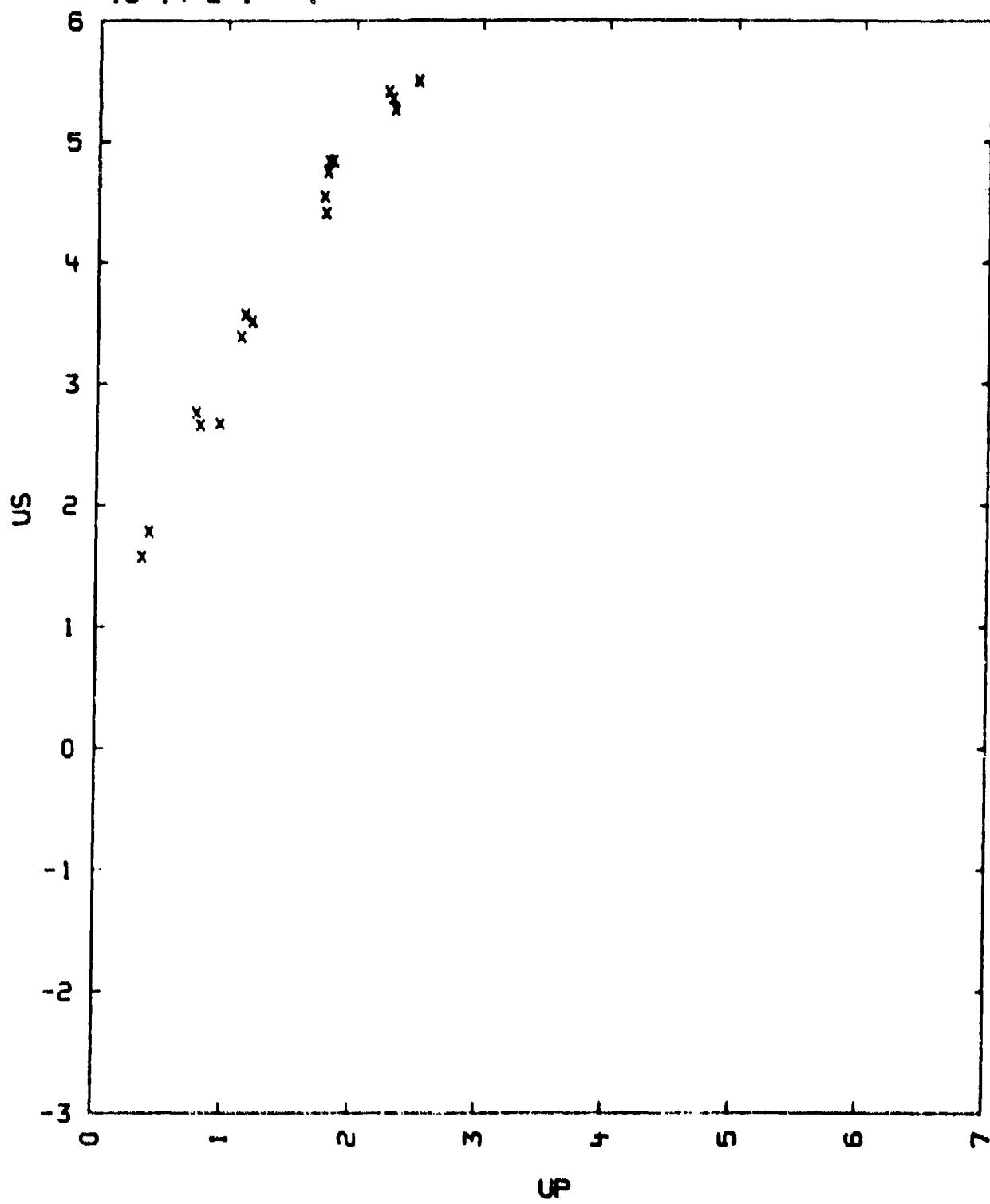


TABLE III

AMMONIUM SULFATE

18-14-2-1---1



23-1---1
CARBON DIOXIDE

C-02

$T_0 = 198$ DEGREES KELVIN
 $V_0 = .649$ CC/G

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN MM/MICROSEC., AND PRESSURE IN KILOBARS.

TABLE

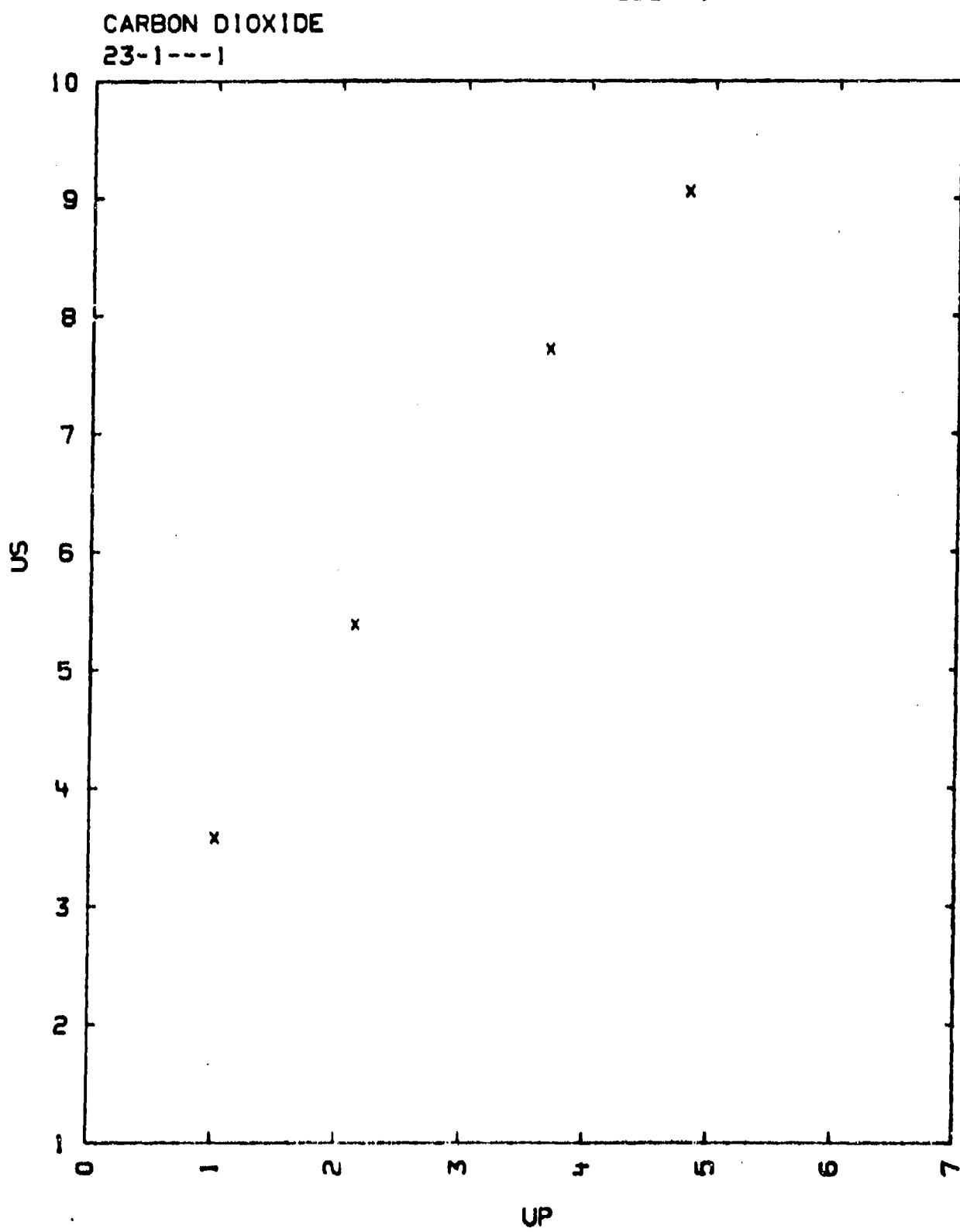
US	UP	P	V/V0
3.57	1.03	53.4	.795
5.30	2.14	167	.841
7.71	3.68	412	.936
9.09	4.79	631	.987

$$US = 1.65 + 1.93 \cdot UP - 0.080 \cdot UP^2 \text{ KM/SEC. SIG.US=0.055}$$

COMMENTS:

- 1) SOURCE: ZUBAREV, V.N. AND TELEGIN, O.S.
SOVIET PHYS. -OBLADY, VOL. 7, P. 34 (1962)
- 2) EXPERIMENTAL TECHNIQUE A
DATA REDUCTION TECHNIQUE B
(THE ADIABAT AND HUGONIOT ARE ASSUMED IDENTICAL)
- 3) EACH POINT IS AN AVERAGE OF 4 TO 12 MEASUREMENTS WITH A MEAN SQUARE DEVIATION OF 1 TO 2 PERCENT.

TABLE I



23-10---1
CARBON TETRACHLORIDE

C-CL4 99+ WT. PERCENT

$T_0 = 12$ TO 30 DEG. C.
 $V_0 = 0.6211$ TO 0.6353 CC/G.

$\text{CO}(22 \text{ DEG. C.}) = 0.03 \text{ KM/SEC.}$

THE TABLE LISTS TEMPERATURE IN DEG. C., DENSITY IN G/CC., VELOCITIES IN KM/SEC. AND PRESSURE IN KBAR. DUS AND DUP ARE THE UNCERTAINTIES IN US AND UP

TABLE

T	RH00	SAMPLE					P	V/V0	- STANDARD -	
		US	DUS	UP	DUP	US(STD)			US(STD)	DUS(STD)
22	1.590	2.32	0.01	0.58	0.08	21.	0.752	5.93	0.07	
29	1.577	2.27	0.01	0.69	0.04	25.	0.697	6.02	0.03	
28	1.571	2.47	0.01	0.69	0.04	27.	0.722	6.02	0.04	
28	1.571	2.79	0.01	0.82	0.02	36.	0.702	6.16	0.04	
24	1.586	2.91	0.01	0.90	0.03	41.	0.692	6.22	0.03	
20	1.594	2.95	0.01	0.90	0.04	42.	0.694	6.23	0.03	
19	1.596	3.28	0.01	1.12	0.03	59.	0.658	6.43	0.02	
32	1.571	3.32	0.01	1.20	0.02	63.	0.637	6.50	0.02	
14	1.606	3.46	0.01	1.20	0.03	67.	0.652	6.52	0.02	
22	1.591	3.44	0.01	1.23	0.02	87.	0.643	6.54	0.02	
18	1.598	3.50	0.01	1.33	0.08	74.	0.621	6.62	0.07	
29	1.577	3.74	0.01	1.49	0.02	88.	0.601	6.78	0.02	
29	1.571	3.86	0.01	1.57	0.01	95.	0.594	6.86	0.01	
14	1.606	4.08	0.01	1.61	0.05	106.	0.604	6.92	0.04	
27	1.580	4.07	0.01	1.65	0.02	106.	0.596	6.95	0.02	
28	1.571	4.27	0.03	1.86	0.09	125.	0.565	7.14	0.08	
28	1.571	4.52	0.01	1.96	0.02	140.	0.566	7.26	0.01	
24	1.586	4.66	0.01	2.00	0.02	148.	0.572	7.31	0.02	
19	1.596	4.71	0.01	2.04	0.04	153.	0.568	7.35	0.03	
30	1.574	4.88	0.01	2.26	0.03	174.	0.537	7.56	0.05	
12	1.610	5.34	0.02	2.46	0.03	211.	0.540	7.80	0.03	
27	1.580	5.21	0.01	2.53	0.02	208.	0.515	7.83	0.02	
23	1.588	5.72	0.03	2.87	0.07	260.	0.499	8.20	0.06	
28	1.571	5.69	0.02	2.98	0.05	266.	0.477	8.29	0.05	
28	1.571	6.13	0.03	3.13	0.03	303.	0.489	8.48	0.03	
25	1.584	6.44	0.05	3.37	0.09	344.	0.478	8.74	0.08	
19	1.598	6.80	0.02	3.58	0.04	387.	0.476	8.97	0.04	
26	1.582	6.72	0.02	3.82	0.02	384.	0.461	9.00	0.06	
27	1.580	6.78	0.03	3.70	0.09	395.	0.455	9.08	0.08	
24	1.586	7.13	0.03	3.98	0.08	450.	0.441	9.39	0.09	
23	1.588	7.55	0.02	4.34	0.08	520.	0.425	9.77	0.08	
23	1.588	7.98	0.03	4.52	0.08	572.	0.432	10.00	0.08	
18	1.598	8.06	0.06	4.69	0.13	604.	0.418	10.17	0.12	
27	1.580	8.24	0.04	4.69	0.11	610.	0.431	10.18	0.10	
25	1.584	8.26	0.03	4.79	0.10	625.	0.421	10.28	0.09	

US = A + B*UP, WITH A = 1.47 KM/SEC. B = 1.57
 $SIG.A = 0.05 \text{ KM/SEC. } SIG.B = 0.03$
FOR US BETWEEN 2.3 AND 4.7 KM/SEC. AND

A = 1.97 KM/SEC B = 1.31
S10.A = 0.13 KM/SEC S10.B = 0.03
FOR US GREATER THAN 4.7 KM/SEC.

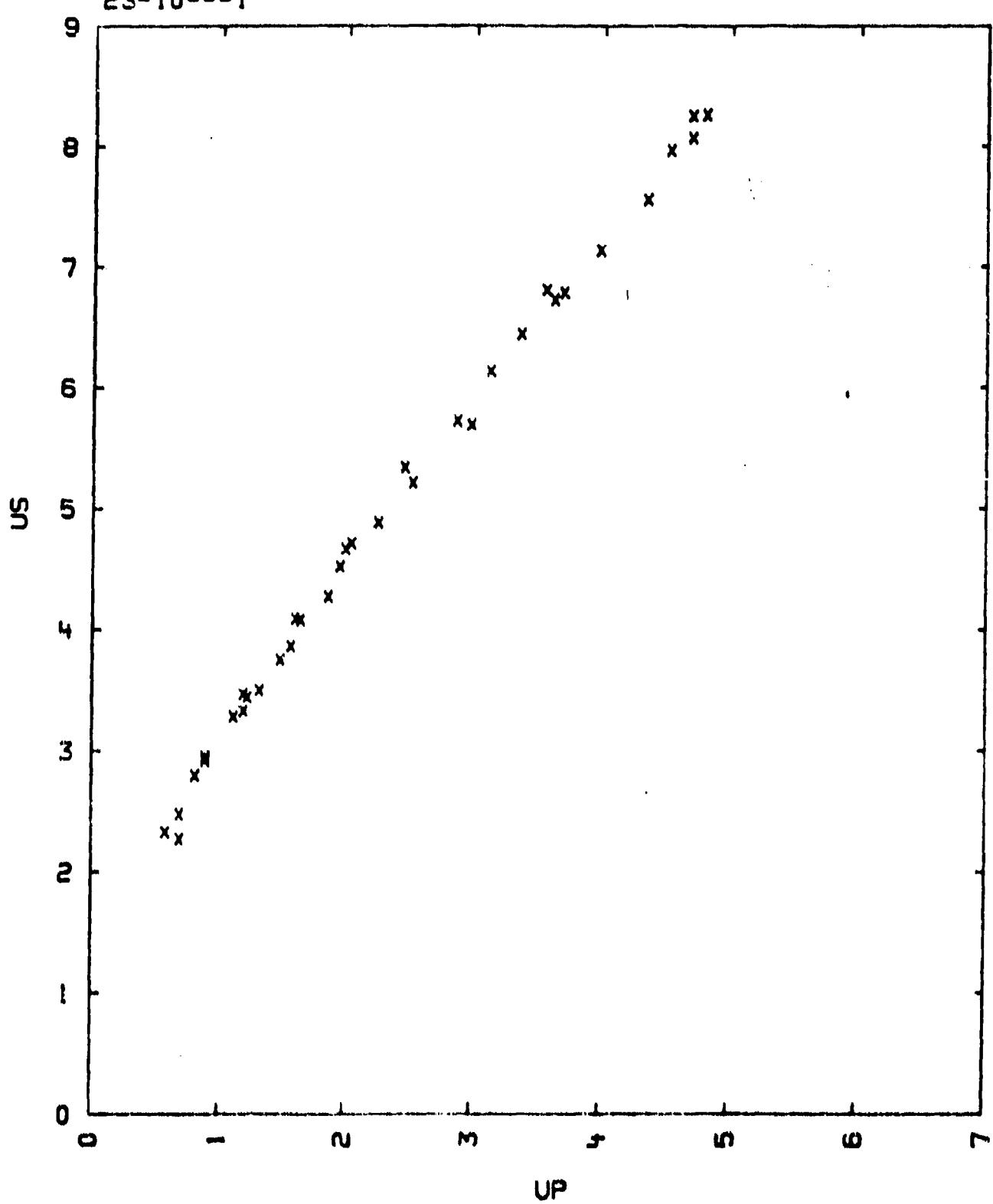
COMMENTS:

- 1) SOURCE: DICK, R. D.
LOS ALAMOS SCIENTIFIC LAB. (THESIS)
LOS ALAMOS SCIENTIFIC LAB.,
LOS ALAMOS, BOX 1663, NEW MEXICO 87544
- 2) EXPERIMENTAL TECHNIQUE: A
DATA REDUCTION TECHNIQUE: B STANDARD MATERIAL 2024 AL ALLOY WITH
US = 5.460 + 1.31B^{0.8} UP RH00 = 2.7850/CC
AND GRUNELSEN GAMMA = 2.22
- 3) THE SOUND SPEED CO HAS A DENSITY DEPENDENCE GIVEN BY $M(V0)/(C0)^{0.1/3}$
= S, WHERE S IS 94.41, 94.34 AND 94.58 AT 10, 30 AND 50 DEG.C. RESP.
AND M=MOLECULAR WEIGHT. BERGMANN L., DER ULTRASCHALL (S. HIRZEL
VERLAG, STUTTGART, 1954).

TABLE I

CARBON TETRACHLORIDE

23-10---1



23-10---2
CARBON TETRACHLORIDE

C-CL4

T0 = 22-25 DEG. CENTIGRADE
V0 = 0.629-0.634 CC/G.

CO = 0.940-0.930 KM/SEC

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBARS, DENSITY IN G/CC. AND TEMPERATURE IN DEG. CENTIGRADE.

TABLE

T0	RHO0	US	UP	P	V/V0
25	1.577	4.85	2.235	171.0	0.939
22	1.590	3.51	1.325	73.9	0.922

US =

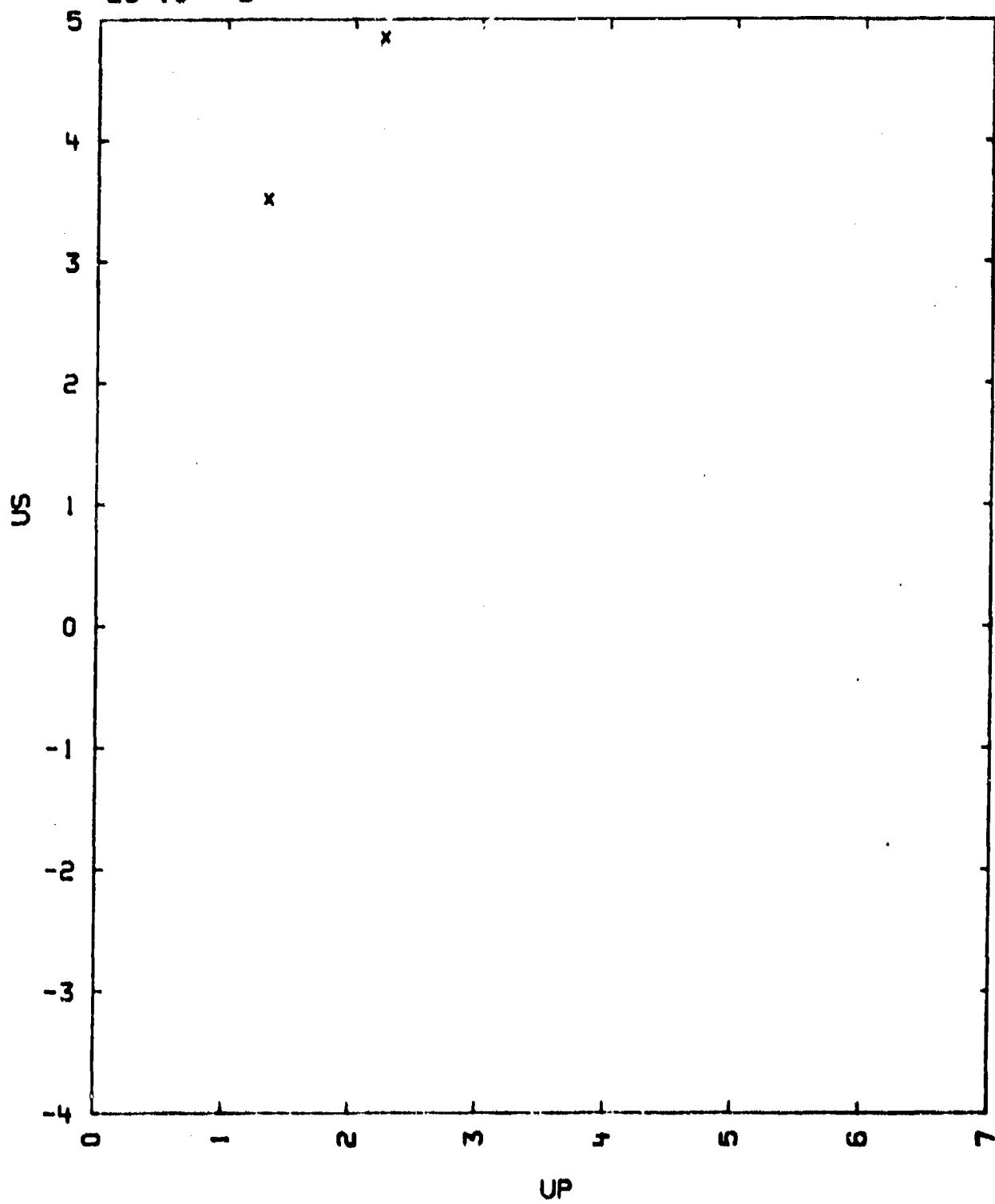
COMMENTS

- 1) SOURCE: WALSH J. H. AND RICE M. H.
JOURNAL OF CHEMICAL PHYSICS, VOL. 26, P. 815 (1957)
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION TECHNIQUE B
STANDARD MATERIAL 24ST ALUMINUM
- 3) THE VALUES FOR CO WERE DETERMINED BY INTERPOLATION OF DATA POINTS
OBTAINED FROM THE AMERICAN INSTITUTE OF PHYSICS HANDBOOK, (MCGRAW-HILL BOOK CO., N. Y. 1963) 2ND ED.

100/14/77

TABLE I

CARBON TETRACHLORIDE
23-10---2



23-10---3
CARBON TETRACHLORIDE

C-CL4

$$T_0 = 10-44 \text{ DEG. CENTIGRADE}$$

$$V_0 = 0.6108 - 0.6502 \text{ CC/0}$$

IN THE TABLE BELOW, TEMPERATURE IS GIVEN IN DEGREE CENTIGRADE, DENSITY IN G/CC., VELOCITIES IN KM/SEC., AND PRESSURE IN KILOBARS.

TABLE

SAMPLE						STANDARD
T ₀	RHO ₀	U _S	U _P	P	V/V ₀	U _S
18	1.598	4.75	2.17	164	0.543	7.45
38	1.554	4.48	1.96	138	0.558	7.20
42	1.545	4.03	1.67	104	0.586	6.90
44	1.538	3.72	1.46	83.5	0.608	6.67
41	1.548	3.50	1.26	68.5	0.637	6.48
35	1.560	3.82	1.56	93.0	0.592	6.75
10	1.616	4.33	1.90	133	0.561	7.16
32	1.568	3.97	1.58	98.4	0.602	6.77
39	1.554	4.78	2.17	160	0.544	7.43
27	1.584	3.53	1.35	75.5	0.618	6.56

$$U_S = 1.62 + 1.44 \cdot U_P \text{ KM/SEC.} \quad \Sigma U_P = 0.04 \text{ KM/SEC.}$$

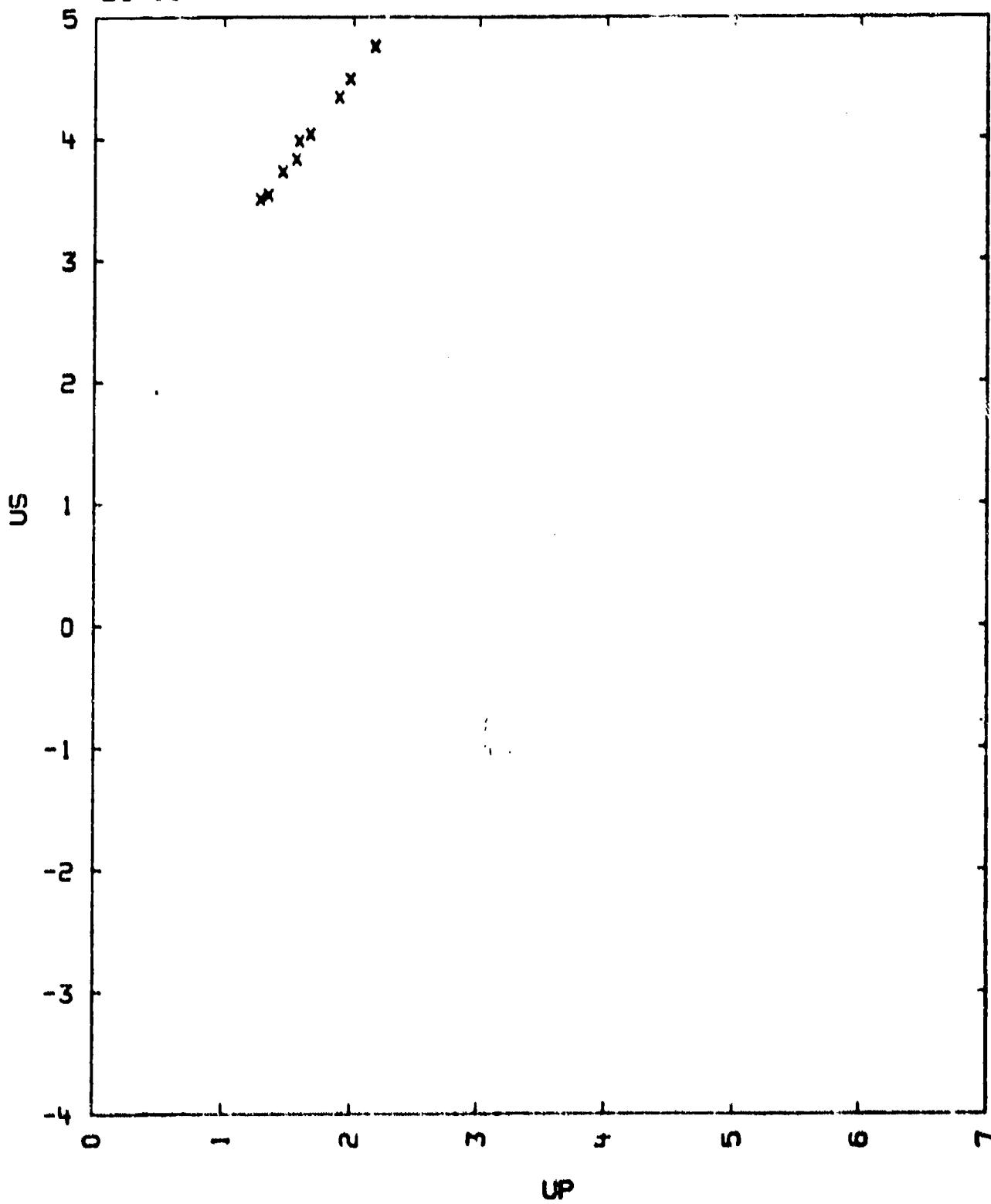
COMMENTS:

- 1) SOURCE: MITCHELL A.C. AND KEELER R.N.
PRIVATE COMMUNICATION (1967)
REVIEW OF SCIENTIFIC INSTRUMENTS (TO BE PUBLISHED).
- 2) EXPERIMENTAL TECHNIQUE A
DATA REDUCTION TECHNIQUE B
STANDARD MATERIAL 2024 ALUMINUM, WHERE $U_S = 5.355 + 1.345 \cdot U_P \text{ KM/SEC.}$
SEE MATERIAL 29---6,
 $\rho_{00} = 2.705 \cdot 0R - 0.003 \text{ G/CC.}$
- 3) THE EXPERIMENTAL UNCERTAINTY OF THE MEASURED SHOCK VELOCITIES IS
WITHIN 1 PERCENT. THE UNCERTAINTY OF CARBON TETRACHLORIDE PRESSURE
DETERMINATIONS ARE BETWEEN 3-5 PERCENT.
- 4) IN THE ABOVE TABLE, ALL THE EXPERIMENTS WITH THE EXCEPTION OF THE
LAST ENTRY HAD EXPLOSIVE IN CONTACT WITH THE BASE PLATE. THE LAST
ENTRY HAS OBTAINED USING A SLOW VELOCITY ALUMINUM FLYING PLATE.
- 5) REAGENT GRADE CARBON TETRACHLORIDE WAS USED. THE SAMPLE DENSITY AT
29 DEG. CENTIGRADE WAS 1.584 \pm 0.001 G/CC.
- 6) PERCENT DENSITY CHANGE WAS CALCULATED USING THE FOLLOWING EXPRESSION:

$$V(t) = V(0) + A t + B t^{1/2} + C t^{3/2}$$
WHERE $V(0)$ IS THE VOLUME AT 0 DEG. CENTIGRADE
 $A = 1.1838 \cdot 10^{-1.31}$
 $B = 0.09881 \cdot 10^{1.61}$
 $C = 1.35135 \cdot 10^{1.61}$

HANDBOOK OF CHEMISTRY AND PHYSICS (THE CHEMICAL RUBBER PUBLISHING CO.
CLEVELAND, OHIO, 1962-1963) 44TH ED.

TABLE I

CARBON TETRACHLORIDE
23-10---3

23-14---1
CARBON DISULFIDE

C-52

T₀ = 17-33 DEG. CENTIGRADE
V₀ = 0.805-0.815 CC/G

C₀ = 1.12-1.17 KM/SEC.

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBARS, DENSITY IN G/CC., AND TEMPERATURE IN DEG. CENTIGRADE.

TABLE

T ₀	RHO ₀	US	UP	P	V/V ₀
33	1.243	4.32	2.412	129.5	0.441
17	1.227	3.37	1.415	58.5	0.580

US =

COMMENTS:

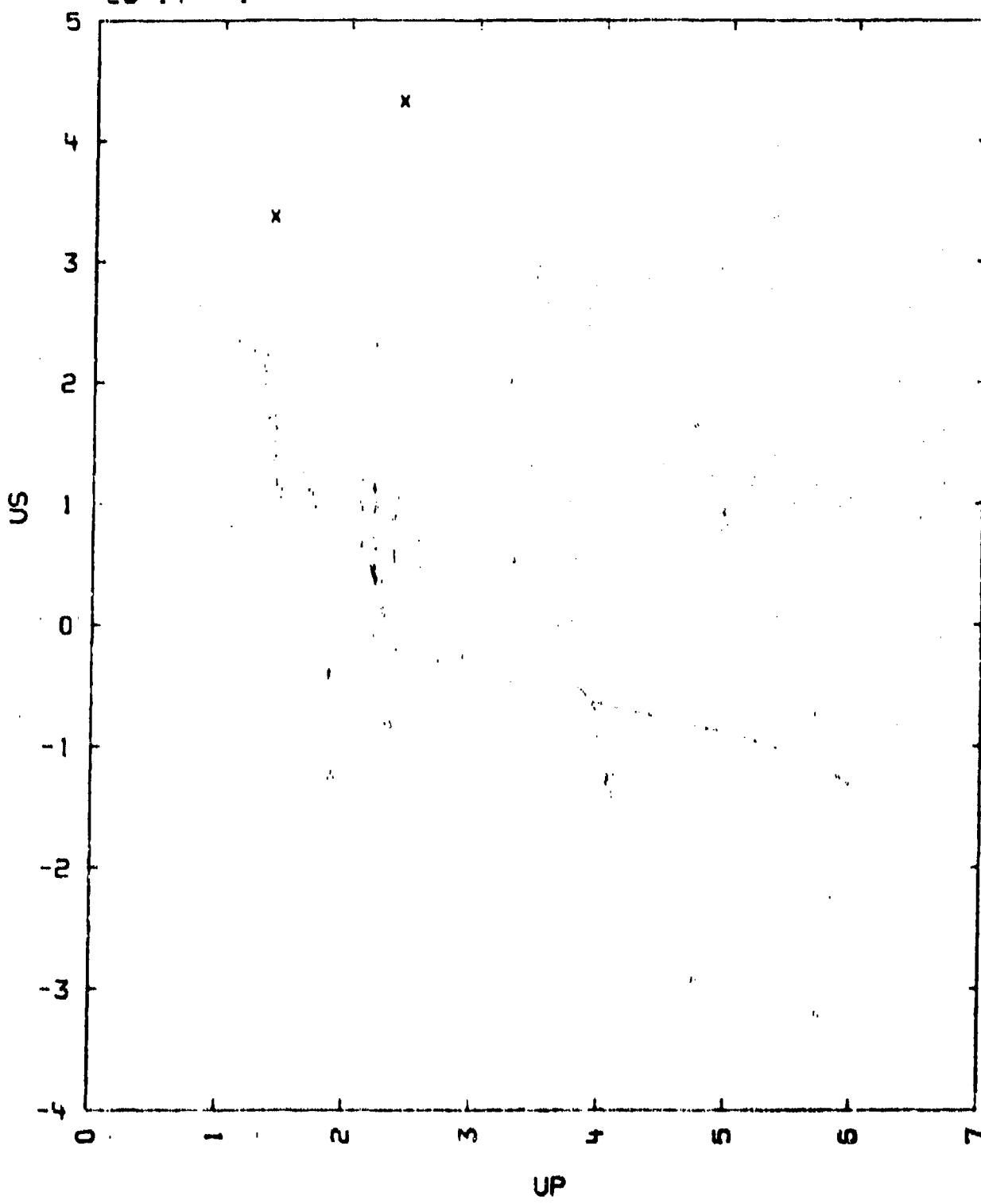
- 1) SOURCE: WALSH J. M. AND RICE M. M.
JOURNAL OF CHEMICAL PHYSICS, VOL. 26, P. 815 (1957)
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION TECHNIQUE B
STANDARD MATERIAL 24ST ALUMINUM
- 3) THE VALUES FOR C₀ WERE DETERMINED BY INTERPOLATING THE DATA POINTS
OBTAINED FROM THE AMERICAN INSTITUTE OF PHYSICS HANDBOOK, (MCRAW-HILL BOOK CO., N. Y. 1963) 2ND ED.

U06/14/77

TABLE I

CARBON DISULFIDE

23-14---1



23-14---2
CARBON DISULFIDE

C-52 99+ WT. PERCENT

T0 = 12 TO 13 DEG. C.
V0 = 0.784 TO 0.801 CC/0

CO(22 DEG. C.) = 1.16 KM/SEC.

THE TABLE LISTS TEMPERATURE IN DEG. C., VELOCITIES IN KM/SEC., DENSITY IN G/CC., AND PRESSURE IN KBAR. DUS AND DUP ARE THE UNCERTAINTIES IN US AND UP

TABLE

T	RH00	SAMPLE				P	V/V0	STANDARD	
		US	DUS	UP	DUP			US(ST)	DUS(ST)
22	1.260	2.47	0.01	0.59	0.08	18.5	0.781	5.93	0.07
29	1.249	2.41	0.01	0.71	0.04	21.	0.705	6.02	0.03
28	1.251	2.59	0.01	0.71	0.05	23.	0.727	6.02	0.04
28	1.251	2.94	0.01	0.86	0.03	32.	0.707	6.16	0.04
24	1.257	3.06	0.01	0.93	0.03	36.	0.696	6.22	0.03
20	1.263	3.09	0.01	0.94	0.04	36.	0.697	6.23	0.03
19	1.264	3.39	0.01	1.17	0.03	50.	0.655	6.43	0.02
32	1.245	3.43	0.01	1.26	0.02	54.	0.634	6.50	0.02
14	1.272	3.47	0.01	1.26	0.01	56.	0.636	6.52	0.02
22	1.260	3.47	0.01	1.29	0.02	56.	0.628	6.54	0.02
18	1.266	3.51	0.01	1.39	0.08	62.	0.603	6.62	0.07
29	1.249	3.52	0.01	1.59	0.03	70.	0.549	6.78	0.02
29	1.249	3.55	0.01	1.68	0.01	74.	0.527	6.86	0.01
14	1.272	3.65	0.01	1.74	0.05	81.	0.523	6.02	0.04
27	1.253	3.62	0.01	1.78	0.02	81.	0.507	6.95	0.02
28	1.251	3.78	0.01	2.01	0.10	95.	0.468	7.14	0.08
28	1.251	4.02	0.01	2.13	0.02	107.	0.471	7.26	0.01
24	1.257	4.18	0.00	2.17	0.02	114.	0.481	7.31	0.02
19	1.264	4.20	0.01	2.22	0.04	118.	0.473	7.35	0.03
30	1.240	4.40	0.01	2.45	0.03	134.	0.444	7.56	0.03
12	1.275	4.86	0.02	2.67	0.03	165.	0.451	7.80	0.03
27	1.253	4.80	0.01	2.73	0.02	164.	0.432	7.83	0.02
23	1.258	5.23	0.02	3.11	0.08	204.	0.406	8.20	0.06
28	1.251	5.20	0.02	3.22	0.06	209.	0.382	8.28	0.05
28	1.251	5.68	0.03	3.39	0.03	241.	0.403	8.48	0.03
25	1.255	6.04	0.03	3.64	0.03	276.	0.398	8.74	0.08
19	1.266	6.46	0.02	3.84	0.04	314.	0.406	8.97	0.04
26	1.254	6.36	0.02	3.90	0.07	311.	0.398	9.00	0.06
27	1.253	6.44	0.04	3.98	0.09	321.	0.383	9.08	0.08
24	1.257	6.73	0.03	4.30	0.09	364.	0.361	9.39	0.05
23	1.258	7.34	0.04	4.65	0.07	429.	0.368	9.77	0.06
23	1.258	7.64	0.05	4.87	0.07	468.	0.362	10.00	0.06
19	1.266	7.83	0.03	5.03	0.14	499.	0.357	10.17	0.12
27	1.253	7.98	0.08	5.03	0.12	503.	0.370	10.18	0.10
25	1.255	8.09	0.05	5.12	0.11	520.	0.367	10.28	0.09

US = A + B*UP WITH A = 1.64 KM/SEC. B = 1.46
SIG.A = 0.08 KM/SEC. SIG.B = 0.08
FOR US BETWEEN 2.4 AND 3.5 KM/SEC. AND

A = 1.25 KM/SEC. B = 1.32
SIG.A = 0.08 KM/SEC. SIG.B = 0.02
FOR US BETWEEN 3.5 AND 8.1 KM/SEC.

COMMENTS:

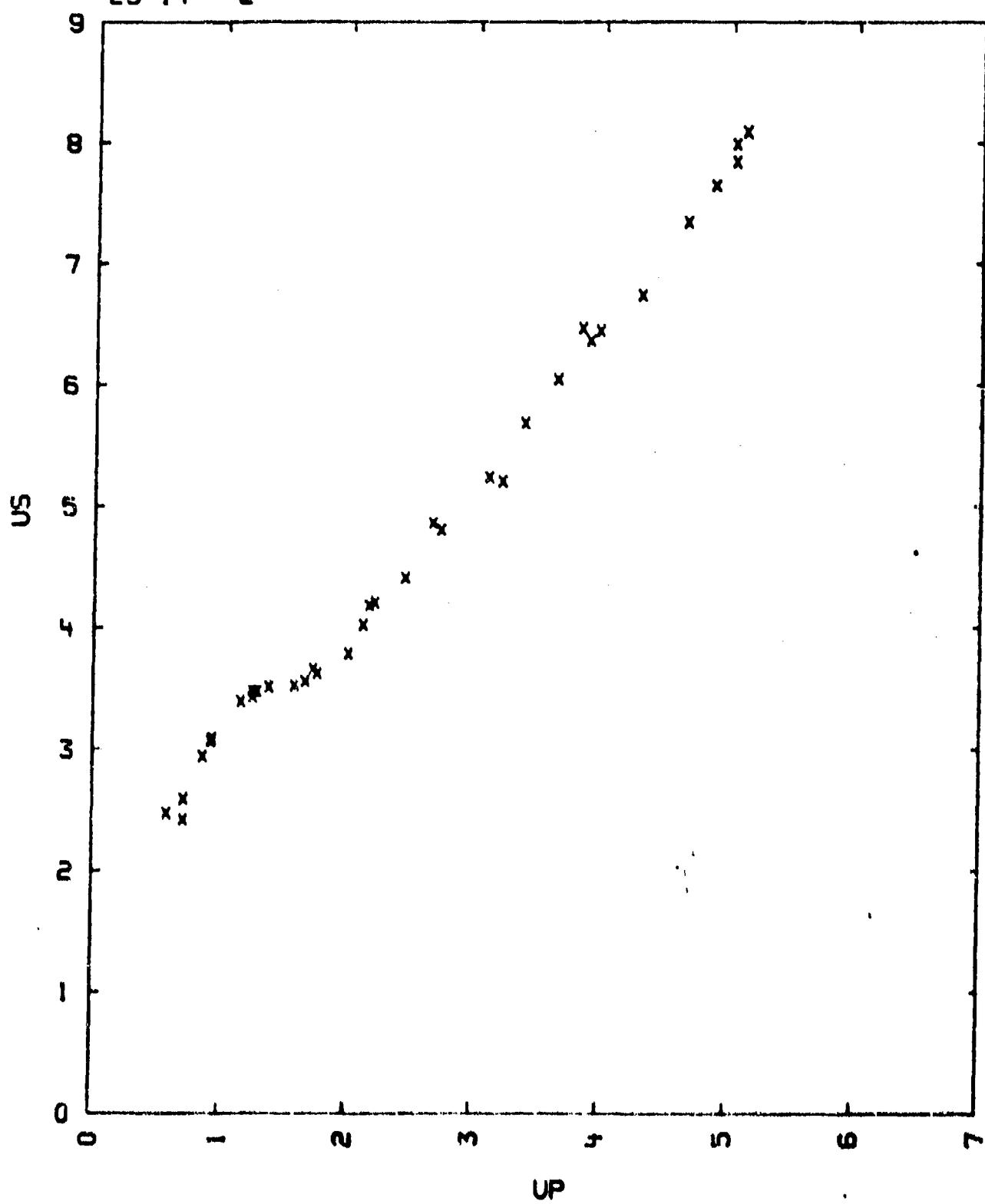
- 1) SOURCE: DICK, R.D.
LOS ALAMOS SCIENTIFIC LAB. (THESIS)
LOS ALAMOS SCIENTIFIC LAB.,
LOS ALAMOS, BOX 1663, NEW MEXICO 87544
- 2) EXPERIMENTAL TECHNIQUE: A
DATA REDUCTION TECHNIQUE: B STANDARD MATERIAL 2024 AL ALLOY WITH
US = 5.480 ± 1.310 UP RHOD = 2.7650/CC
AND GRUNEISEN GAMMA = 2.22

UDC/14/77

TABLE I

CARBON DISULFIDE

23-14---2



24-1---0
QUARTZ SUMMARY

51-02

$$V_0 = 0.3774 - 0.525 \text{ CC}/0$$

$$V_{01} = 0.3774 \text{ CC}/0$$

THE TABLE LISTS THE HUGONIOT POINTS CALCULATED FROM THE FIT GIVEN BELOW.
 UNITS ARE G/CC., KM/SEC., KBAR AND KBAR.GC/G FOR THE ENERGY DIFFERENCE.

TABLE

RHO0	US	UP	P	V/V0	E-E0
2.65	5.882	2.5	398.	0.582	31.2
-	6.869	3.0	546.	0.583	45.0
-	7.734	3.5	717.	0.547	61.2
-	8.576	4.0	909.	0.534	80.0
-	10.194	5.0	1351.	0.509	125.
-	11.722	6.0	1864.	0.488	180.
-	12.453	6.5	2145.	0.478	211.
2.204	5.179	2.5	285	0.517	31.2
-	5.976	3.0	395	0.498	45.0
-	6.795	3.5	521	0.482	61.2
-	7.512	4.0	652	0.468	80.0
1.60	4.631	2.5	185.	0.460	31.2
-	5.316	3.0	295.	0.438	45.0
-	5.979	3.5	335.	0.415	61.2
-	6.620	4.0	424.	0.395	80.0

$$US = 1.214 + 2.019 \cdot UP - 0.044 \cdot UP^{1/2} - 1.237(2.65 \cdot RH00) +$$

$$+ 0.868(2.65 \cdot RH00)^{1/2} - 0.385(2.65 \cdot RH00) \cdot UP$$

FOR UP BETWEEN THE LIMIT OF THE TABLE

$$SI0.US = 0.11 \text{ KM/SEC}$$

COMMENTS:

- 1) SOURCE: COMPILER
- 2) DATA OF 24-1---4,5,6 AND 7 ARE USED IN THIS SUMMARY. THE UP^{1/2} TERM IS CAUSED BY THE HIGHEST PRESSURE POINT OF 24-1---8 ONLY. WEIGHTS OF 4 WERE GIVEN TO THE DATA OF 24-1---4, 3 TO THOSE OF 24-1---5, 4 AND 2 TO 24-1---8, 1 TO 24-1---7. ONLY THE DATA IN THE (HIGH PRESSURE) STISHOVITE PHASE ARE USED.
- 3) AT LOWER PRESSURE AN ELASTIC PRECURSOR WHOSE STRESS (PRESSURE) LEVEL DEPENDS ON THE MAIN WAVE APPEARS. THIS PHENOMENON COMPLICATES THE ANALYSIS. INITIALLY POROUS SAMPLES ARE IN ADDITION QUITE NONUNIFORM AT THESE LOW PRESSURES DUE TO THE HIGH DYNAMIC STRENGTH OF QUARTZ.
- 4) GOOD REPRESENTATIONS OF LOW PRESSURE DYNAMIC PROPERTIES HOWEVER ARE STILL OBTAINABLE FROM 24-1---1 AND 7 FOR POROUS SAMPLES AND FROM 24-1---4 AND 5 FOR SINGLE CRYSTAL AND FUSED SAMPLES.
- 5) THE SOUNDSPEED OF STISHOVITE IS: CL = 11.01 KM/SEC

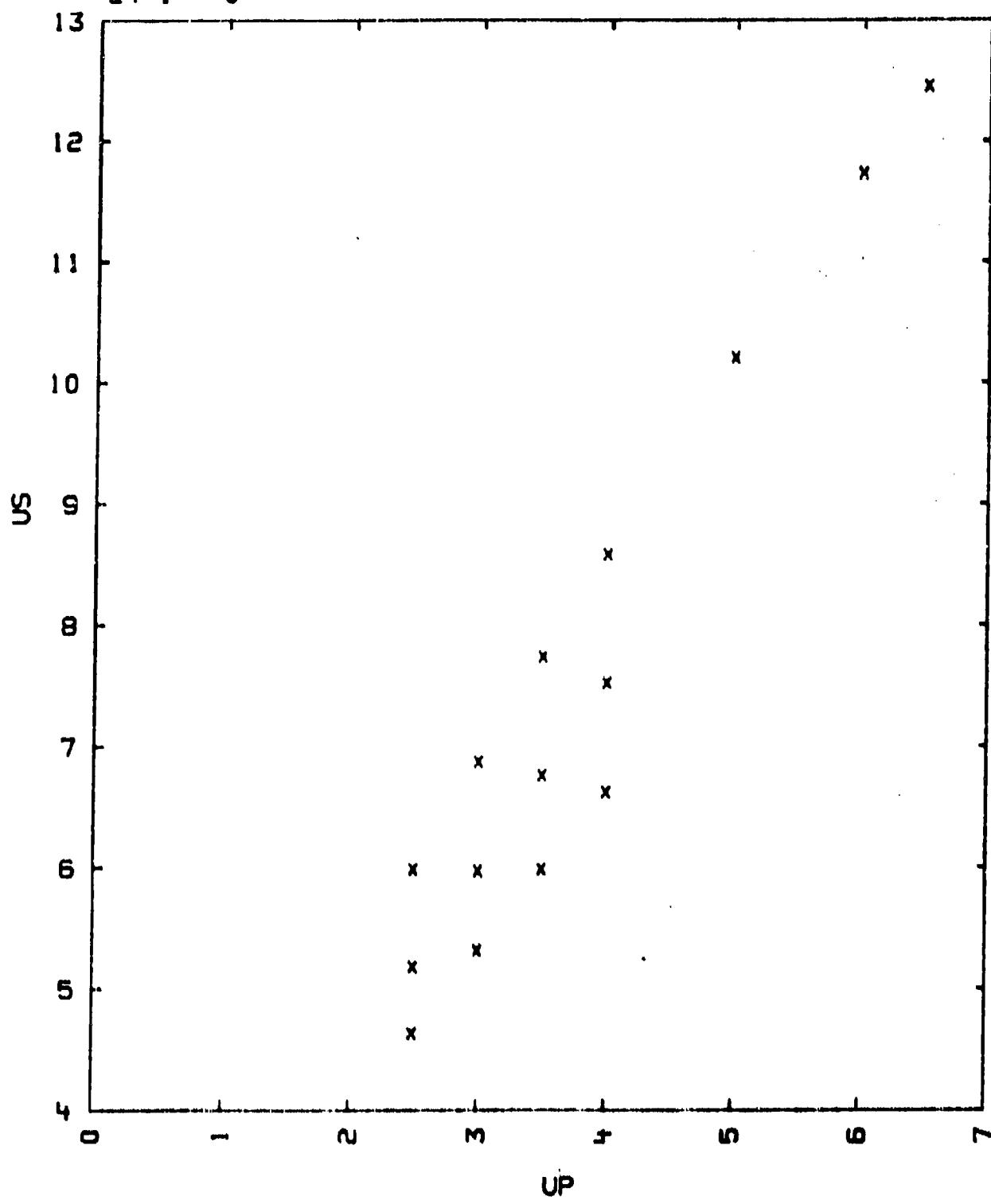
CS = 6.29 -
CD = 8.26 - AT RHOO=4.287 G/CC

D.H. CHUNG: AMERICAN GEOPHYS UNION, TRANS., V.54, P.475, (1973)
THE EXPANSION COEFFICIENTS BETWEEN T = 0 AND 600 DEG. C. ARE:
 $(1/L) \cdot DL/DT = 14.9 + 0.12 \cdot T \cdot 10^{-6}$ PER DEG. (A AXIS)
 $(1/L) \cdot DL/DT = (-.8 + .014 \cdot T) \cdot 10^{-6}$ PER DEG. (C AXIS)
 $(1/V) \cdot DV/DT = (8.9 + .038 \cdot T) \cdot 10^{-6}$ PER DEG.
WHERE THE UNCERTAINTIES ARE BETWEEN 0.5 AND 1.5 FOR THE FIRST TERM
AND BETWEEN 0.021 AND 0.023 FOR THE SECOND.
J. SCOTT WEAVER ET ALL IBID

TABLE I

QUARTZ SUMMARY

24-1---0



24-1---1
SANDSTONE COCONINO

QUARTZ S1-02 97 PERCENT BY WEIGHT
 MICROCLINE (ORTHOCLASE) K-AL (S13-08) 3 PERCENT BY WEIGHT
 POROSITY 24 PERCENT
 GRAIN SIZE .12 TO .15 MM

$V_0 = .5098 \text{ CC}/\text{O}$
 $V_{01} = .378 \text{ CC}/\text{O}$

TABLE I LISTS THE HUGONIOT VELOCITY DATA IN KM/SEC. TABLE II LISTS THE INITIAL DENSITY IN G/CC, PRESSURE IN KBAR AND COMPRESSION CORRESPONDING TO THE TABLE I ENTRIES. D STANDS FOR SAMPLE THICKNESS AND SNO IS THE SOURCE EXPERIMENT NUMBER. STM IS THE STANDARD MATERIAL: PLEXIGLAS-PLEX

TABLE I

SAMPLE						STANDARD		
NO	US1	UFS1	'UP1	US2	UFS2	UP2	UFS	STM
1				4.126	2.50	1.74	2.568	AL
2				4.039	2.24	1.53	2.208	-
3				3.295	1.93	1.26	1.77	-
4				3.141	1.63	1.11	1.54	-
5				3.321	1.88	1.09	2.46	PLEX
6				3.126	1.99	1.02	2.29	-
7	2.622	0.312	0.156	2.305	0.698	0.317	0.938	AL
8	2.853	0.148	0.074	2.385	0.499	0.371	-	-
9				4.306	4.481			
10				4.481	3.837			
11				4.600		1.98		AL
12	2.705	0.308	0.154	2.354	1.08	0.475	1.076	PLEX
13	3.027	0.172	0.086	2.357	1.22	0.500	-	-
14				4.615	2.872			
15				4.898	2.940			
16				4.633		2.041	2.872	AL
17				2.793		0.875		
18				3.11		1.09		
19				3.082		1.128		
20				4.26		1.75		
21				4.29		1.095		
22	3.080		0.085					
23	3.007		0.090					
24				2.483		0.798		
25				2.002		0.266		
26				1.601		0.066		

$US2 = 1.40 + 2.65 \cdot UP \text{ KM/SEC. } S10.US = 0.13 \text{ KM/SEC.}$

FOR UP BELOW 0.4 KM/SEC

$US2 = 1.43 + 1.98 \cdot UP \text{ KM/SEC. } S10.US = 0.27 \text{ KM/SEC.}$

FOR UP BETWEEN 0.8 AND 2. KM/SEC

TABLE II

NO	RHO0	P1	V1/V0	P2	V2/V0	D	SNO
1	1.951			144	0.557	6.32	8974
2	-			124	0.610	6.35	-
3	-			83	0.606	6.63	8975
4	-			70	0.633	6.43	-
5	-			73	0.651	6.35	8989
6	-			62	0.574	6.32	-
7	-	8.0	0.942	18	0.798	5.07	8107
8	-	4.1	0.975	18	0.798	9.29	
11	-			173	0.559	0.00*	8106
12	-	8	0.889	23.8	0.785	6.34	8208
13	-	5.1	0.971	24.9	0.709	9.58	-
16	-			186	0.559	0.00*	8342
17	2.00			48.9	0.687		8151
18	1.97			68.8	0.650		7862
19	1.975			68.2	0.632		7861
20	1.98			146	0.589		7809
21	2.00			171	0.535		8164
22	2.031	5.3	0.972				8269
23	-	5.5	0.970				-
24	2.000				39.5	0.680	8262
25	-				10.6	0.867	-
26	-				2.1	0.958	-

TABLE III

NO	US	UP	P	V/V0
27	4.86	2.15	207.	0.558
28	5.19	2.75	283.	0.470
29	5.71	2.82	317.	0.506
30	5.87	2.99	352.	0.499

US*

COMMENTS:

- 1) SOURCE: OREGON, V.O., AHRENS, T.J. AND PETERSEN, C.F.
 REPORT NO. AFCRL 63-662
 STANFORD RESEARCH INSTITUTE, MENLO PARK, CALIFORNIA.
 CATALOGUED BY DOC NO. 413819 MARCH 1963
 AHRENS, T. J. AND OREGON JR., V. O.
 J. GEOPHYS. RES., VOL. 69, P. 4839 (1964)
 AHRENS T.J., ROSENBERG J.T., RUDERMAN M.H.
 DYNAMIC PROPERTIES OF ROCKS
 PROJECT FOU-4B16. REPORT DASA 1868 (SEPT. 30 1966)
 STANFORD RESEARCH INSTITUTE
 MENLO PARK, CALIF., USA
- 2) EXPERIMENTAL TECHNIQUE C1 EXCEPT FOR NO: 18 20 21 22 AND 23

USED METHOD D
IN NO: 24 25 AND 26
AN XRAY METHOD WAS USED

DATA REDUCTION METHOD B AND D WITH 2UP+UFS.

- 3) • INDICATES VALUES OBTAINED FROM EXTRAPOLATION OF EXPERIMENTAL SHOCK VELOCITIES TO ZERO SAMPLE THICKNESS.
- 4) PI AND V1/V0 OBTAINED FROM US1 AND UP1, EXCEPT FOR LAST PI ENTRY, WHICH WAS OBTAINED WITH A QUARTZ TRANSDUCER.
P2 AND V2/V0 WERE OBTAINED FROM THE INTERFACE CONDITION WITH BRASS AND ALUMINUM STANDARDS.
- 5) VOI LEADS TO A 26 PERCENT POROSITY INSTEAD OF THE 24.1 PER CENT MEASURED BY THE ABOVE SOURCE.
VOI OBTAINED FROM QUARTZ AND MICROCLINE DENSITIES GIVEN IN:
DANAS MANUAL OF MINERALOGY (JOHN WILEY AND SONS, NEW-YORK 1983)
1ST ED.

006/14/77

TABLE I

SANDSTONE COCONINO

24-1---1

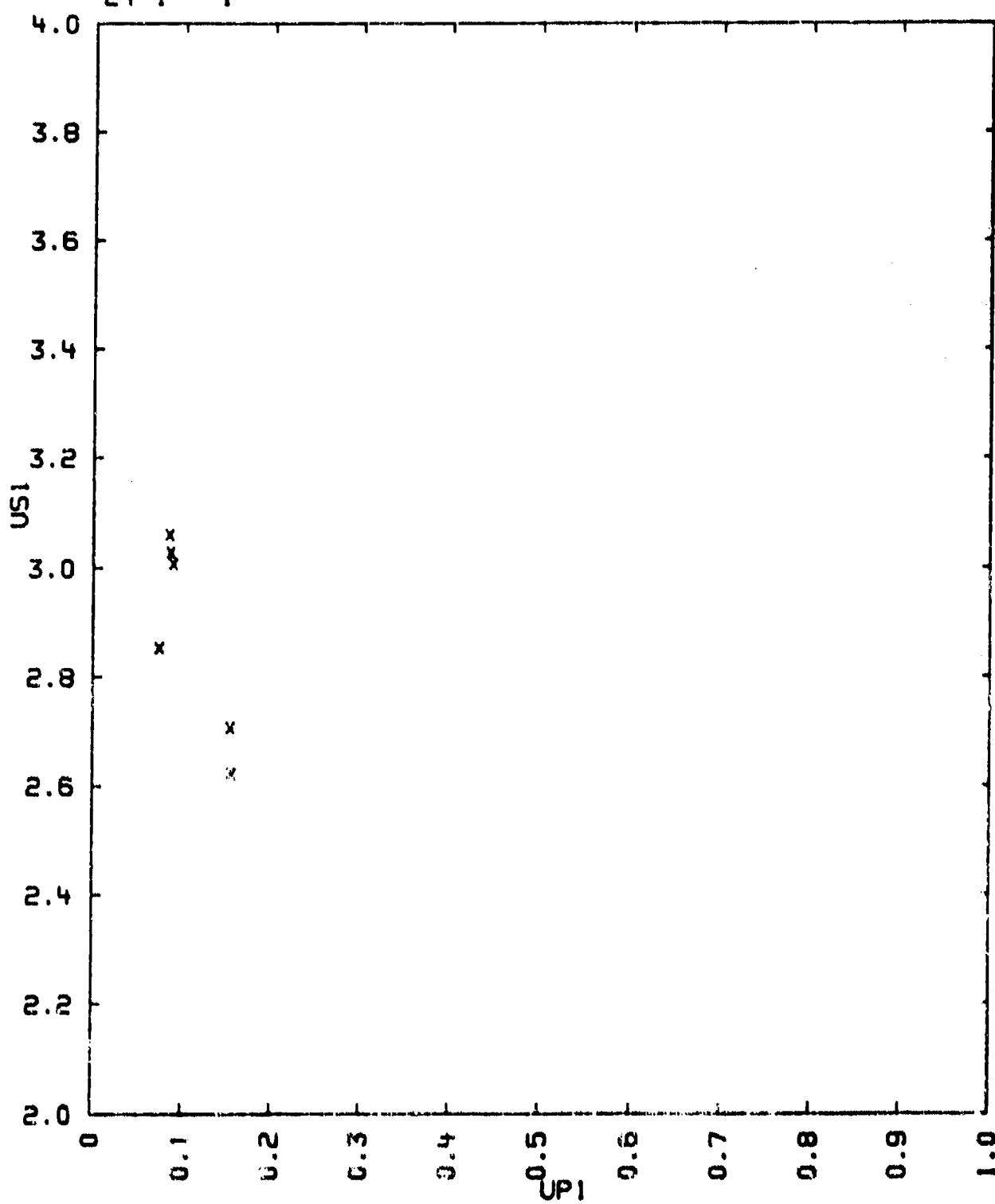


TABLE I

SANDSTONE COCONINO
24-1---1

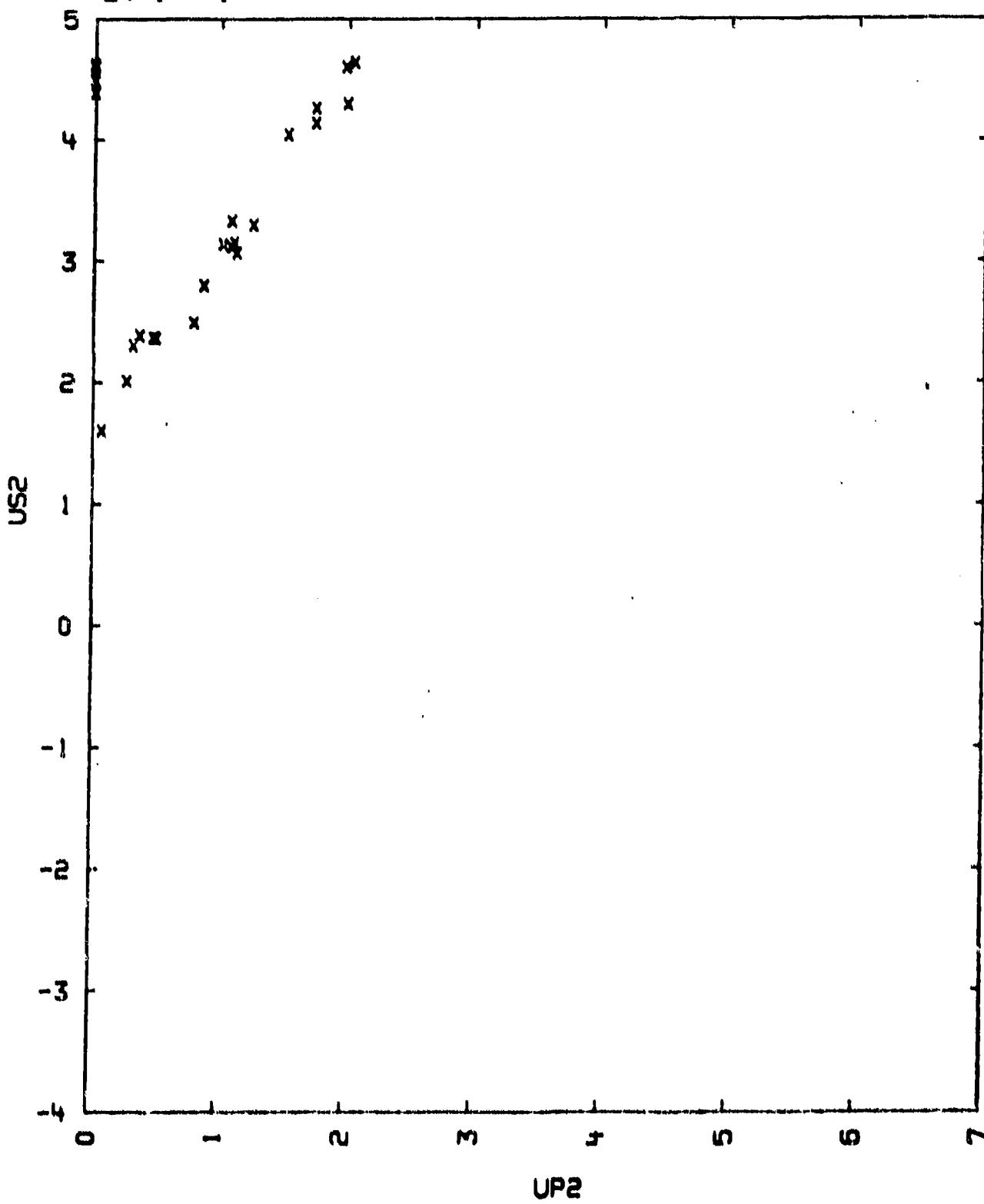
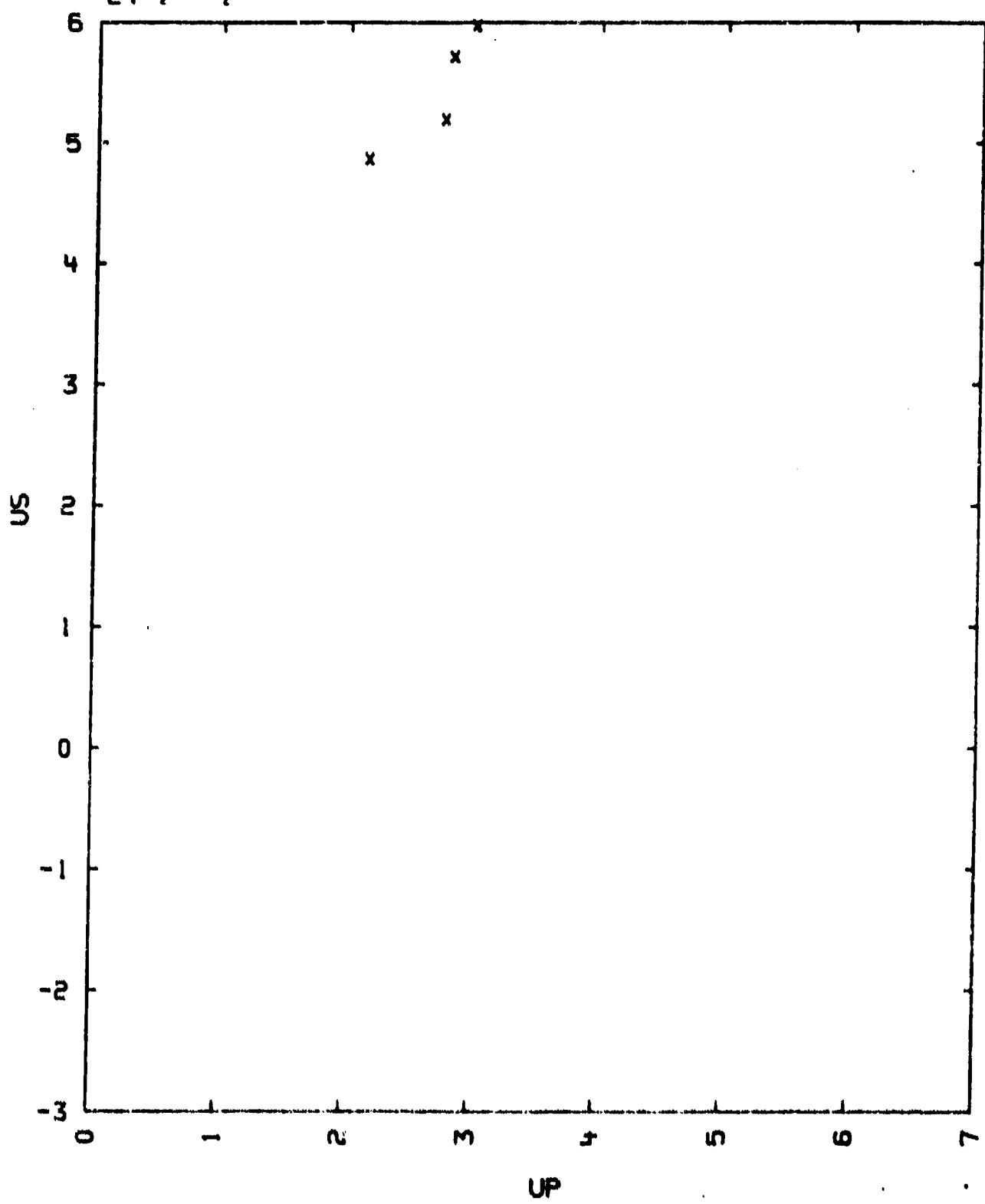


TABLE III

SANDSTONE COCONINO
24-1---1



24-1---2
SILICA (SAND)

SILICON DIOXIDE SI-02 100 PERCENT
PARTICLE SIZE LESS THAN .075 MM. 1. PERCENT. TO .15 MM MAXIMUM
POROSITY 41 PERCENT

$$V_0 = 0.633 \text{ CC}/\text{O}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN MM/MICRO-SEC., AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UP	P	V/V0
1.58	3.13	1.17	58	.626
1.58	3.23	1.18	59	.641
1.58	3.42	1.61	88	.529
1.58	3.47	1.70	93	.510
1.56	4.26	2.25	150	.472
1.62	4.27	2.23	153	.474

$$US = 1.9 + 1.02 UP \text{ KM/SEC.} \quad SIG.US = 0.14 \text{ KM/SEC.}$$

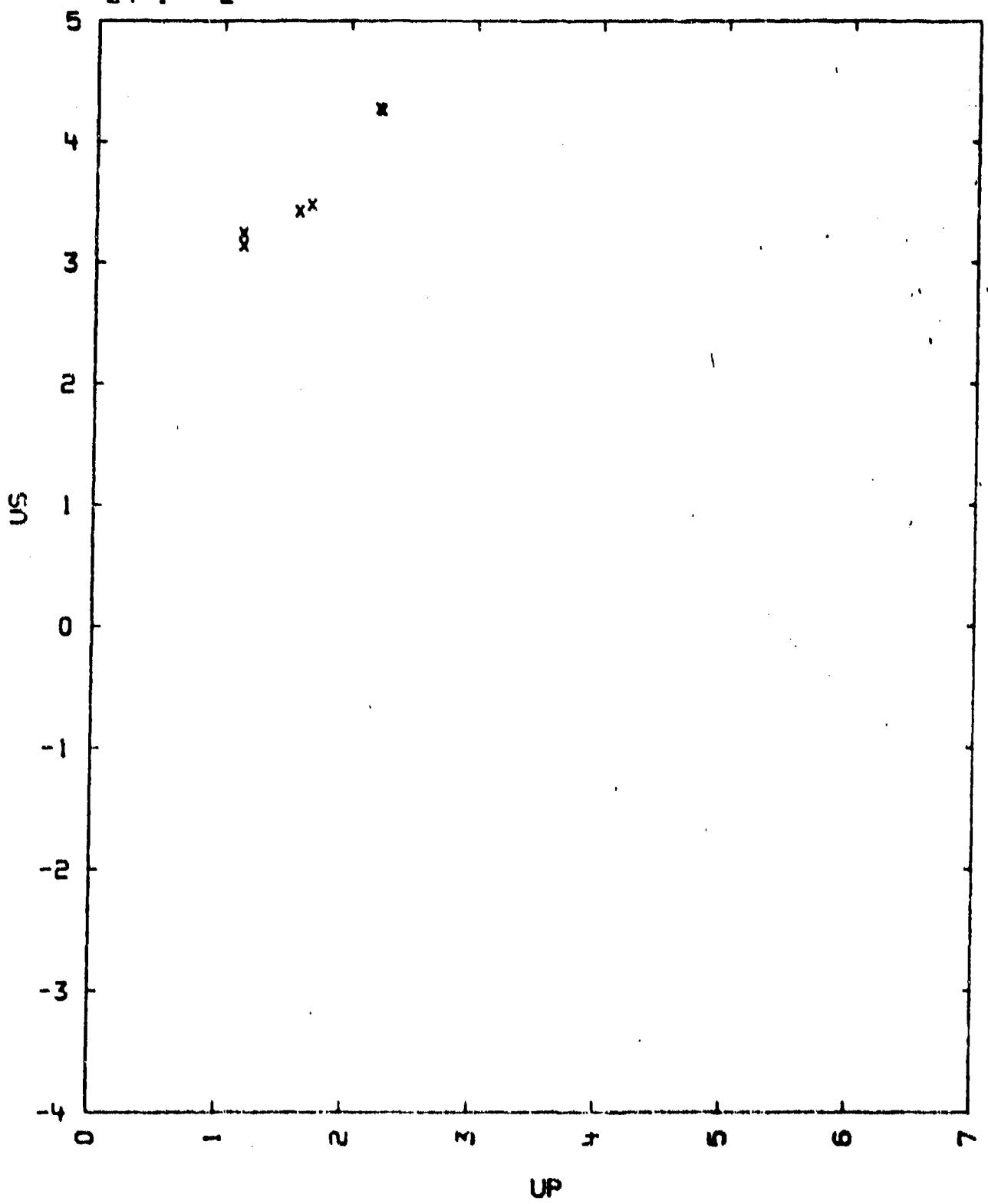
COMMENTS:

- 1) SOURCE: RASS, R.C., HAWK, H.L. AND CHABAI, A.J.
REPORT NO. SC-4903 RR (1963)
SANDIA CORPORATION, ALBUQUERQUE, N. M.
- 2) EXPERIMENTAL TECHNIQUE A
DATA REDUCTION TECHNIQUE B
TECHNIQUE USED FERRO ELECTRIC TRANSDUCERS TO MEASURE THE ARRIVAL OF SHOCK WAVES AT SAMPLE AND DRIVER PLATE SURFACES.
- 3) THE INTERFACE WAS MATCHED WITH THE ALUMINUM HUGONIOT REFLECTED IN THE PRESSURE - MASS VELOCITY PLANE.

TABLE I

SILICA (SAND)

24-1---2



24-1---3
SILICA (SAND)

SILICON DIOXIDE SI-02 100 PERCENT
PARTICLE SIZE: LESS THAN 0.075 MM - 80 PERCENT, TO 0.15 MM MAXIMUM.
POROSITY 22 PERCENT

$$V_0 = 0.481 \text{ CC}/\text{O}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICRO-SEC., AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UP	P	V/V0
2.02	3.45	1.07	75	.690
2.14	3.70	1.48	116	.605
2.03	4.78	2.03	197	.575

$$US = 1.0 + 1.42 UP \text{ KM/SEC.} \quad SIG.US = 0.24 \text{ KM/SEC.}$$

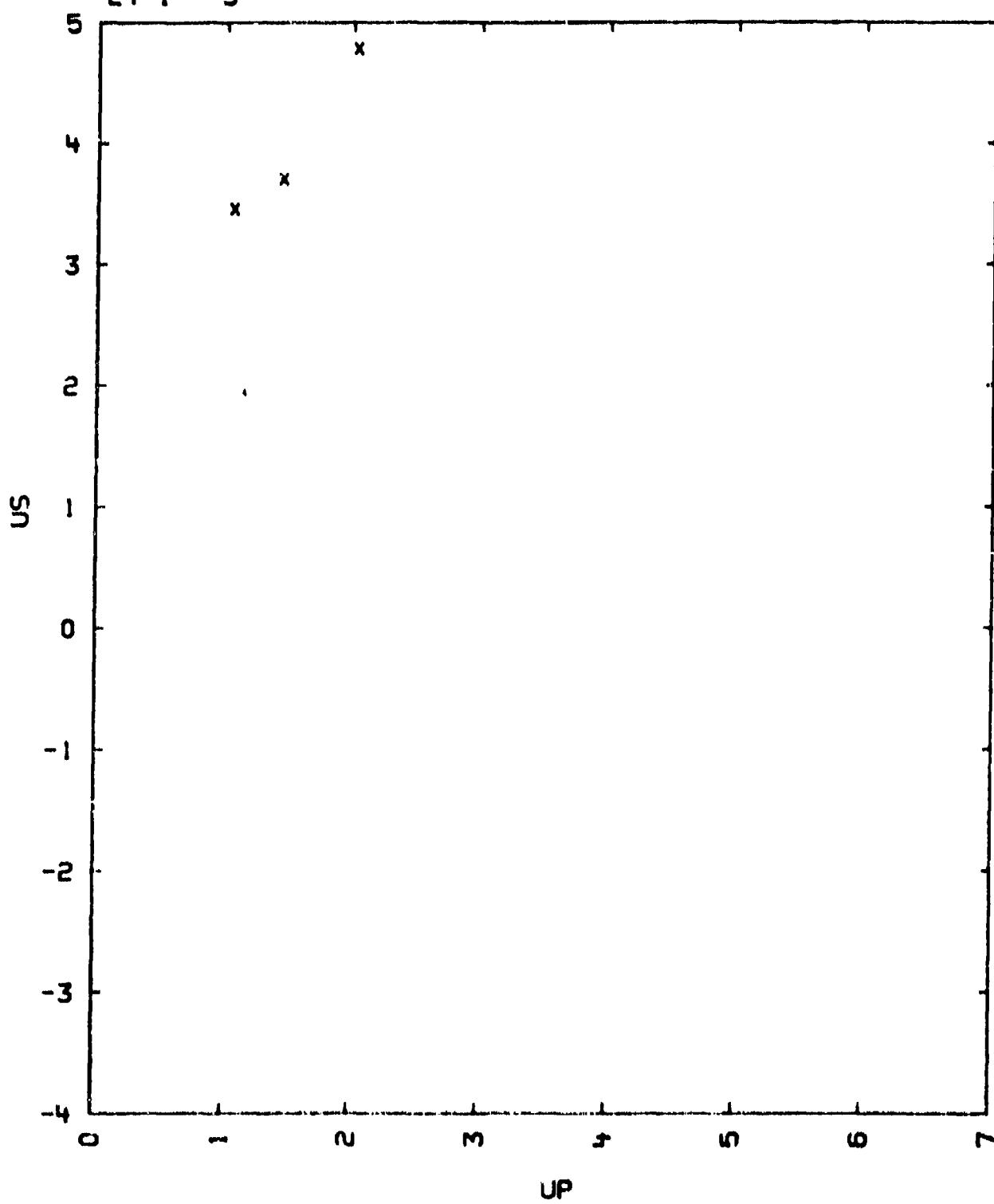
COMMENTS:

- 1) SOURCE: BASS, R.C., HAWK, H.L. AND CHABAI, A.J.
REPORT NO SC-4903 RR (1963)
SANDIA CORPORATION, ALBUQUERQUE, N. M.
- 2) EXPERIMENTAL TECHNIQUE A
DATA REDUCTION TECHNIQUE B
TECHNIQUE USED FERROELECTRIC TRANSDUCERS TO MEASURE THE ARRIVAL OF SHOCK WAVES AT SAMPLE AND DRIVER PLATE SURFACES.
- 3) THE INTERFACE HAS MATCHED WITH THE ALUMINUM HUGONIOT REFLECTED IN THE PRESSURE - MASS VELOCITY PLANE.

TABLE I

SILICA (SAND)

24-1---3



24-1--4
QUARTZ CRYSTAL

51-02

$V_0 = 0.377 \text{ CC}/\text{O}$
 $V_{01} = 0.3774 \text{ CC}/\text{O}$

CL (COMMENT 0) $C_D = 3.69 \text{ KM}/\text{SEC}$

IN TABLE I BELOW, DENSITY IS GIVEN IN G/CC., AND VELOCITIES IN KM/SEC.
FOR EXPLANATION OF DIFFERENT UP1 VALUES SEE COMMENTS. CUT DESIGNATES
THE CRYSTAL AXIS PERPENDICULAR TO THE SHOCK FRONT. ID IS FOR
IDENTIFICATION BETWEEN THE TABLES.

IN TABLE II, PRESSURES ARE GIVEN IN KILOGARS AND VELOCITY IN KM/SEC.,
SI DESIGNATES THE STANDARD MATERIAL PI IS THE PRESSURE JUST AHEAD OF
WAVE 2. PL = PLEXIGLAS.

TABLE I

ID	ρ_{H00}	US1	UP1 MAX.	UP1 MIN.	UP1 AV.	US2	UP2	UFS2	CUT
1	2.65	5.89	0.33	0.275	0.285				X
2	-	5.92	0.34	0.275	0.29				-
3	-	5.93	0.37	0.29	0.32	2.88	0.43	0.84	-
4	-	6.00	0.40	0.34	0.36	4.74	0.67	1.32	-
5	-	6.01	0.41	0.35	0.37	5.11	0.85		-
6	-	6.07	0.44	0.40	0.415	5.24	0.92		-
7	-	6.10		0.44		5.64	1.24		-
8	-	6.12	0.52	0.48	0.50	5.69	1.69		-
9	-	5.89	0.31	0.275	0.285				-
10	-	5.94	0.34	0.285	0.305	5.14	0.82		-
11	-	5.96	0.41	0.39	0.40	5.61	1.21	1.27	-
12	-	6.03		0.39		4.74	0.71	2.20	-
13	-	6.04		0.36		5.18	0.81		-
14	-	6.1		0.45		5.61	1.26		-
15	-	6.21		0.57		5.76	1.82		-
16	-			0.61		6.12	2.55		-
17	-					6.29	2.70		-
18	-					6.66	2.89		-
19	-					6.95	3.03		-
20	-					7.70	3.52		-
21	-					7.83	3.50		-
22	-	6.19	0.49	0.44	0.455	4.85	0.86		Y
23	-	6.17	0.50	0.46	0.48	4.88	0.86		-
24	-	6.24	0.60	0.58	0.59	5.47	1.25		-
25	-	6.26	0.66	0.64	0.65	5.61	1.71		-
26	-	6.12		0.60		5.88	1.30		-
27	-					6.66	2.89		-
28	-					6.95	3.03		-
29	2.65					7.72	3.50		Y
30	-					7.75	3.52		-
31	-	6.82	0.31	0.29	0.295				Z
32	-	6.07	0.39	0.34	0.35				-
33	-	7.23	0.68	0.60	0.625				-
34	-	7.21	0.64	0.57	0.59	3.68	1.83		-
35	-	7.54	0.71	0.565	0.595	4.71	1.23		-

QUARTZ CRYSTAL

ID	RHO0	US1	UP1	UP1	UP1	US2	UP2	UFSE2	CUT
36	-	7.51	0.73	0.71	0.72				-
37	-					7.76	3.42		-
38	-					7.76	3.49		-

US = A + B*UP KM/SEC

FITS OF US1 VERSUS UP1 (MAX) ALONG THE PRINCIPLE AXES

	X	Y	Z
A	5.61	6.01	6.38
SIG A	0.04	0.07	0.10
B	0.89	0.32	1.36
SIG B	0.09	0.13	0.16

FITS OF US2 VERSUS UP2 X AND Y DIRECTION COMBINED

	UP<1	1<UP<2	UP>2
A	1.31	5.36	1.83
B	4.47	0.19	1.67
SIG US	0.13	0.07	0.04

FOR UP2 GREATER THAN 2 KM/SEC.

TABLE II

-----SAMPLE----- STANDARD-----

ID	P1	V1/V0	P2	V2/V0	UP(S1)	P(ST1)	ST
1	43	0.953			0.790	36.4	PL
2	43	0.954			0.790	36.4	PL
3	48	0.951	56	0.900	0.790	36.4	PL
4	54	0.942	94	0.869	0.644	112	AL
5	56	0.942	126	0.842	0.818	147	AL
6	64	0.934	135	0.829	0.906	166	AL
7	71	0.928	189	0.785	1.176	227	AL
8	78	0.922	269	0.707	1.580	329	AL
9	43	0.953			0.644	112	AL
10	45	0.952	116	0.847	0.818	147	AL
11	62	0.935	184	0.788	1.176	227	AL
12	56	0.942	99	0.863	0.644	112	AL
13	58	0.940	152	0.837	0.818	147	AL
14	73	0.926	200	0.770	1.176	227	AL
15	94	0.908	277	0.690	1.580	329	AL
16		414	0.935	2.218	515		AL
17		490	0.971	2.218	515		AL
18		511	0.968	2.34	620		AL
19		550	0.934	2.88	660		AL
20		700	0.930	3.18	850		AL
21		721	0.940	3.18	850		AL
22	72	0.929	126	0.841	0.818	147	AL
23	79	0.925	126	0.843	0.818	147	AL
24	95	0.907	190	0.783	1.176	227	AL
25	108	0.899	263	0.705	1.580	329	AL

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26	97	0.902	198	0.773	1.176	227	AL
27			511	0.568	2.54	620	AL
28			558	0.564	2.66	660	AL
29			725	0.546	3.18	850	AL
30			714	0.548	3.18	850	AL
31	52	0.958			0.680	29.8	PL
32	62	0.951			0.790	38.4	PL
33	115	0.917			0.644	112	AL
34	109	0.921	130	0.844	0.818	147	AL
35	139	0.908	196	0.783	1.176	227	AL
36	141	0.906			1.580	329	AL
37			703	0.550	3.18	850	AL
38			718	0.550	3.18	850	AL

COMMENTS:

- 1) SOURCE: HACKERLE, J.
JOURNAL OF APPLIED PHYS., VOL. 33, P. 922, (1962)
- 2) EXPERIMENTAL TECHNIQUES B AND E.
DATA REDUCTION TECHNIQUE D, FOR THE FIRST HAVE, ASSUMING $U_{P1} = U_{FS}$,
FOR THE SECOND HAVE TECHNIQUE B HAS USED.
STANDARD MATERIALS ALUMINUM 2024 ALLOY AND PLEXIGLAS (PL IN TABLE).
- 3) THE ESTIMATED EXPERIMENTAL PRECISION IN U_{FS} AND UP RANGES FROM 2-4 PERCENT.
ESTIMATED EXPERIMENTAL ERROR IN THE USI MEASUREMENT IS 0.5 PERCENT
AND FOR U_{S2} IT IS 1.0 PERCENT.
- 4) U_{FS1} ATTENUATED EXPONENTIALLY IN TIME: $U_{P1}(\text{MAX})$ IS HALF OF THE INITIAL JUMP OFF VELOCITY, $U_{P1}(\text{MIN})$ IS HALF OF THE FINAL VELOCITY JUST BEFORE ARRIVAL OF THE 2ND. WAVE AT THE SURFACE,
 $U_{P1}(\text{AV})$ IS THE TIME AVERAGE VALUE.
USI IS THE VELOCITY OF THE ATTENUATING WAVE ON ARRIVAL AT THE FREE SURFACE AND HAS BEEN USED AS SUCH IN THE CALCULATION OF P_1 AND P_2 .
 $U_{P1}(\text{MIN})$ IS USED IN CALCULATING P_1 AND P_2 .
- 5) V_{O1} HAS CALCULATED USING THE LATTICE CONSTANTS $A = 4.91267$ AND $C = 5.40459$ ANGSTROMS, OBTAINED FROM A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION, POLYCRYSTAL BOOK SERVICE 1963) 2ND. ED.
- 6) AN ESTIMATE HAS MADE OF THE HUGONIOT OF THE HIGH PRESSURE STISHOVITE PHASE OF QUARTZ. A HYPOTHETICAL STISHOVITE SAMPLE WITH A DENSITY OF 4.35 G/CC AT $P = 0$ HAS THE HUGONIOT EQUATION
 $US = 10 + 1.0 \cdot UP$ KM/SEC
MCQUEEN, R.O., FRITZ, J.N. AND MARSH, S.P.
JOURNAL OF GEOPHYSICAL RESEARCH, VOL. 68, P. 2319, (1963)
- 7) USING THE PIEZOELECTRIC RESPONSE OF X-CUT QUARTZ GRAHAM OBTAINED THE FOLLOWING STATISTICAL FIT OF THE SHOCK SPEED
 $US = A + B \cdot UP$ WITH $A = 5.728$ •OR• 0.018 KM/SEC
AND $B = 0.312$ •OR• 0.112 FOR $UP < 1$
R.A.GRAHAM, PHYS. REV., V. B6 (12), P. 4779, (1972)
- 8) LONGITUDINAL VELOCITIES PARALLEL AND PERPENDICULAR TO THE A AXIS ARE RESP 6.36 AND 5.78 KM/SEC AT 1 BAR AND 6.63 AND 6.21 AT 15 KBAR.
G.D. AFANAS'YEV AND YE.I. BAYUK ET ALL, DOKLADY, GEOPHYSICS VOL. 201, P. 27, (1973)

TABLE I

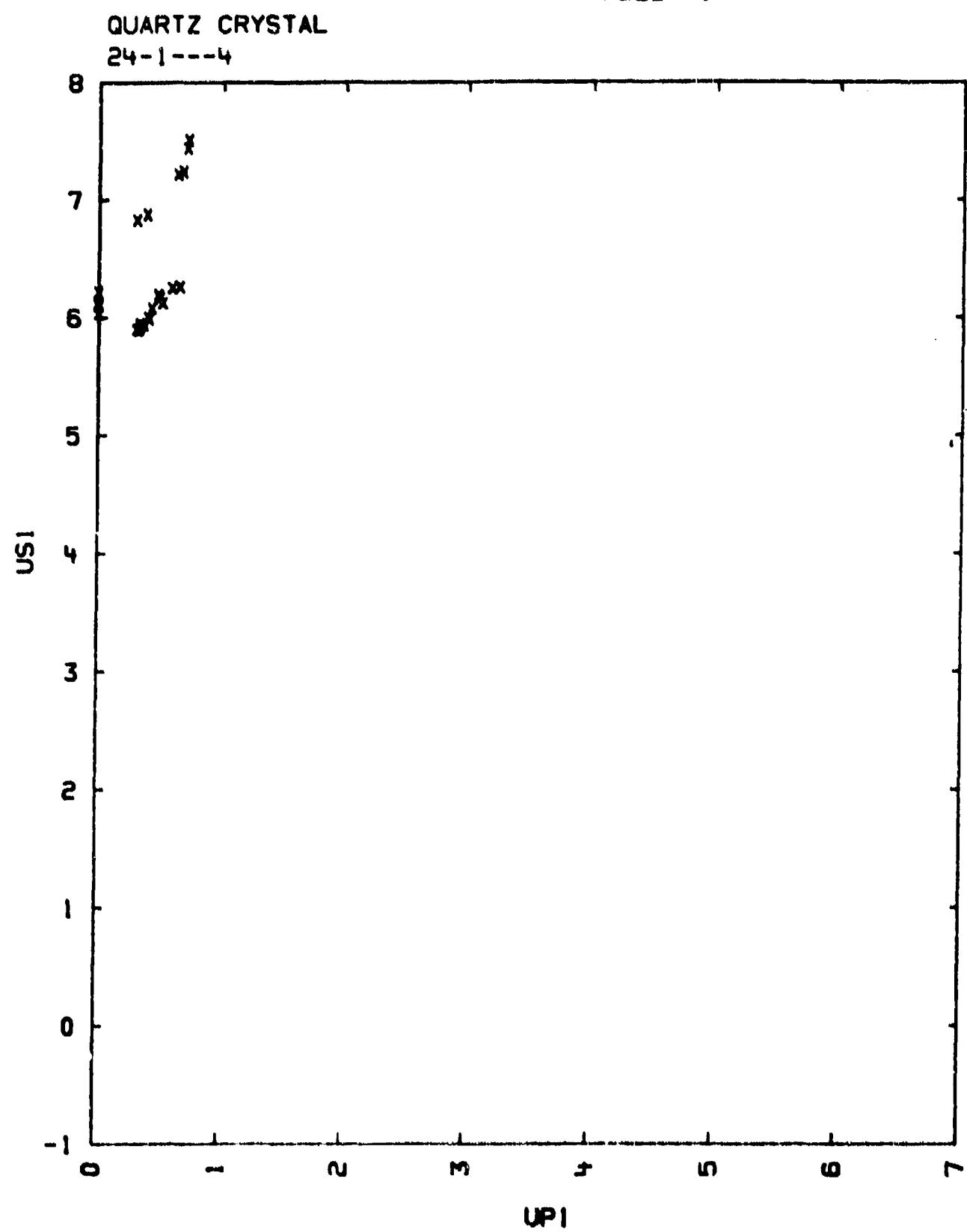
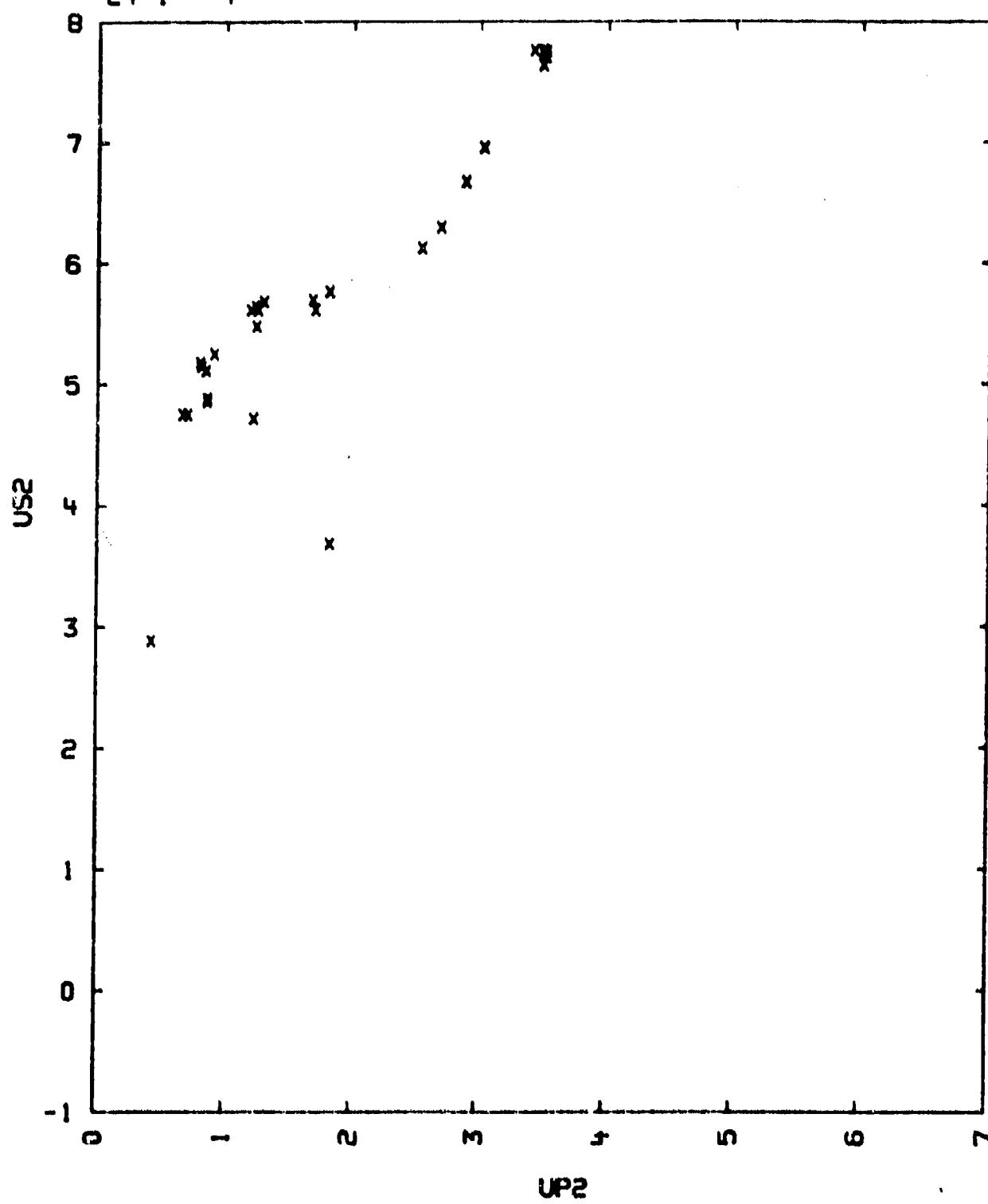


TABLE I

QUARTZ CRYSTAL

24-1---4



24-1---5
QUARTZ, FUSED

SI-02

$$V_0 = 0.4537 \text{ CC/O.} \quad C_L = 5.958 \text{ KM/SEC.} \quad C_D = 4.09 \text{ KM/SEC.}$$

$$V_{01} = 0.3774 \text{ CC/O.} \quad C_S = 3.784 \text{ KM/SEC.}$$

IN TABLE I BELOW, DENSITY IS GIVEN IN G/CC. AND VELOCITIES IN KM/SEC.
ID IS FOR IDENTIFICATION BETWEEN THE TABLES.

IN TABLE II, PRESSURES ARE GIVEN IN KILOBARS AND VELOCITY IN KM/SEC.,
SI DESIGNATES THE STANDARD MATERIAL.

TABLE I

ID	RHO0	US1	UP1	UFS1	US2	UP2	UFS2
0	2.204	5.890	0.000	0.000			
1	-	5.751	0.037	0.074			
2	-	5.624	0.076	0.152			
3	-	5.503	0.120	0.240			
4	-	5.387	0.174	0.348			
5	-	5.275	0.235	0.470			
6	-	5.168	0.306	0.612			
7	-	5.15	0.40	0.80			
8	-	5.17	0.49	0.98			
9	-	5.22	0.74	1.49			
10	-	5.25	0.81	1.63			
11	-	5.17	0.82	1.64			
12	-	5.20	0.83	1.67	4.52	1.04	1.74
13	-	5.23	0.84	1.68	4.67	1.40	1.98
14	-	5.20	0.85		4.70	1.41	
15	-	5.20	0.89	1.78	4.97	1.90	3.04
16	-	5.23	0.86	1.74	4.96	1.95	3.09
17	-				5.62	2.76	4.12
18	-				5.53	2.78	4.11
19	-				5.62	2.78	
20	-				8.43	3.29	
21	-				8.44	3.33	
22	-				7.28	3.01	6.39
23	-				7.30	3.07	

US1 = $5.76 - 2.14 \text{ UP KM/SEC.}$ FOR UP FROM 0.0 TO 0.4 KM/SEC.

US1 = $5.07 + 0.183 \text{ UP KM/SEC.}$ FOR UP FROM 0.4 TO 0.9 KM/SEC.

US2 = $4.03 + 0.477 \text{ UP KM/SEC.}$ FOR UP FROM 1.0 TO 1.9 KM/SEC.

US2 = $1.30 + 1.58 \text{ UP KM/SEC.}$ FOR UP FROM 2.5 TO 3.8 KM/SEC.

TABLE II

-----SAMPLE----- -----STANDARD-----

ID PI V/V01 P2 V/V02 UP(S1) P(S1) S1

0	0.00	1.000					
1	4.69	0.9936					
2	9.42	0.9855					
3	14.55	0.9782					
4	20.66	0.9677					
5	27.32	0.9555					
6	34.85	0.9408					
7	45.4	0.922		0.580	29.8	PL	
8	55.8	0.905		0.790	35.4	PL	
9	65.6	0.887		0.844	112	AL	
10	94.3	0.845		0.810	147	AL	
11	93.4	0.842		0.810	147	AL	
12	95.7	0.839	117	0.791	0.906	166	AL
13	96.0	0.839	153	0.717	1.176	227	AL
14	96.0	0.836	157	0.716	1.176	227	AL
15	102.0	0.829	211	0.624	1.580	329	AL
16	99.1	0.836	217	0.614	1.580	329	AL
17			342	0.509	2.218	515	AL
18			337	0.501	2.218	515	AL
19			346	0.512	2.218	515	AL
20			460	0.495	2.66	660	AL
21			482	0.484	2.66	660	AL
22			611	0.477	3.18	850	AL
23			623	0.470	3.18	850	AL

COMMENTS:

- 1) SOURCE: WACKERLE, J.
JOURNAL OF APPLIED PHYS., VOL. 33, P. 922, (1962)
- 2) EXPERIMENTAL TECHNIQUE E FOR ID = 0-17 AND B FOR THE REST.
DATA REDUCTION TECHNIQUE D, USED FOR THE FIRST-HAVE, ASSUMING
PUP= UPS. FOR THE SECOND-HAVE TECHNIQUE B, HAS USED.
STANDARD MATERIALS ALUMINUM 2024 AND PLEXIGLASS (PL IN TABLE).
- 3) VOI HAS CALCULATED FROM THE LATTICE CONSTANTS A = 4.91287 AND
C = 5.40459 ANGSTROMS; A.C.A. MONOGRAPH NUMBER 5 (AMERICAN
CRYSTALLOGRAPHIC ASSOCIATION, POLYCRYSTAL BOOK SERVICE, BROOKLYN,
N.Y., 1963) 2ND ED.
- 4) CL HAS VERIFIED EXPERIMENTALLY FOR THE SAMPLES USED. CL AND CS WERE
OBTAINED FROM GARY, D. H., (AMERICAN INSTITUTE OF PHYSICS HANDBOOK,
MCGRAW-HILL BOOK CO. INC., NEW YORK, 1957).
- 5) THE FIRST SHOCK VERSUS PARTICLE VELOCITY FIT IS NOT THAT OF A STEP
FUNCTION BUT DEFINES A PRESSURE RAMP AHEAD OF ALL THE HIGHER PRESSURE
WAVES. BETWEEN UP = 1.0 TO 1.9 KM/SEC THE MATERIAL IS IN THE
TWO PHASE REGION AND ABOVE 1.9 KM/SEC IN THE STISHOVITE PHASE.
THE MOST COMPLETE SHOCK STRUCTURE REPRESENTED BY THE ABOVE DATA IS A
RAMP FOLLOWED BY TWO PRESSURE STEPS.
- 6) THE FOLLOWING FUSED QUARTZ CURVE
 $P = 776.0 \cdot EPS - 4159 \cdot EPS^{0.2} + 30340 \cdot EPS^{0.3} - 89260 \cdot EPS^{0.4}$
 $P = 131.7 \cdot UP - 73.61 \cdot UP^{0.2} + 29.47 \cdot UP^{0.3} - 41.63 \cdot UP^{0.4}$
 REPORTED BY BARKER, L. M. AND HOLLOWBACH, J. APPL. PHYS. 41 4208 70
 FITS THE HUGONIOT UP TO 65 KBAR AND RELEASE CURVES FROM P = 37 KBAR
 AND BELOW.

TABLE I

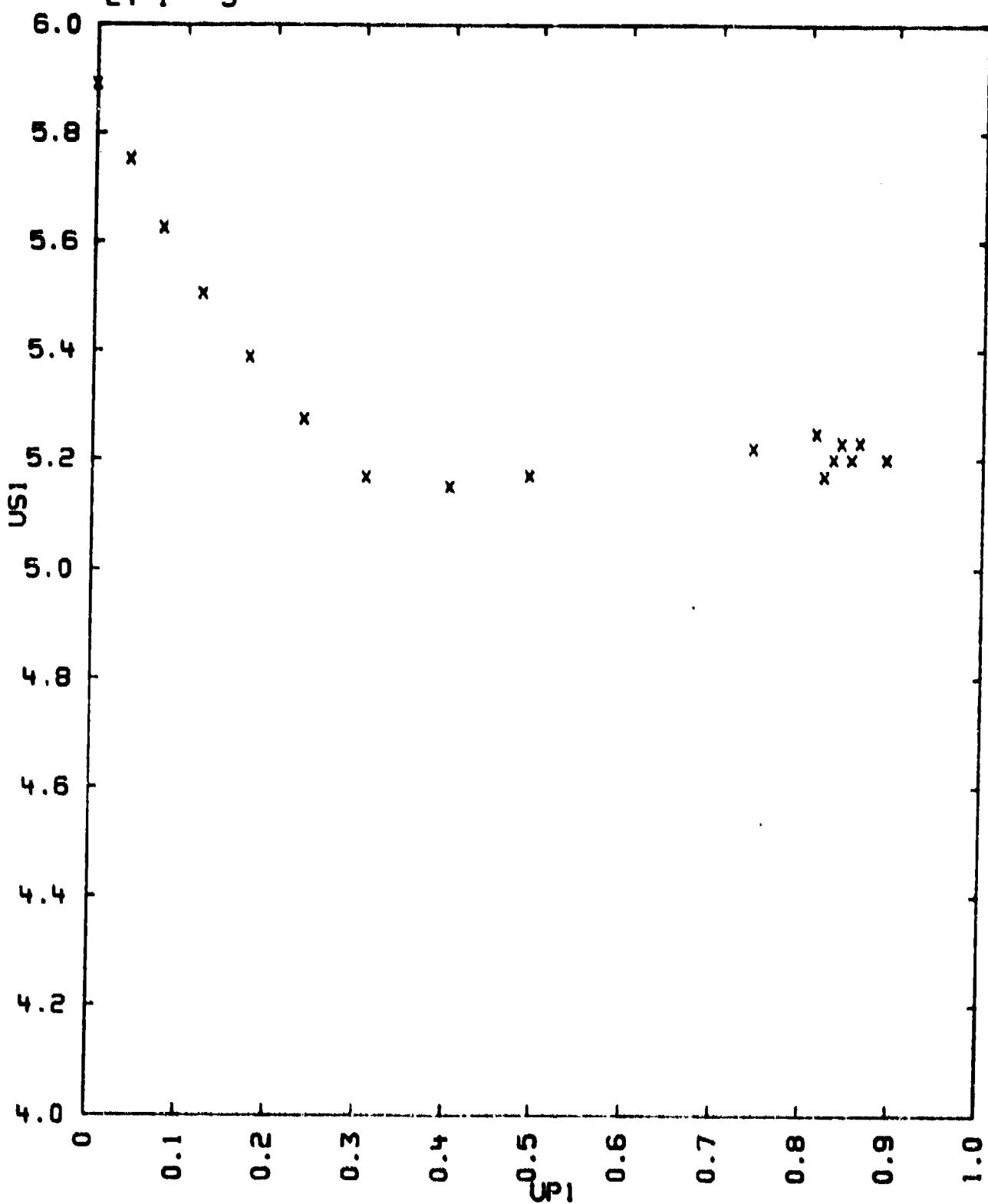
QUARTZ, FUSED
24-1---5

TABLE I

QUARTZ, FUSED
24-1---5

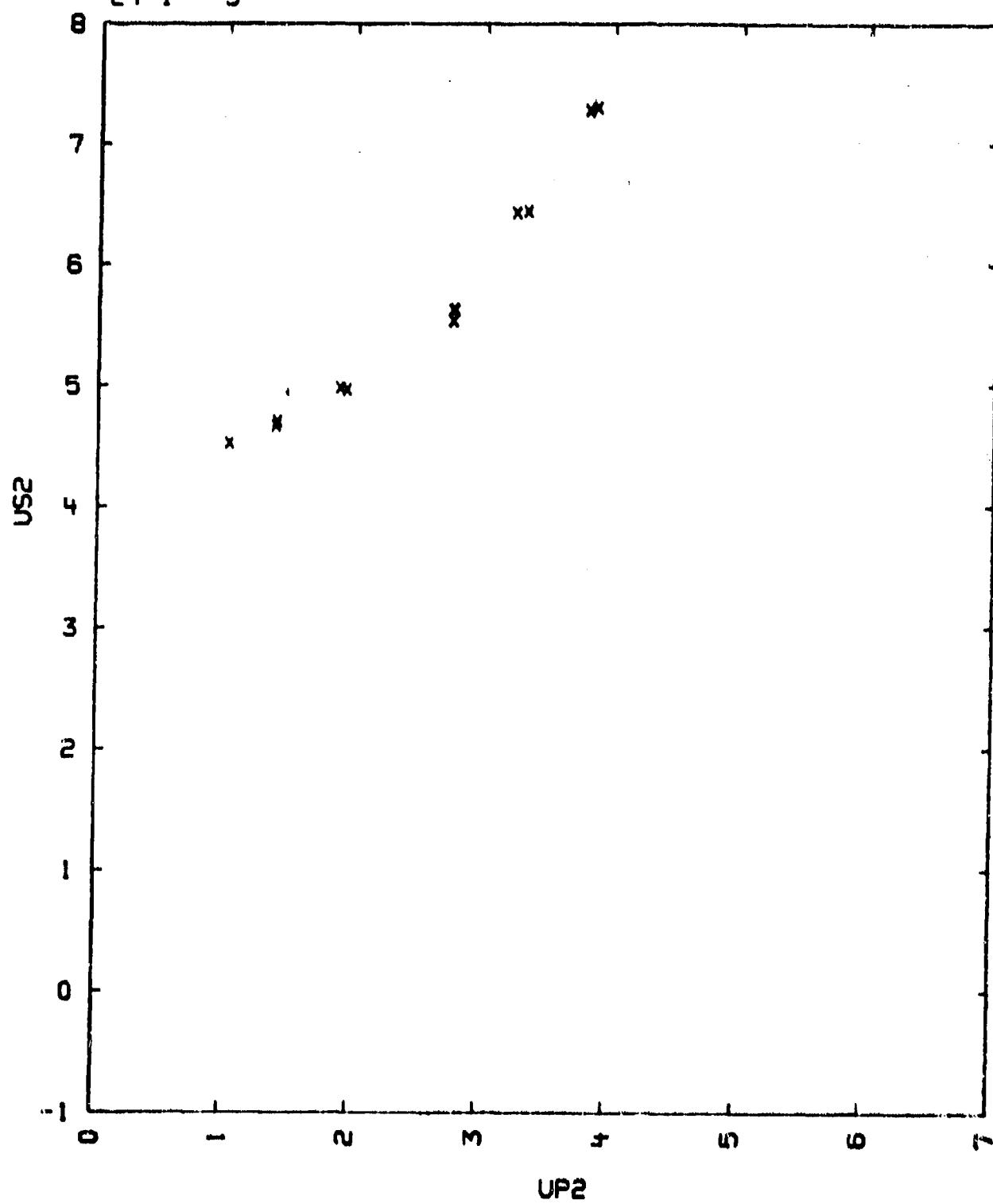
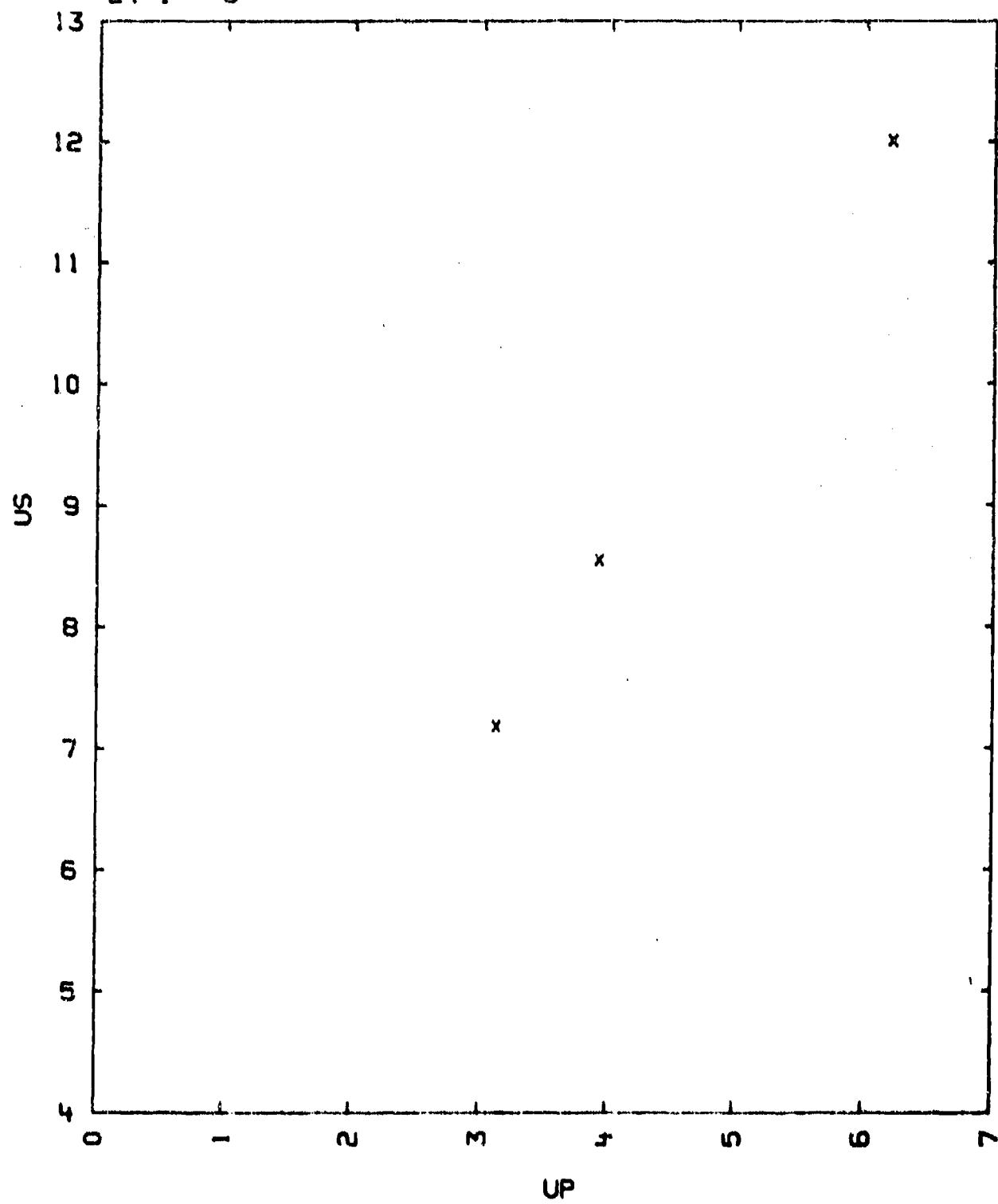


TABLE I

QUARTZ CRYSTAL (SILICON DIOXIDE)

24-1---6



24-1---8

QUARTZ CRYSTAL (SILICON DIOXIDE)

SI-02

 $\rho_0 = 0.3774 \text{ CC/G}$ $\rho_{01} = 0.3774 \text{ CC/G}$

THE TABLE LISTS DENSITIES IN G/CC., VELOCITIES IN KM/SEC AND PRESSURE IN KBARS.

TABLE

ρ_{00}	U_S	U_P	P	V/V_0
2.65	7.18	3.13	595	0.584
-	8.54	3.92	887	0.541
-	12.01	6.2	1974	0.484

 $U_S = 2.35 + 1.56 U_P \text{ KM/SEC}$ $\Sigma \Delta U_S = 0.092 \text{ KM/SEC}$

COMMENTS:

- 1) SOURCE: AL'TSHULER, L. V., TRUNIN, R. F., SIMAKOV, O. V.
IZV. AKADEMII NAUK SSSR. FIZIKA ZEMLI NO. 10, 1965, P. 1-6
- 2) EXPERIMENTAL TECHNIQUE: NOT REPORTED
DATA REDUCTION METHOD: NOT REPORTED
- 3) ρ_{01} WAS OBTAINED FROM THE HEXAGONAL LATTICE PARAMETERS $A = 4.91265$ AND $C = 5.40441$ ANGSTROM.: CRYSTAL DATA DETERMINATIVE TABLES, MONOGRAPH 5 (AMERICAN CRYST. ASSN., JOHN WILEY AND SONS, 1963) 2ND ED.
- 4) TWO ISOTHERMS FOR THE HIGH DENSITY FORM OF QUARTZ (STISHOVITE) AT 0 AND 4000 DEG. K WERE CALCULATED WITH A GRUNEISEN GAMMA = 0.9 AND THE MCQUEEN METHOD OF CALCULATING THE STISHOVITE HUGONIOT:
MCQUEEN FRITZ AND MARSH, J. GEOPHYS. RES., VOL. 68, P. 2319 (1963)

P	$\rho_{01}(0)$	$\rho_{01}(0 \text{ DEG. K})$	$\rho_{01}(4000 \text{ DEG. K})$
0	4.35	4.35	4.28
20	4.335	4.335	4.48
40	4.708	4.710	4.85
60	4.87	4.872	4.81
80	5.03	5.033	4.975
100	5.18	5.19	5.13
120	5.33	5.34	5.278
140	5.47	5.483	5.42
160	5.61	5.63	5.565
180	5.74	5.77	5.705
200	5.87	5.91	5.846
220	6.00	6.053	5.987
240	6.12	6.18	6.123
260	6.25	6.33	6.268

NO PHYSICAL SIGNIFICANCE IS ATTACHED TO THE DISCONTINUITY AT
UP = 1.54 KM/SEC.

- 5) VOI HAS CALCULATED WITH THE HEXAGONAL UNIT CELL CONSTANTS
A=4.91267 AND C=5.40459 ANGSTROMS: A.C.A. MONOGRAPH NO 5 (AMERICAN
CRYST. ASSN., POLYCRYSTAL BOOKSERVICE, N.Y., 1963) 2ND ED.

24-1--7
QUARTZ (SAND)

SI-02 97 PERCENT BY WEIGHT
POROSITY 4.0 PERCENT
GRAIN SIZE LESS THAN 1MM.

$$V_0 = 0.625 \text{ CC/G.}$$

$$V_{01} = 0.3774 \text{ CC/G.}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN KM/SEC., AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UP	P	V/V0
1.60	1.88	0.58	17	0.892
-	1.97	0.57	18	0.711
-	2.22	0.82	29	0.630
-	2.15	0.86	30	0.600
-	2.94	1.07	50	0.636
-	2.98	1.08	51	0.638
-	4.04	1.54	100	0.619
-	4.12	1.54	102	0.620
-	4.07	1.72	112	0.577
-	4.12	1.71	113	0.585
-	4.26	1.76	120	0.586
-	4.70	2.31	175	0.508
-	4.78	2.40	184	0.493
-	5.60	3.21	208	0.427
-	5.91	3.34	216	0.435
-	6.04	3.85	353	0.598
-	6.46	3.88	401	0.599

US = C.441 + 2.33 UP KM/SEC. SIGMA US = 0.16 KM/SEC.
FOR UP RANGING FROM 0.57 TO 1.54 KM/SEC.

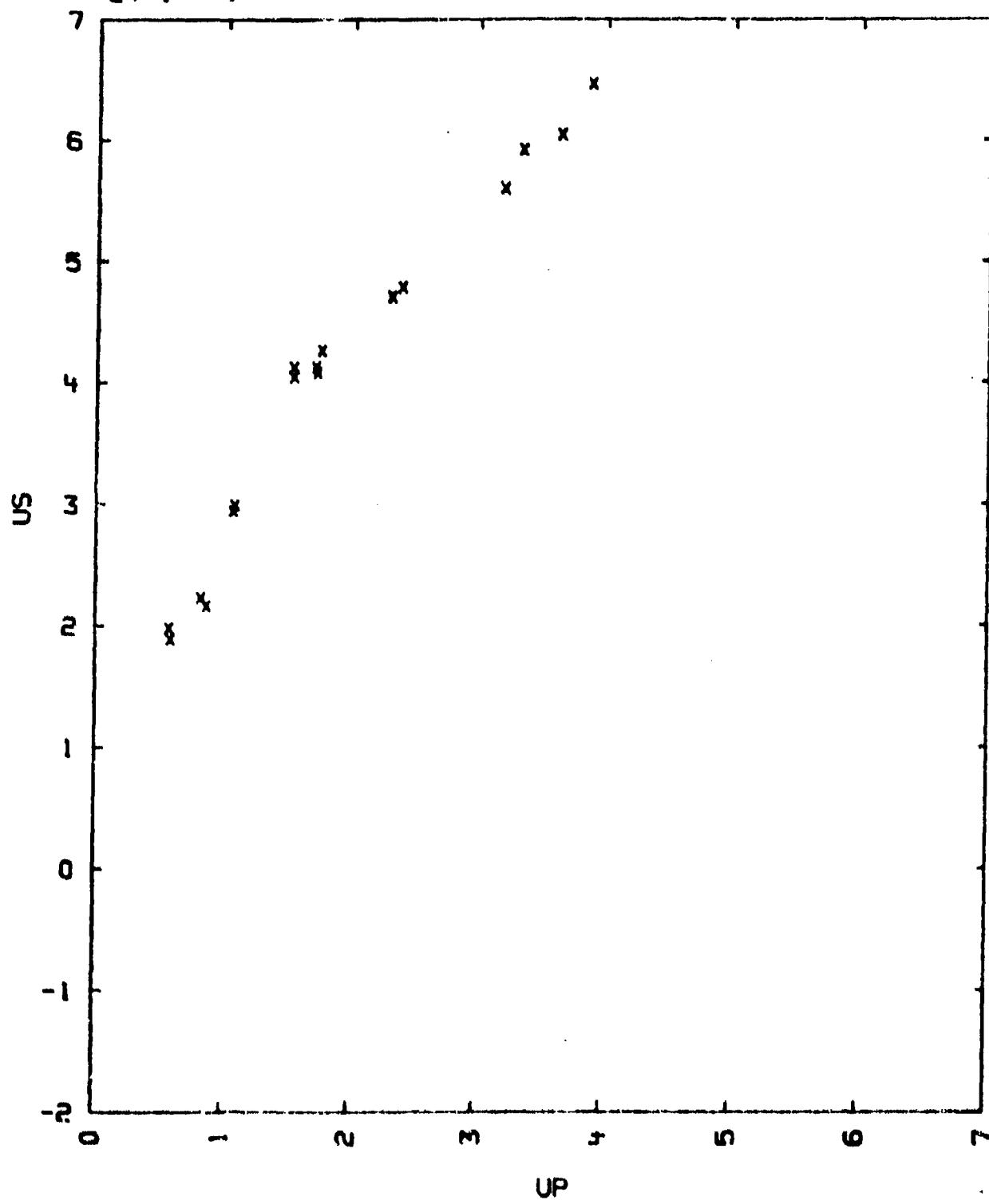
US = 2.32 + 1.04 UP KM/SEC. SIGMA US = 0.08 KM/SEC
FOR UP RANGING FROM 1.72 TO 3.88 KM/SEC.

COMMENTS:

- 1) SOURCE: HART AND SKIDMORE I. C.
PRIVATE COMMUNICATION (1965)
SKIDMORE I. C.
APPLIED MATERIALS RESEARCH, VOL. 4, P. 131, (1965)
- 2) EXPERIMENTAL TECHNIQUE A.
DATA REDUCTION TECHNIQUE B.
ALUMINUM, IRON, AND BRASS WERE USED AS STANDARDS.
- 3) X-RAY DIFFRACTION SHOWED A CLEAR CUT PATTERN OF ALPHA QUARTZ WITH NO OTHER PHASE PRESENT. THE TECHNIQUE IS NOT SENSITIVE TO IMPURITY PHASES OF LESS THAN 5 PERCENT.
- 4) ANOTHER FIT OF THE LOW PRESSURE DATA USING OTHER THEORETICAL CONSIDERATIONS IS: UP = 10.327 * US^{1/11} - 0.0102 * US⁻²¹ KM/SEC.

TABLE I

QUARTZ (SAND)
24-1---7



24-1---8
QUARTZITE

COMPOSITIONS FROM THREE DIFFERENT LOCATIONS

A ARKANSAS NOVACULITE (AN): SI-02 AS QUARTZ ABOUT 100 PERCENT BY VOL.
 PARTICLE SIZE - 0.01 MM.

B SIOUX QUARTZITE (SO): SI-02 AS QUARTZ - 99 PERCENT BY VOL.
 PARTICLE SIZE 0.1 MM
 HEMATITE DUST REMAINDER

C EUREKA QUARTZITE (EO): SI-02 AS QUARTZ ABOUT 99 PERCENT BY VOL.
 SI-02 CEMENT TRACE

$$V_0 = 0.3774 - 0.3788 \text{ CC/G}$$

$$V_{01} = 0.3774 \text{ CC/G}$$

TABLE I LISTS THE SHOCK AND PARTICLE VELOCITIES OF AN ELASTIC AND PLASTIC WAVE IN KM/SEC. SM = SAMPLE MATERIAL: DEFINED ABOVE. STM IS THE STANDARD MATERIAL. TABLE II LISTS THE CORRESPONDING PRESSURES IN KBARS, COMPRESSIONS AND THE SOURCE EXPERIMENT NUMBERS(SNO).

TABLE I

SAMPLE						STANDARD	
NO	SM	US1	UP1	US2	UP2	STM	UF5
1	AN	5.08	0.53	3.12	0.66	AL	1.188
2	-	6.40	0.571	3.07	0.59	AL	
3	-	6.235	0.479				
4	-	6.225	0.449				
5	-	6.190	0.386				
6	-	6.129	0.139				
7	-	5.392	0.204				
8	-	6.112	0.336				
9	-	6.104	0.306				
10	-	6.098	0.262				
11	-	6.091	0.256				
12	-	6.080	0.234				
13	SO			6.20	1.415	AL	
14	-	5.626	0.249	4.081	0.615		
15	-	5.561	0.206	4.029	0.787		
16	-	5.541	0.168	4.729	0.703		
17	-	5.499	0.106	4.620	0.508		
18	-	5.477	0.066	4.546	0.342		
19	EO	5.616	0.233	4.856	0.313		
20	-	5.648	0.319				
21	-	5.671	0.222				
22	-	5.696	0.174				

US -

UOG/14/77

TABLE II

NO	SM	RHO0	P1	V1/V0	P2	V2/V0	SNO
1	AN	2.65	82	0.910	92	0.864	8238
2	-	2.65	95.8	0.9108	132	0.808	8270
3	-	2.642	78.8	0.9232			8300
4	-	-	73.8	0.9292			-
5	-	-	63.1	0.9377			-
6	-	-	21.8	0.9780			-
7	-	2.649	32.4	0.9860			8275
8	-	2.642	54.2	0.9450			8299
9	-	-	49.4	0.9499			-
10	-	-	45.4	0.9538			-
11	-	-	41.2	0.9580			-
12	-	-	37.0	0.9625			-
13	SO	2.64		252	0.772		7693
14	-	2.640	37.0	0.9558	83.8	0.8802	7468
15	-	-	30.2	0.9630	103.8	0.8419	-
16	-	-	24.6	0.9697	91.5	0.8567	-
17	-	-	15.4	0.9817	64.2	0.8943	-
18	-	-	9.5	0.9880	42.5	0.9271	-
19	EO	-	37.5	0.9550			7998
20	-	-	47.8	0.9435			-
21	-	-	33.2	0.9600			-
22	-	-	26.1	0.9695			-

COMMENTS:

1) SOURCE: AHRENS T. J. AND GREGSON JR. V. O.
J. GEOPHYS. RES., VOL. 69, P. 4039 (1964)

2) EXPERIMENTAL TECHNIQUE: C AND D

IN MOST EXPERIMENTS THE INCIDENT WAVE REACHED THE SURFACE AT AN ANGLE AND VARIED IN PRESSURE ALONG THE FRONT, ALLOWING SEVERAL PRESSURE MEASUREMENTS IN A SINGLE EXPERIMENT.

DATA REDUCTION METHOD: B AND D WITH 2UP+UFS.

3) V01 WAS CALCULATED USING THE HEXAGONAL LATTICE CONSTANTS-
 $A=4.91267$ AND $B=5.40459$ ANGSTROM. CRYSTAL DATA DETERMINATIVE TABLES MONOGRAPH 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION, POLYCRYSTAL BOOK SERVICE, BROOKLYN, N.Y., 1963) 2ND ED.

4) ENTRIES 3 TO 7 WERE OBTAINED FROM A SINGLE WEDGE OF QUARTZ AS WERE ENTRIES 8 TO 13, 14 TO 19 AND 19 THROUGH 22.

THE ELASTIC PRECURSOR WAVE 1 SHOWS A YIELD POINT WHICH IS A FUNCTION OF ITS SEPARATION FROM WAVE 2. IN ENTRY NO 14 - 19 UP1 DECREASES AS THE WAVE SEPARATION INCREASES IN THE 2 DIMENSIONAL WEDGE METHOD USED. P2 AND V2/V0 WERE COMPUTED TAKING THE LISTED NUMBERS AS THOSE OF SIMPLE SQUARE PRESSURE STEPS

TABLE I

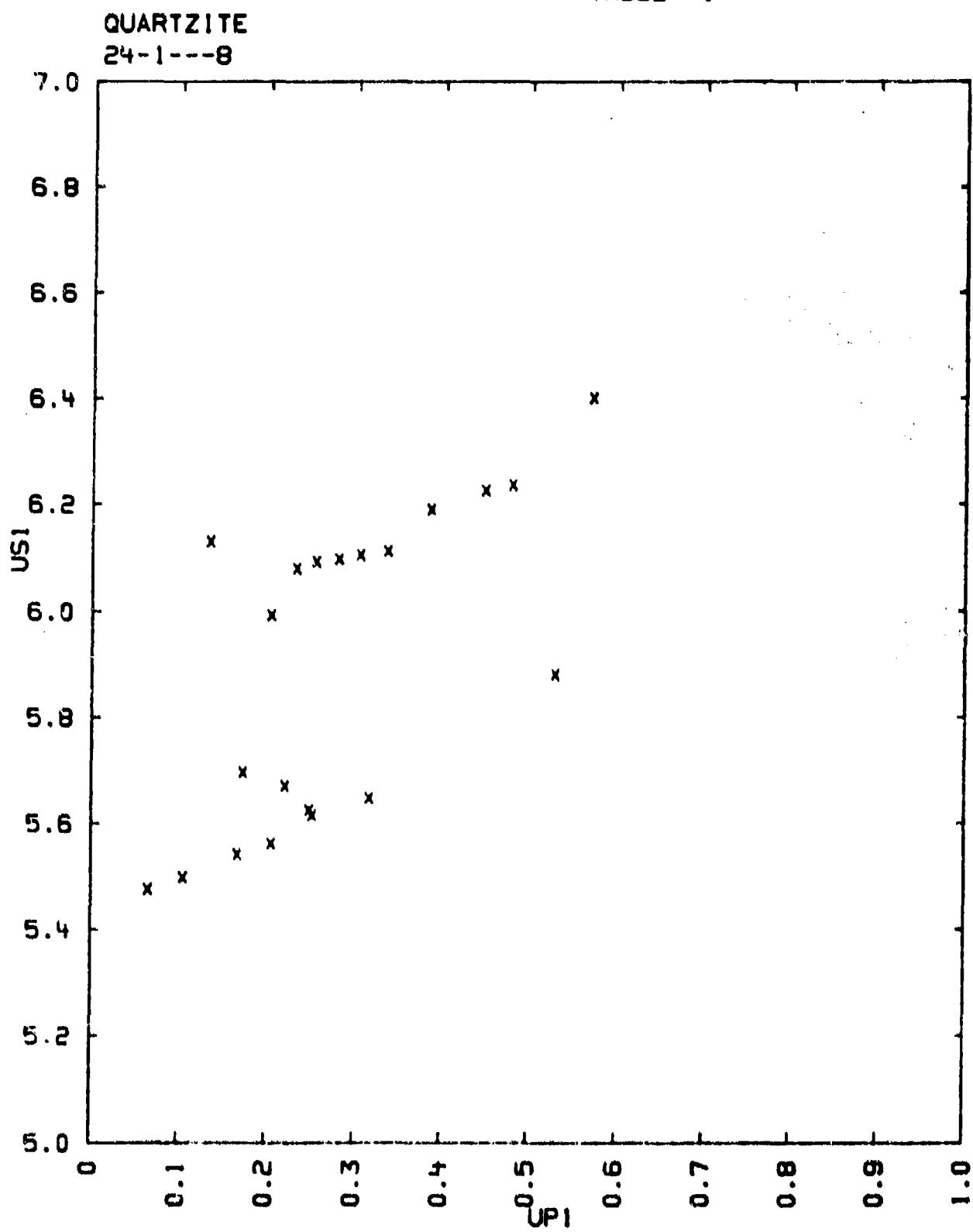
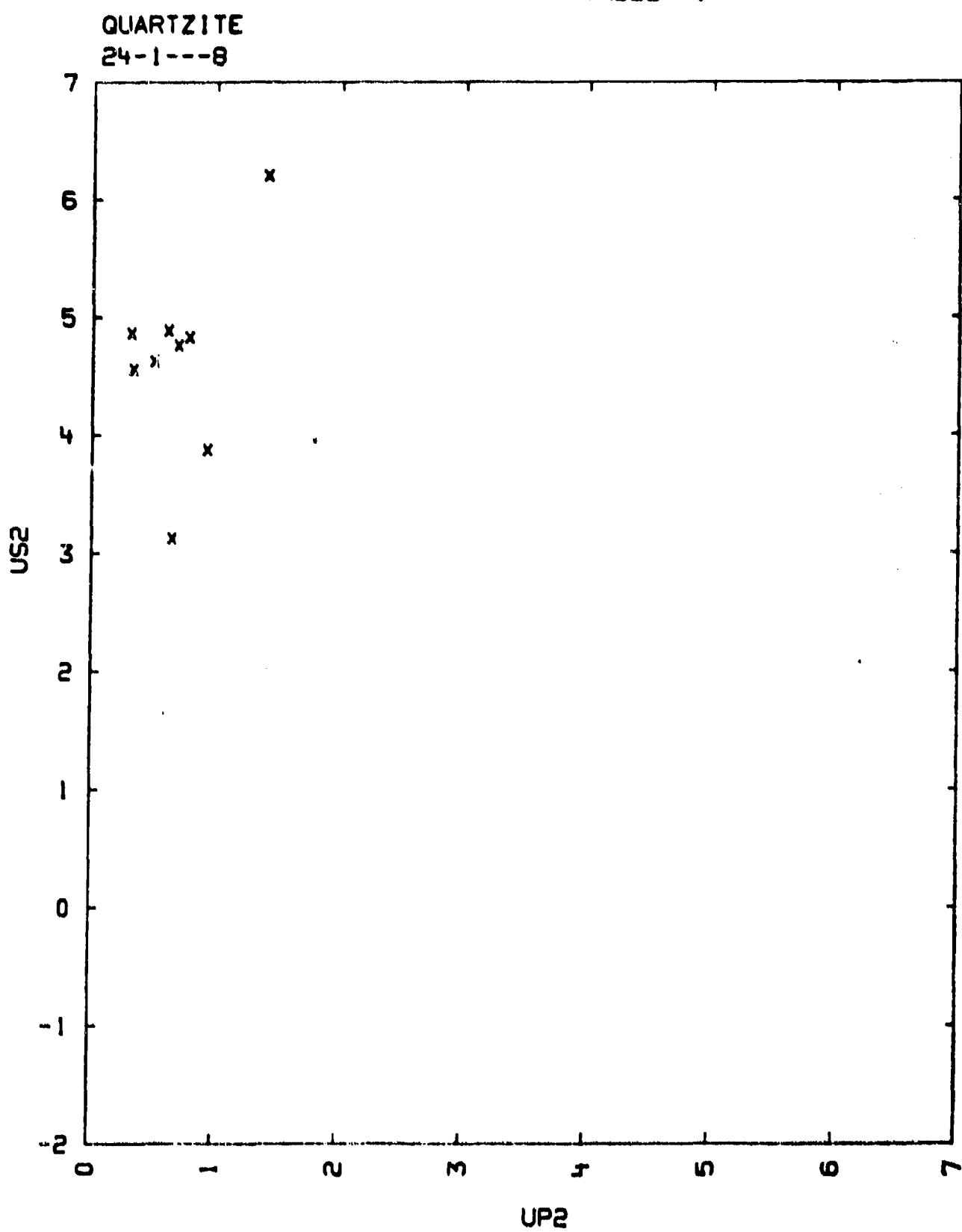


TABLE I



24-1---8
QUARTZITE

ARKANSAS NOVACULITE (AN):	QUARTZ			
SIOUX QUARTZITE (SO):	QUARTZ	ABOUT 100 PERCENT BY VOL.		
	PARTICLE SIZE	- 0.01 MM		
	HEMATITE DUST	- 99 PERCENT BY VOL.		
EUREKA QUARTZITE (EQ):	SI-O2 CEMENT	REMAINDER		
	QUARZ	-		
	SI-O2 CEMENT	ABOUT 99	-	-
		TRACE		

$$V_0 = 0.3774 - 0.3788 \text{ CC}/\text{O}$$

$$V_{01} = 0.3774 \text{ CC}/\text{O}$$

TABLE I GIVES SHOCK VELOCITY AND PARTICLE VELOCITY OF THE ELASTIC AND PLASTIC WAVE IN KM/SEC AS WELL AS FREE SURFACE VELOCITY. D = SAMPLE THICKNESS IN MM. SM = SAMPLE MATERIAL.

TABLE II GIVES CORRESPONDING PRESSURE AND COMPRESSION. VF IS A CALCULATED VOLUME AFTER DECOMPRESSION. INITIAL DENSITY IN G/CC.

TABLE IA

SAMPLE								STANDARD
NO	SM	US1	UP1	US2	UP2	UFS2	D	UFS
1	AN	8.35	0.645	5.18	1.13	1.98	3.28	2.03
2	-	6.26	0.673	4.55	1.16	1.06	3.28	-
3	-	6.18	0.652	4.86	1.14	-	6.56	-
4	-	6.04	0.598	4.84	1.18	1.98	6.51	-
5	-	6.28	0.438	5.12	1.15	1.92	13.19	-
6	-	6.24	0.522	5.04	1.14	-	13.19	-
7	-	6.14	0.408	5.45	0.97	-	12.74	1.76
8	-	6.14	0.496	4.85	0.98	1.79	12.74	-
9	-	5.97	0.832	4.37	0.985	1.96	2.95	1.79
10	-	5.94	0.665	3.72	1.025	2.03	3.45	1.78
11	-	6.15	0.441	5.09	1.00	1.50	13.41	1.80
12	-	6.14	0.444	5.04	1.01	1.56	13.36	1.81
13	-	6.12	0.50	4.96	-	1.71	12.97	-
14	EQ	8.06	0.484	5.41	1.075	1.81	3.34	1.93
15	-	5.83	0.471	4.97	1.10	1.83	6.61	-
16	-	5.92	0.540	4.72	1.10	1.91	6.65	-
17	-	5.98	0.431	5.19	1.085	1.79	12.94	-
18	-	5.94	0.460	4.98	1.095	1.69	12.94	-
19	SO	8.31	0.409	5.53	1.03	1.84	3.34	1.88
20	-	5.96	0.290	5.39	1.05	-	6.61	-
21	-	5.95	0.305	5.20	1.08	-	11.44	-
22	AN	8.313	0.85	5.77	1.76	3.29	9.56	3.20
23	-	6.144	0.38	5.894	1.95	2.91	8.89	3.43
24	-	6.170	0.84	5.942	2.00	3.38	6.35	3.48

QUARTZITE

NO	SM	US1	UP1	US2	UP2	UFS2	D	UFS
25	-	6.378		5.596	1.98	3.78	6.38	-
26	-	6.302	0.671	5.982	1.74	2.97	6.38	
27	-	-	-	5.238	1.98	3.41	6.38	
28	-	6.36	0.68	5.62	2.02		6.36	
29	-	6.22	0.67	5.86	2.37	4.26	8.14	
30	-	6.155	0.41	5.81	2.41	3.45	6.80	
31	-	6.18	0.83	5.91	2.40	4.17	4.56	
32	-	6.17	0.453	4.68	0.77	1.23	11.07	1.41
33	-	6.06	0.432	4.82	0.875	1.24	13.42	1.55
34	-	6.04	0.422	4.80	0.865	1.19	13.42	1.55
35	-	6.12	0.413	4.88	0.87	1.16	13.42	1.57
36	-	5.94	0.665	3.72	1.025	2.03	3.45	1.78
37	-	6.18	0.468	5.03	0.98	1.65	11.07	1.78
38	-	6.14	0.406	5.45	0.97		12.74	1.76
39	-	6.14	0.496	4.85	0.98	1.78	12.74	
40	-	6.15	0.441	5.09	1.00	1.50	13.41	1.80
41	-	6.14	0.444	5.04	1.01	1.56	13.38	1.81
42	-	5.97	0.832	4.37	0.985	1.98	2.95	1.79
43	-	6.12	0.50	4.96	(1.08)	1.71	12.97	(1.92)
44	-	6.206	(0.29)	5.530	(1.95)	(3.08)	6.38	3.49
45	-	6.302	0.671	5.238	1.98	3.41	6.38	3.49
46	-	6.36	0.68	5.82	2.02		6.36	3.58
47	-	6.22	0.67	5.88	2.37	4.265	6.14	3.28
48	-	6.15	(0.41)	5.81	2.41	3.45	6.80	4.19
49	-	6.18	0.83	5.91	2.40	4.17	4.56	3.33

US *

TABLE 1B

NO	SM	US	UP	UFS	D	UFS
50	AN	6.234	2.41	3.61		4.31
51	-	6.15	2.50	4.26		4.42
52	-	6.27	2.47	4.07		4.43
53	-	6.25	2.59	4.06		4.61
54	-	6.28	2.70	4.53		4.78

US *

TABLE 1IA

NO	SM	RHO0	P1	V1/V0	P2	V2/V0	VT/V0
1	AN	2.628	107.6	0.8924	170	0.8018	
2	-	-	110.7	0.8925	164	0.7904	
3	-	-	105.0	0.8945	167	0.7907	
4	-	-	94.9	0.9010	154	0.7816	

5	-	-	72.3	0.9303	165	0.7888	
6	-	-	85.6	0.9163	165	0.7910	
7	-	-	65.5	0.9339	144	0.8295	
8	-	-	80.0	0.9192	140	0.8170	
9	-	-	130.5	0.9606	147	0.8234	
10	-	-	103.8	0.9880	136	0.7834	
11	-	-	71.3	0.9283	145	0.8167	
12	-	-	71.6	0.9277	145	0.8134	
13	-	-	80.4	0.918			
14	EQ	2.629	77.1	0.9214	159	0.8108	
15	-	-	72.2	0.9192	153	0.7907	
16	-	-	84.0	0.9088	152	0.7870	
17	-	-	67.8	0.9279	156	0.8004	
18	-	-	71.8	0.9225	153	0.7923	
19	SO	2.626	67.8	0.9352	157	0.8218	
20	-	-	49.4	0.9513	153	0.8095	
21	-	-	47.7	0.9487	150	0.8024	
22	AN	2.65	142.0	0.865	279	0.705	0.882
23	-	2.629	61	0.938	295	0.661	0.733
24	-	-	103	0.898	297	0.648	0.817
25	-	-	-	-	298	0.654	
26	-	-	111	0.894	278	0.714	0.854
27	-	-	-	-	287	0.637	0.846
28	-	-	114	0.893	311	0.651	
29	-	-	110	0.892	369	0.600	
30	-	-	67	0.933	371	0.588	0.662
31	-	-	137	0.866	382	0.598	
32	AN	2.629	74.	0.927	111.	0.857	
33	-	-	68.7	0.929	120.5	0.830	
34	-	-	67.0	0.930	122.	0.838	
35	-	-	66.7	0.932	123.5	0.837	
36	-	-	103.8	0.888	136.	0.783	
37	-	-	76.2	0.924	142.	0.820	
38	-	-	65.5	0.934	144.	0.829	
39	-	-	80.0	0.919	140.	0.817	
40	-	-	71.3	0.928	144.5	0.817	
41	-	-	71.6	0.928	145.5	0.813	
42	-	-	130.5	0.861	147.	0.823	
43	-	-	80.4	0.918	154.	0.793	
44	-	-	-	-	306.	0.668	0.778
45	-	-	111.	0.894	287.	0.637	0.846
46	-	-	114.	0.893	308.	0.651	
47	-	-	110.	0.892	369.	0.630	
48	-	-	67.	0.933	371.	0.588	0.662
49	-	-	135.	0.866	377.	0.598	

TABLE 118

NO	SM	RHO0	P	V/V0	VF/V0
50	AN	2.629	395	0.613	0.704
51	-	-	404	0.594	0.796

106/14/77

52	-	-	407	0.606	0.773
53	-	-	426	0.586	0.717
54	-	-	445	0.570	0.767

TABLE III LISTS RELEASE STATES BETWEEN P=0 AND P2 OBTAINED BY RELEASE OF THE ABOVE SHOCKS INTO BUFFERS OF MAGNESIUM (MO), GLYCEROL (GL), WATER (W), ETHANOL (ET), ETHYLEETHER (ETE), OR BY ACCELERATING A BRASS SHIM (BS) P1/U IS A RELEASE STATE FROM THE ELASTIC PRECURSOR AND P2R FROM THE FINAL SHOCK STATE P2. P IS IN KBAR AND U IN KM/SEC.

TABLE III

ENTRY	32	33	33	34	34	35
P1/U	51.5/.558	24.3/.591	13.4/.627	23.9/.570	15.7/.555	22.8/.748
P2/U	79.5/.817	54.5/1.02	41.2/1.12		36.5/.894	38.1/1.01
BUFFER	MO	GL	ET	GL	H	W
ENTRY	35	39	39	40	40	41
P1/U	13.5/.657	46.0/.505	52.3/.568	24.8/.575	21.7/.693	13.3/.637
P2/U	34.2/1.20	96.0/.958	96.0/.96	71.0/1.19	58.4/1.25	58.5/1.07
BUFFER	ET	MO	MO	GL	H	W
ENTRY	41	41	43	43	46	46
P1/U	23.1/.758	15.0/.675	28.2/.651	17.6/.755		
P2/U		48.1/1.29	75.3/1.26		184./2.36	109./2.71
BUFFER	W	ET	GL	ET	GL	ETE
ENTRY	47	47	49	49	49	
P2/U	41.0/3.22	31.0/3.44	332./2.51	275./3.13	134./3.04	
	BS	BS	MO	GL	ETE	

COMMENTS

- 1) SOURCE: AHRENS, T. J. AND DUVALL, G. E.
J. GEOPHYS. RES., VOL. 71, P. 4349 (1966) (ENTRY 1-22)
AHRENS, T. J. AND ROSENBERG, J. T.
CONFERENCE ON SHOCK METAMORPHISM (1966)
POULTER LABORATORY, PALO ALTO, CALIF. USA (ENTRY 22-31,50-54)
AHRENS T.J., ROSENBERG J.T., RUOFERMAN M.H.
DYNAMIC PROPERTIES OF ROCKS
PROJECT FOU-4816. REPORT DASA 1968 (SEPT. 30 1966)
STANFORD RESEARCH INSTITUTE
MENLO PARK, CALIF., USA (ENTRY 32-49)
- 2) EXPERIMENTAL TECHNIQUE C2
DATA REDUCTION METHOD B STANDARD MATERIALS 2024 ALUMINUM
356 BRASS
D WITH UPI = 1/2*UFS1.
- 3) VOI WAS CALCULATED FROM THE HEXAGONAL LATTICE CONSTANTS A=4.91267 AND B=5.40459 ANGSTROM: CRYSTAL DATA DETERMINATIVE TABLES, MONOGRAPH 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION, POLYCRYSTAL BOOK SERVICE, BROOKLYN, N.Y., 1963) 2ND ED.
- 4) THE ATTENUATION OF THE ELASTIC WAVE WAS DETERMINED TO BE ABOUT 3 dB PER MM.

- 5) CALCULATED FINAL VOLUMES INDICATE THAT THE SHOCK TRANSFORMED MATERIAL REMAINS IN THE HIGH DENSITY PHASE.
- 6) VF IS CALCULATED ON THE ASSUMPTION THAT THE ISENTROPIC RELEASE PATH IN THE P,V PLANE IS LINEAR
- 7) ENTRIES 22 23 44 AND 48 HAVE UNCERTAIN UP1 VALUES. UP1 VALUES OF ENTRY 46 47 AND 49 WERE ESTIMATED. UP2 OF ENTRY 44 IS ALSO UNCERTAIN. AND UP1 VALUE FOR THE CALCULATION OF P2 AND V2/V0 ESTIMATED.
- 8) THE DATA IN THE 260 - 300 KBAR RANGE INDICATED AN INCREASE OF COMPRESSIBILITY AND THE POSSIBILITY OF A TWO WAVE STRUCTURE.
- 9) THE SLOPE DP/DV ALONG THE RELEASE PATH IMPLIES A FROZEN COMPOSITION EXCEPT THAT A) ENTRY 47 AND 49 SHOW RECONVERSION FROM STISHOVITE TO ALPHA QUARTZ BELOW 40 KBAR. AND B) RECOVERED SAMPLES CONSIST MAINLY OF POWDERED ALPHA QUARTZ.
- 10) HANGANIN AND PARTICLE VELOCITY GAUGE EXPERIMENTS CONFIRM THE ABOVE BEHAVIOR AND INDICATE THAT MURNAGHAN FORMS FOR ALPHA QUARTZ AND STISHOVITE CAN BE USED TO REPRESENT THE RELEASE PATHS OF THE MIXED PHASES. THE SAMPLES USED WERE ARKANSAS NOVACULITE ($\rho_{H00}=2.63 \text{ g/cc}$ $C_L=0.59 \text{ km/sec}$) AND NUGGET SANDSTONE ($\rho_{H00}=2.63 \text{ g/cc}$ $C_L=0.58 \text{ km/sec}$) (W.J. MUERY AND D.E. GRADY, EQUATION OF STATE OF ROCKS, (LAWRENCE LIVERMORE LABORATORY, LIVERMORE CALIF. 94550, REPORT NO. UCRL-13580 1973)

TABLE IA

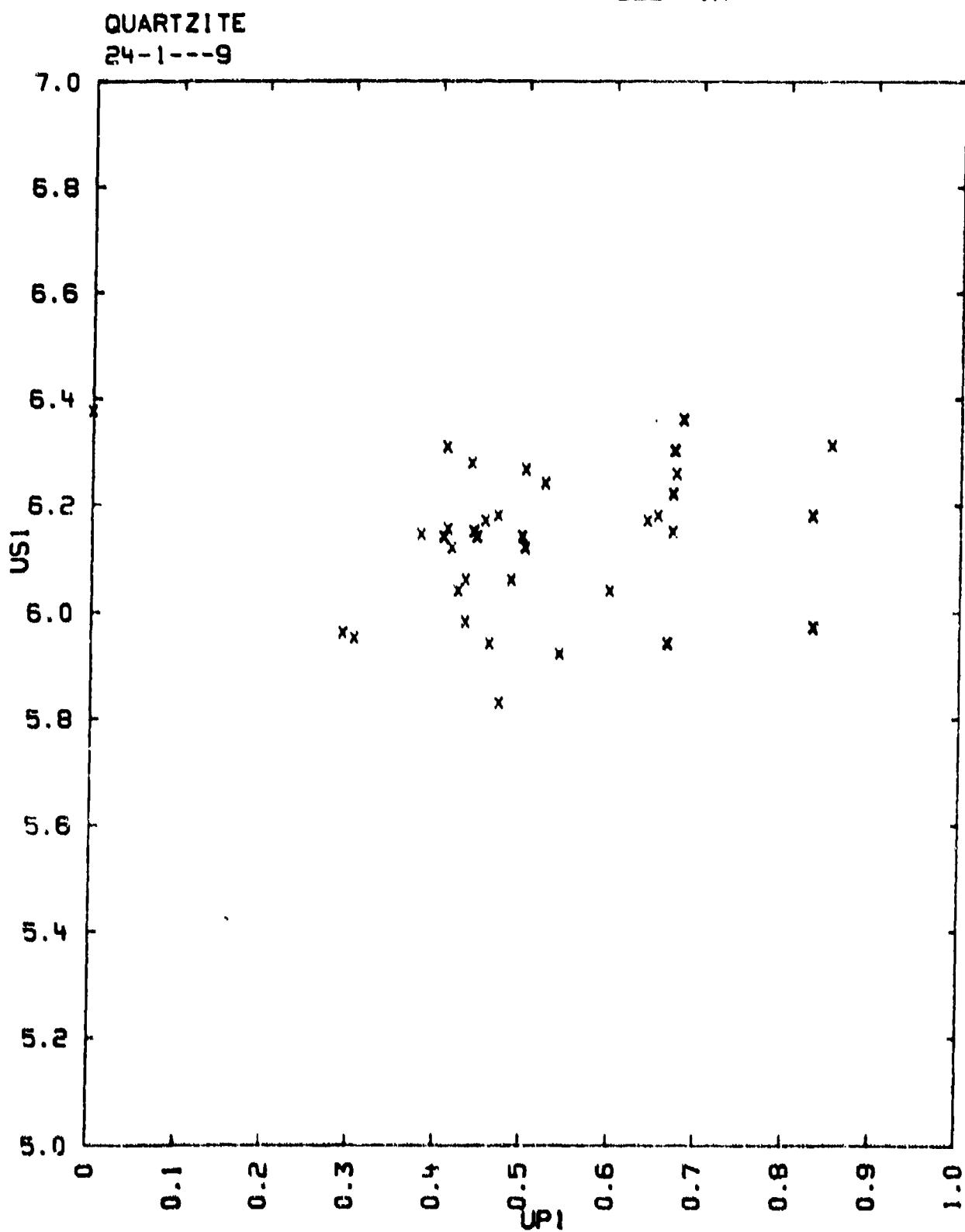


TABLE IA

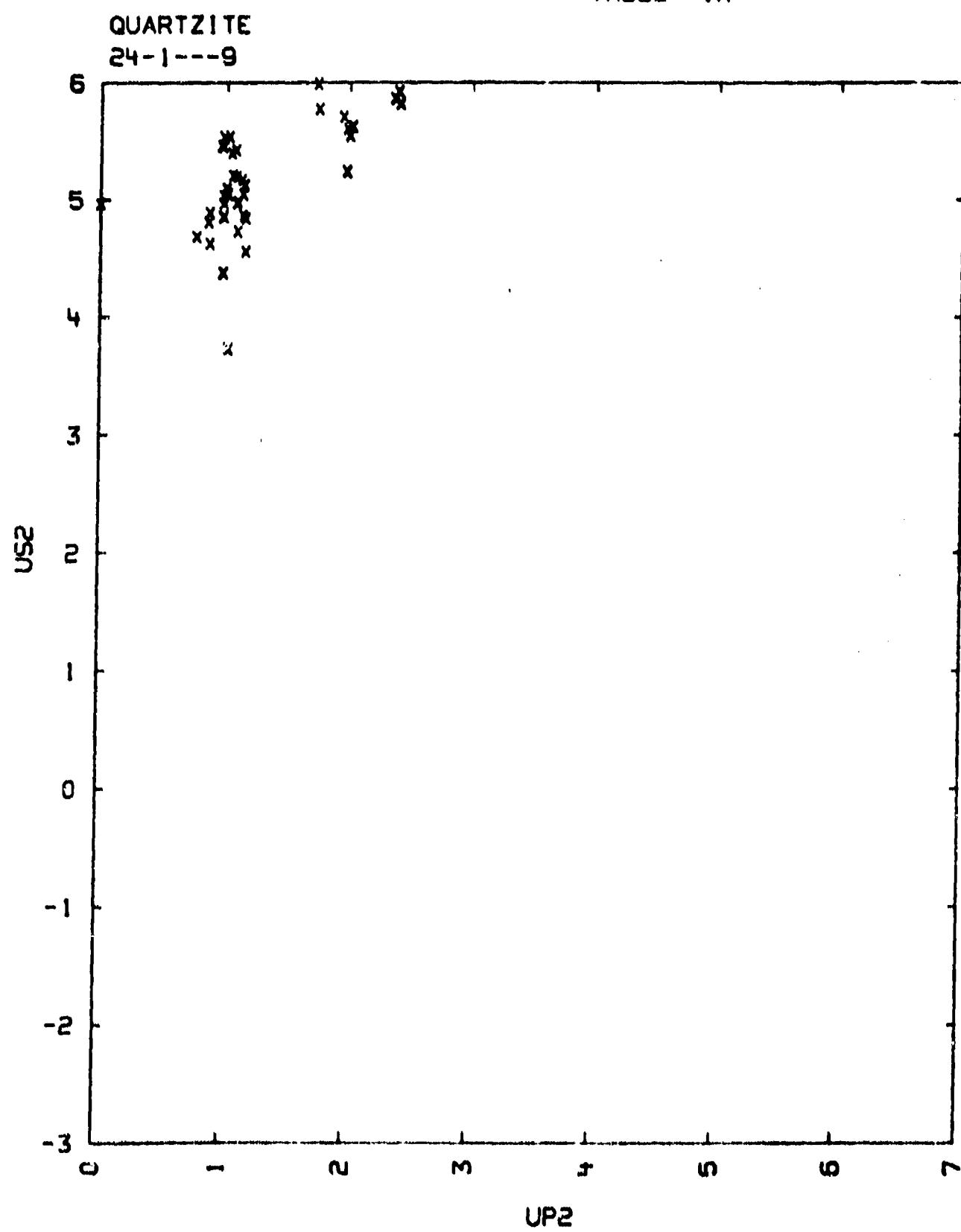
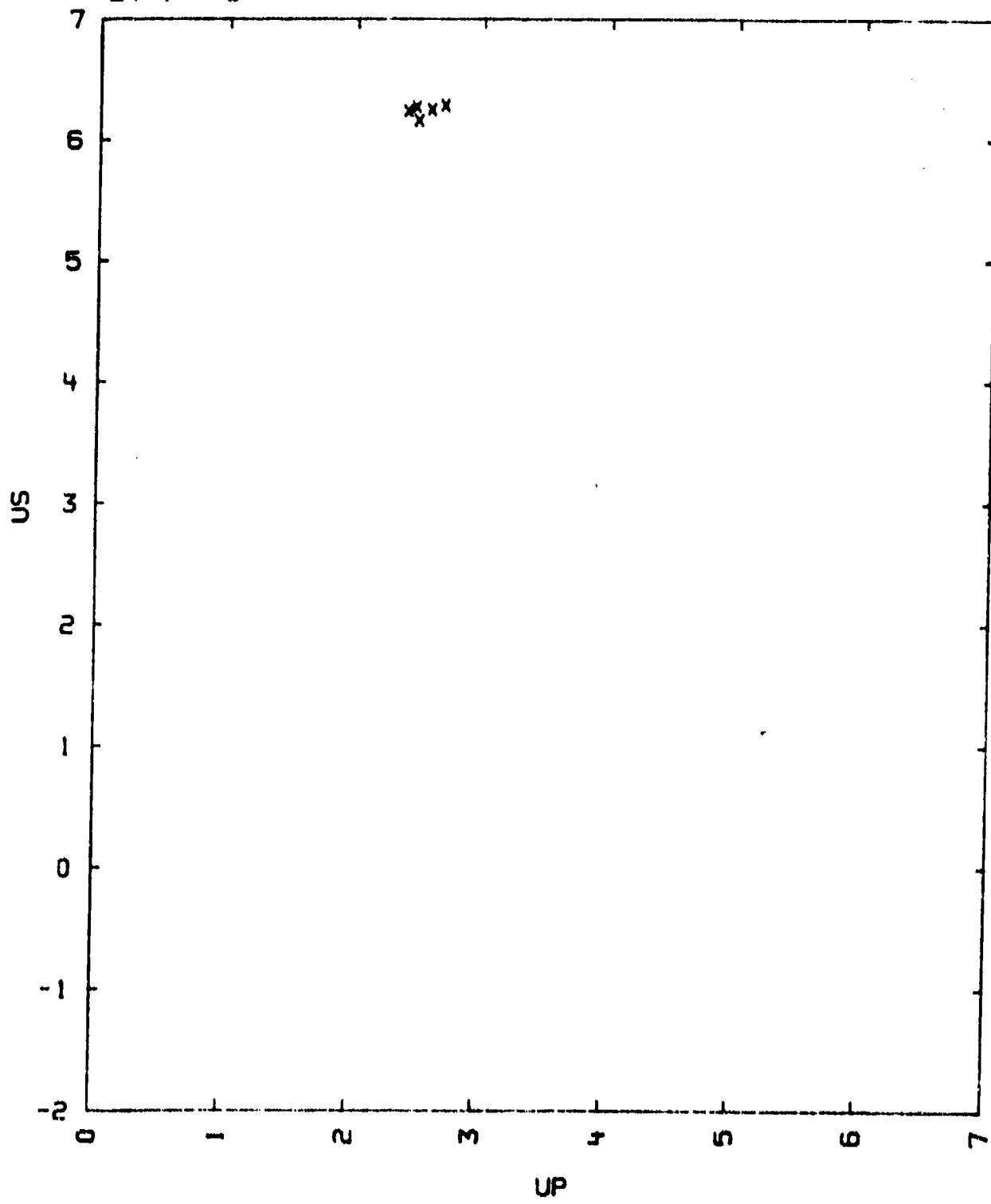


TABLE 1B

QUARTZITE
24-1---9



24-1--10
QUARTZ CRYSTAL (SILICON DIOXIDE)

SI-02

$$V_0 = 0.3767 \text{ CC}/\text{O}$$
$$V_{01} = 0.3774 \text{ CC}/\text{O}$$

THE TABLE GIVES PRESSURE IN KBARS VELOCITIES IN KM/SEC AND DENSITY IN O/CC. AXIS GIVES THE PROPAGATION DIRECTION OF THE SHOCK WAVE. D IS SAMPLE THICKNESS IN MM.

TABLE I

RHO0	US1	UP1	P1	V1/V0	US2	UP2	UFS2	P2	V2/V0	D	AXIS
2.654	5.8	0.66	102	0.888	5.42	2.01	3.3	295	0.558	3.40	X
-	6.27	0.54	89	0.914	5.72	1.94	3.17	299	0.604	6.38	X
-	6.427	0.537	91.6	0.916	5.661	1.93	3.29	298	0.602	6.60	Y
-	7.29	0.81	157	0.888	5.92	2.40	3.38	401	0.528	6.60	Z

US -

TABLE II

RHO0	US	UP	UFS	P	V/V0	D	AXIS
2.654	5.635	1.815	3.46	272	0.678	6.40	X
-	5.696	1.803		272.5	0.684	3.22	X
-	5.685	1.98	3.356	298	0.652	6.38	X
-	5.79	2.46	4.13	377	0.575	6.38	X
-	5.78	2.48	4.10	380	0.571	3.39	X
-	6.003	2.61	4.29	416	0.465	6.38	X
-	5.82	2.46	4.08	379	0.578	6.60	Y
-	6.218	2.58	4.19	426	0.585	6.60	Y

US -

COMMENTS:

- 1) SOURCE: AHRENS, T. J. AND ROSENBLUTH, J. T.
CONFERENCE ON SHOCK METAMORPHISM (1966)
POULTER LABORATORIES, PALO ALTO, CALIF.
- 2) EXPERIMENTAL TECHNIQUE: C2
DATA REDUCTION METHOD: B STANDARD MATERIALS .0254 ALUMINUM
350 BRASS
D WITH UP1=1/2+UFS1 FOR THE ELASTIC WAVE.
- 3) V01 WAS OBTAINED FROM THE HEXAGONAL LATTICE PARAMETERS A=4.91265 AND
C=5.40441 ANGSTROM; CRYSTAL DATA DETERMINATIVE TABLES, MONOGRAPH 9
AMERICAN CRYSTALLOGRAPHIC ASSOCIATION, POLYCRYSTAL BOOK SERVICE.

BROOKLYN, N.Y., 1963) 2ND ED.
4) AS IN MATERIAL 24-1---9 VOLUMES CALCULATED FROM RELEASE ISENTROPES
DENSER THAN THE ORIGINAL QUARTZ.
INDICATED THAT THE RELEASED MATERIAL IS BETWEEN 7 AND 32 PERCENT

TABLE II

QUARTZ CRYSTAL (SILICON DIOXIDE)

24-1---10

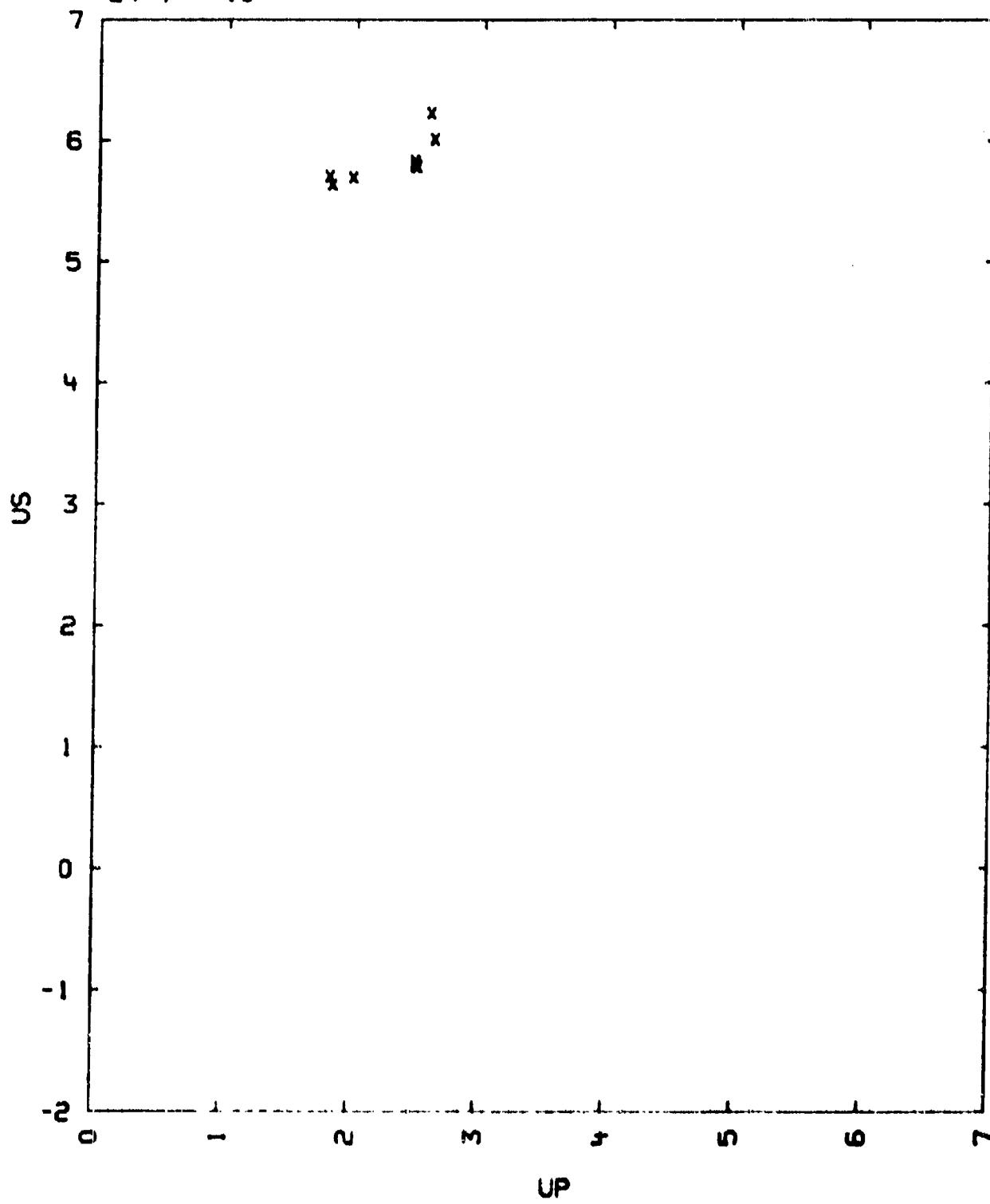


TABLE I

QUARTZ CRYSTAL (SILICON DIOXIDE)

24-1---10

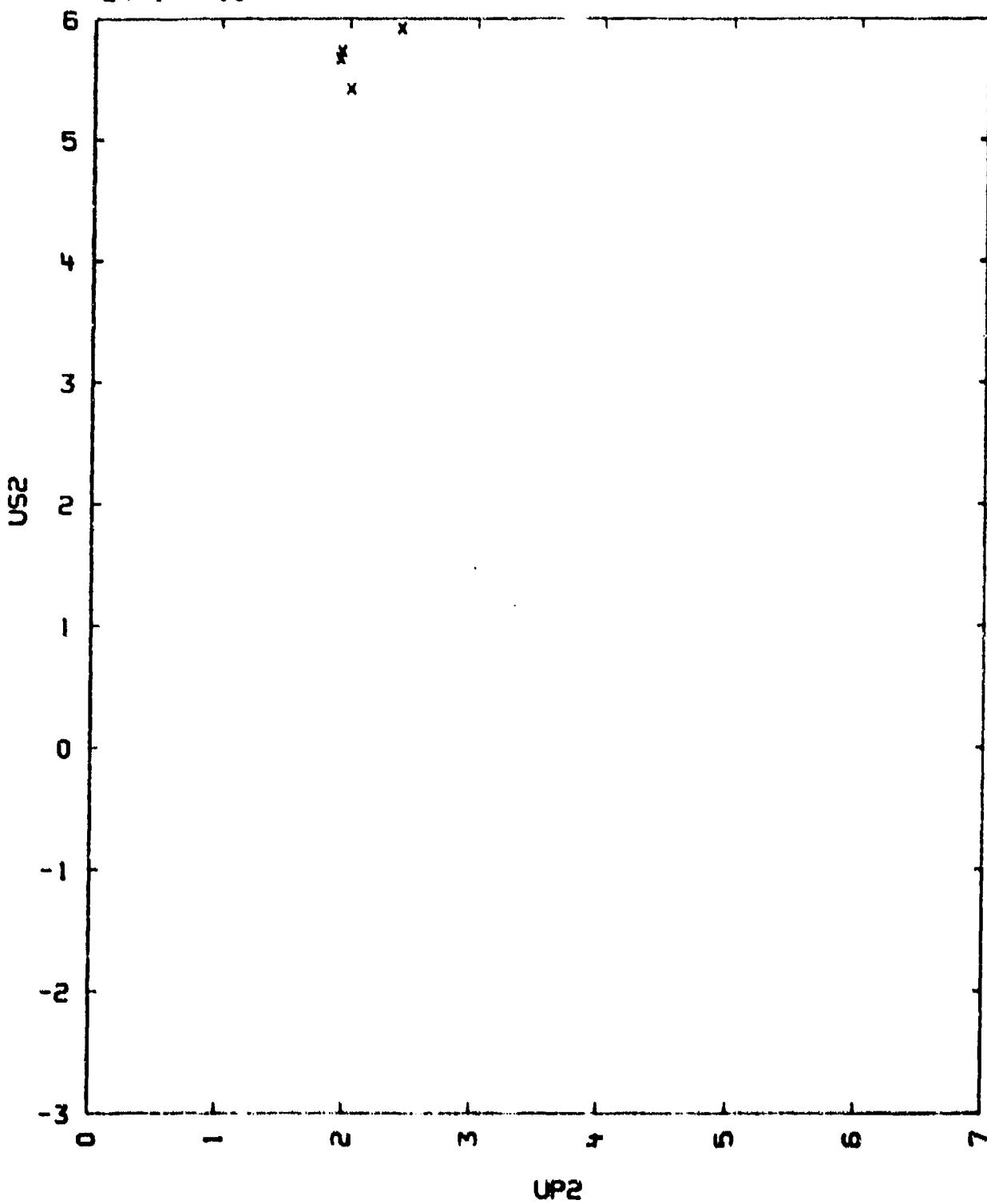
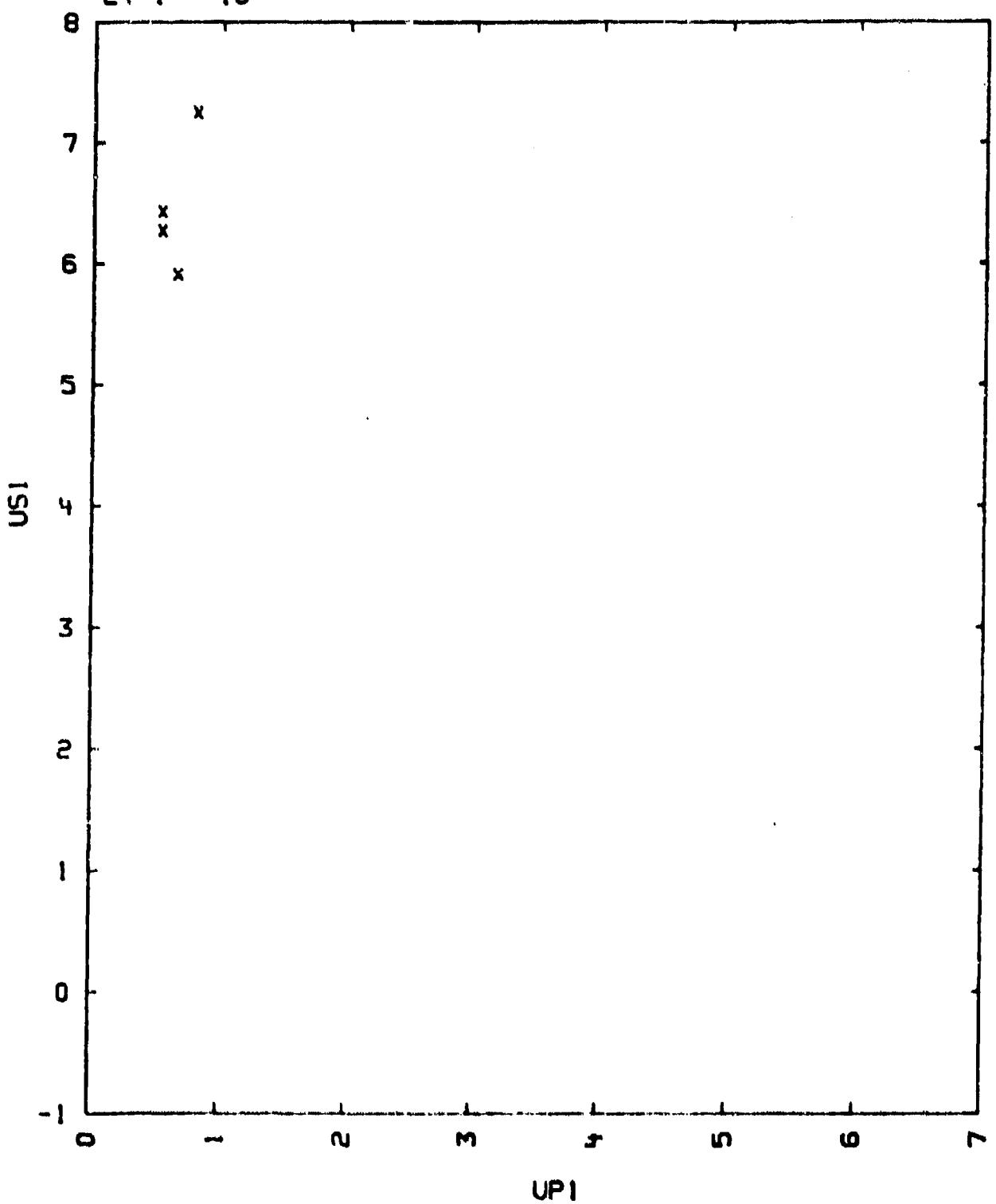


TABLE I

QUARTZ CRYSTAL (SILICON DIOXIDE)
24-1---10



24-1---11
QUARTZ (SAND)

SI-02 100 PERCENT BY WT
POROSITY 37 PERCENT BY VOL.
PARTICLE SIZE 74-149 MICRONS

$$V_0 = 0.606 \text{ CC}/\text{O}$$

$$VOL = 0.3774 \text{ CC}/\text{O}$$

IN THE TABLE BELOW, TEMPERATURE (T_0) IS GIVEN IN DEGREES CENTIGRADE,
DENSITY IS IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS.

TABLE

T_0	ρ_{H_2O}	US	UP	P	V/V ₀
-10	1.65	4.07	2.17	146	0.487
-10	1.65	4.05	2.25	150	0.445
-10	1.65	5.31	3.13	274	0.410
-10	1.65	6.39	3.61	404	0.402

$$US = 0.868 + 1.44 \cdot UP \text{ KM/SEC} \quad \text{SIGMA US} = 0.09 \text{ KM/SEC}$$

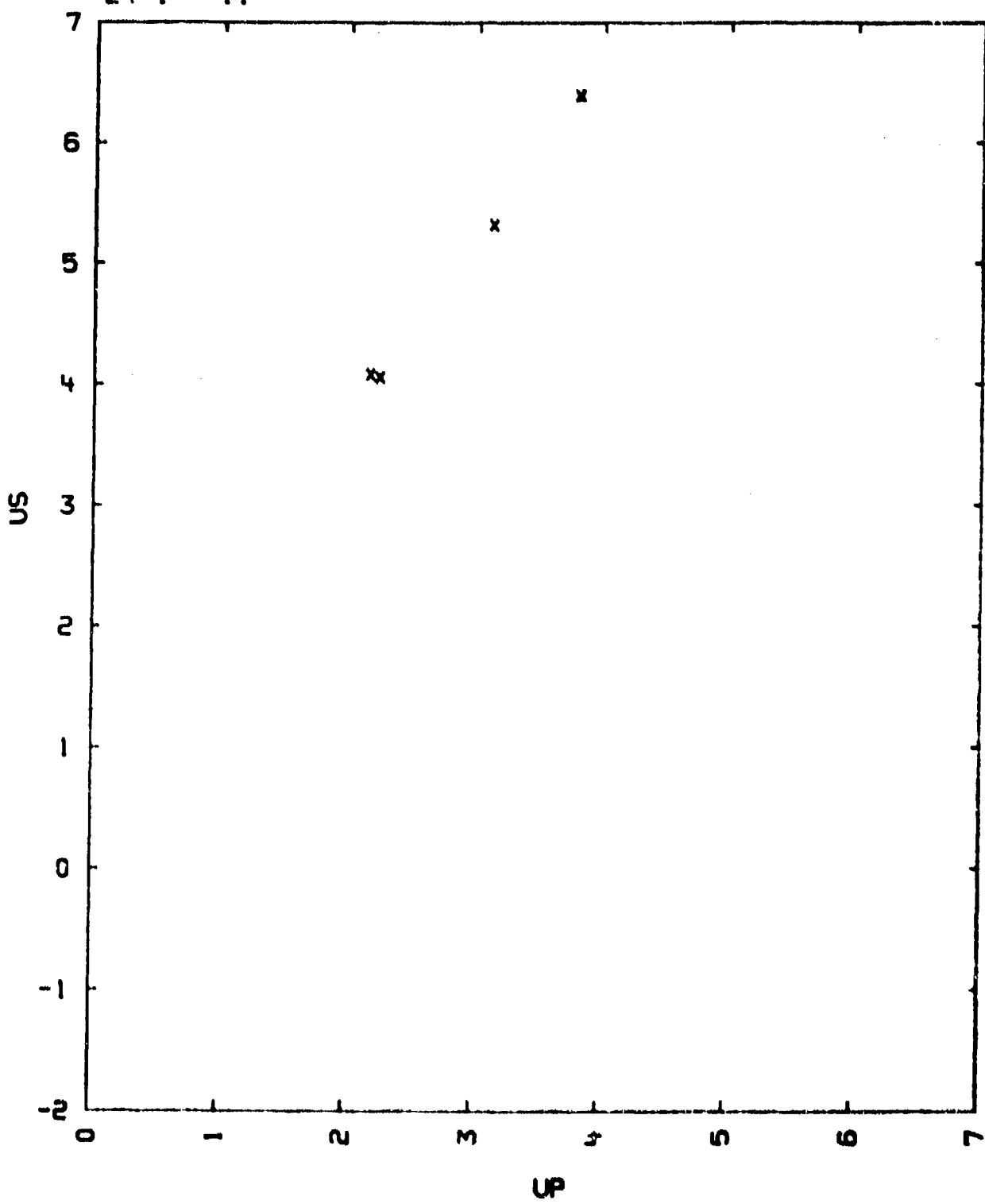
COMMENTS:

- 1) SOURCE: ANDERSON, O. D.
INTERIM DATA REPORT FOU-6392 (1967)
STANFORD RESEARCH INSTITUTE, MENLO PARK, CALIFORNIA, USA.
- 2) EXPERIMENTAL TECHNIQUE D.
DATA REDUCTION TECHNIQUE B.
STANDARD MATERIAL 2024 ALUMINUM
- 3) THE SAMPLE WAS OTTAWA BANDING SAND, OBTAINED FROM THE OTTAWA SILICA CO., OTTAWA, ILLINOIS, U.S.A..
- 4) VOL WAS CALCULATED WITH THE HEXAGONAL UNIT CELL CONSTANTS A = 4.91267 AND C = 5.40450 ANGSTROMS; A.C.A. MONOGRAPH NO. 5 (AMERICAN CRYST. ASSN., POLYCRYSTAL BOOKSERVICE, NEW YORK, N. Y., USA (1963)) 2ND ED.

TABLE I

QUARTZ (SAND)

24-1---11



24-1---12
QUARTZ (COCONINO SANDSTONE)

QUARTZ	SI-02	97 VOLUME PERCENT
FELDSPAR:		3 - -
	K-AL-S13-08	
	NA-AL-S13-08	
	CA-AL2-S12-08	
CLAY AND HEAVY MINERALS		TRACE
POROSITY (CALC.)		2%
GRAIN SIZE		0.06 - 0.7 MM.

$$V_0 = 0.505 \text{ CC}/\text{O} \quad C_0 = 1.43 \text{ KM}/\text{SEC.}$$

$$V_{01} = 0.3774 \text{ CC}/\text{O}.$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES ARE IN KM/SEC.
AND PRESSURE IN KILOBARS. CS = COCONINO SANDSTONE, FC = FUSED QUARTZ

TABLE

RHO0	US	UP	P	V/V0	MAT
1.98	3.67	1.33	97.	0.637	CS
-	4.10	1.63	132.	0.602	-
-	4.49	2.18	194.	0.514	-
-	4.84	2.57	258.	0.468	-
-	5.66	3.12	349.	0.449	-
-	5.79	3.25	373.	0.438	-
-	7.57	4.30	644.	0.432	-
-	7.79	4.43	684.	0.431	-
-	8.82	5.07	886.	0.429	-
-	10.09	5.94	1186.	0.411	-
-	11.20	6.43	1426.	0.406	-
	2.204	11.42	6.34	1596.	0.445
					FC

US = $0.36 + 1.67 \cdot UP$ KM/SEC. FOR THE CS DATA.

COMMENTS:

1) SOURCE: JONES, A. H., ISDELL, W. M., SHIPMAN, F. H., PERKINS, R. D., GREEN, S. J. AND MAIDEN, C. J.
INTERIM REPORT, CONTRACT NAS2-3427, 1968
GENERAL MOTORS TECH. CENTER, WARREN, MICHIGAN 48090

2) EXPERIMENTAL TECHNIQUE A:
DATA REDUCTION TECHNIQUE A

STANDARD MATERIALS: OFHC COPPER AND FANSTEEL-77 ALLOY. THE
COPPER STANDARD US-UP HUGONIOT RELATIONSHIP IS
GIVEN BY:

$$US = 3.96 + 1.497 \cdot UP \text{ KM/SEC. } RHO0 = 8.93 \text{ G/CC}$$

THE FANSTEEL US-UP HUGONIOT IS GIVEN BY:

$$US = 3.96 + 1.295 \cdot UP \text{ KM/SEC. } RHO0 = 17.01 \text{ G/CC}$$

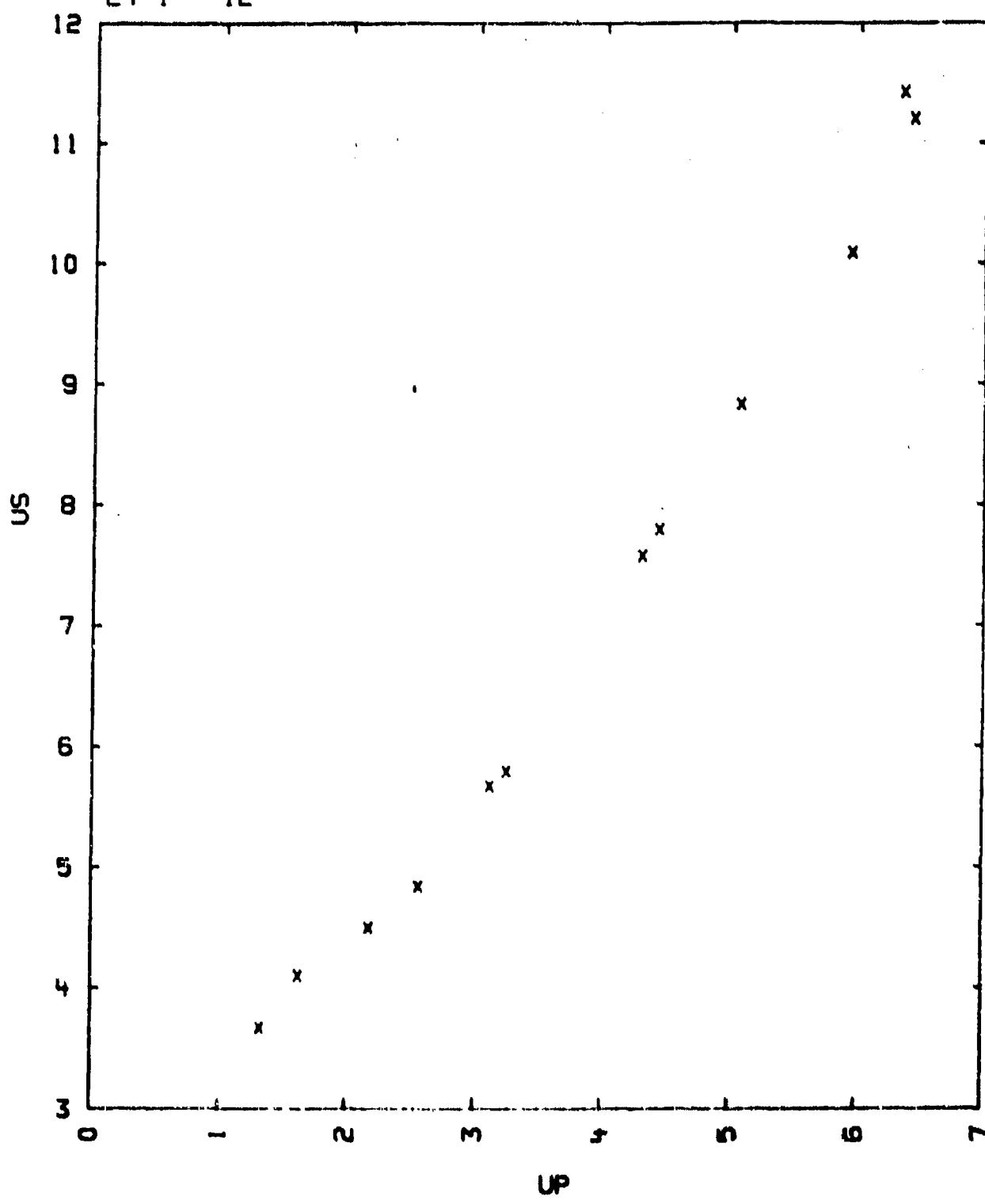
3) THESE PRESSURES WERE ACHIEVED BY USING A TWO-STAGE LIGHT GAS GUN.
THE PROJECTILE IMPACT VELOCITY AND TILT WERE MEASURED BY TWO TIMED

- FLASH X-RAY SHADOWGRAPHS OF THE PROJECTILE.
- 4) THE ESTIMATED EXPERIMENTAL ERROR IN MEASURING US 15 .2 - 2 PERCENT UP IS PRECISE TO 0.2 PERCENT.
- 5) SAMPLE DESCRIPTION: SANDSTONE IS WEAKLY TO MODERATELY WELL CEMENTED WITH SILICA, IN THE FORM OF QUARTZ OVERGROWTHS ON THE GRAINS. SUBPARALLEL LAMINAEE 5.0 TO 17.5 MM THICK SEPARATED BY THIN LAMINAEE 0.5 MM THICK CONTAINING MORE THAN AVERAGE AMOUNTS OF SILT AND CLAY SIZED GRAINS.
- 6) THE UNCONFINED CRUSHING STRENGTH NORMAL TO BEDDING WAS $3.14(10^{10})$ DYNES/(CM 2) FOR A DRY SAMPLE AND $3.64(10^{10})$ DYNES/(CM 2) FOR A SAMPLE SATURATED WITH WATER

TABLE I

QUARTZ (COCONINO SANDSTONE)

24-1---12



24-23---1
SILICON CARBIDE

SI-C

$$V_0 = 0.3196 - 0.3211 \text{ CC/G} \quad C_L = 11.73 \text{ KM/SEC} \quad C_0 = 8.00 \text{ KM/SEC}$$

$$V_{01} = 0.3105 - 0.3088 \text{ CC/G} \quad C_S = 7.43 \text{ KM/SEC}$$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBARS AND DENSITY IN G/CC.

TABLE I

-----SAMPLE-----					-----STANDARD-----	
RHO0	US	UP	P	V/V0	MATERIAL	US(IST)
3.124	10.77	0.48	155.	0.9573	2024 AL	8.22
3.114	10.05	0.87	210.	0.9333	2024 AL	8.52
3.127	9.99	0.92	287.	0.9079	2024 AL	6.90
3.120	9.88	1.37	422.	0.8613	2024 AL	7.53
3.110	9.56	1.58	484.	0.8368	2024 AL	7.76
3.128	9.83	1.67	513.	0.8301	2024 AL	7.93
3.116	9.78	1.93	588.	0.8027	2024 AL	8.26
3.126	10.03	2.16	677.	0.7846	2024 AL	8.59
3.123	10.42	2.47	804.	0.7630	2024 AL	9.03
3.115	10.65	2.79	926.	0.7380	2024 AL	9.45
3.124	10.83	2.83	957.	0.7387	2024 AL	9.53
3.113	10.70	3.00	999.	0.7196	2024 AL	9.71
3.129	10.59	3.20	1060.	0.6978	2024 AL	9.95
3.129	10.59	3.20	1060.	0.6978	2024 AL	9.95
3.124	10.84	3.24	1097.	0.7011	2024 AL	10.03
3.113	10.58	3.56	1170.	0.6629	CU	8.02

$$US = 8.000 + 0.950 \cdot UP \text{ KM/SEC} \quad \text{FOR UP GREATER THAN 1.7}$$

TABLE II

-----SAMPLE-----					-----STANDARD-----	
RHO0	US	UP	P	V/V0	MATERIAL	US(IST)
2.368	5.93	2.05	288.	0.6443	2024 AL	7.65
2.295	6.34	2.24	326.	0.6467	2024 AL	7.88
2.364	6.91	2.44	399.	0.6469	2024 AL	8.19
2.423	7.19	2.48	432.	0.6551	2024 AL	8.30
2.307	6.86	2.52	399.	0.6327	2024 AL	8.24
2.311	7.42	2.86	490.	0.6146	2024 AL	8.67
2.292	6.14	3.15	588.	0.6130	2024 AL	9.08
2.309	6.37	3.19	469.	0.4992	2024 AL	9.16
2.302	6.21	3.27	618.	0.6017	2024 AL	9.22
2.357	6.51	3.44	690.	0.5959	2024 AL	9.48
2.302	6.82	3.62	776.	0.5669	2024 AL	9.88

$$US = -1.419 + 4.629 \cdot UP - 0.506 \cdot UP^2 \text{ KM/SEC}$$

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SILICON CARBIDE

RHOD US UP P V/VO MATERIAL US(ST)

SIG US = 0.16 KM/SEC

COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M., AND CARTER, W.J.,
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B
DATA REDUCTION TECHNIQUE: B
- 3) VD1 IS LESS FOR THE CUBIC THAN THE RHOMBOHEDRAL AND HEXAGONAL STRUC-
TURES, HYCKOFF, CRYSTAL STRUCTURES (JOHN WILEY AND SONS, N.Y., 1963)
VOL. 1
- 4) VDOP/DV1 = 1.25
- 5) THE ELASTIC WAVE WAS NOT OVERDRIVEN IN THESE SHOTS. INTERCEPT WAS
FORCED TO FIT CO

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TABLE I

SILICON CARBIDE
24-23---1

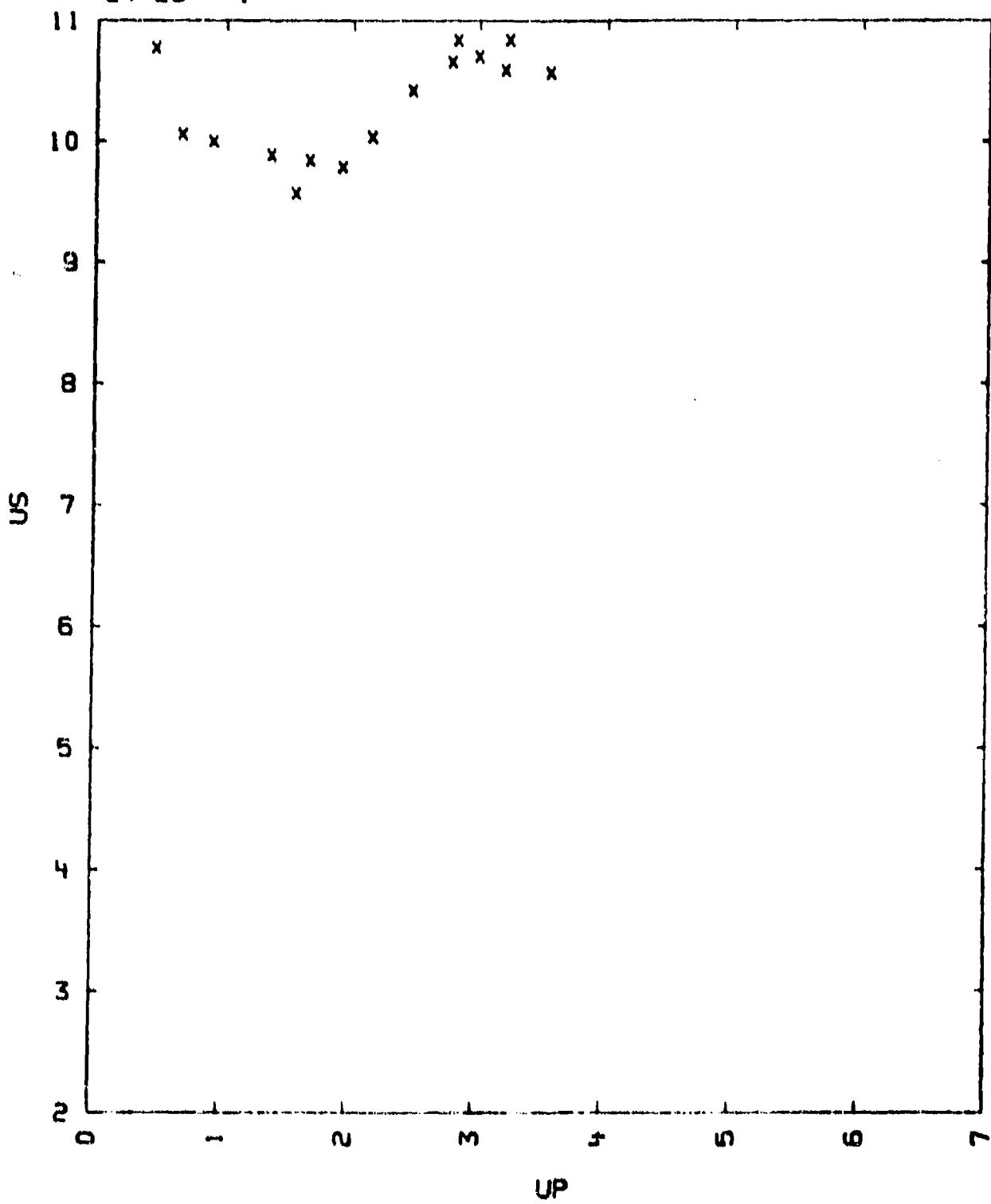
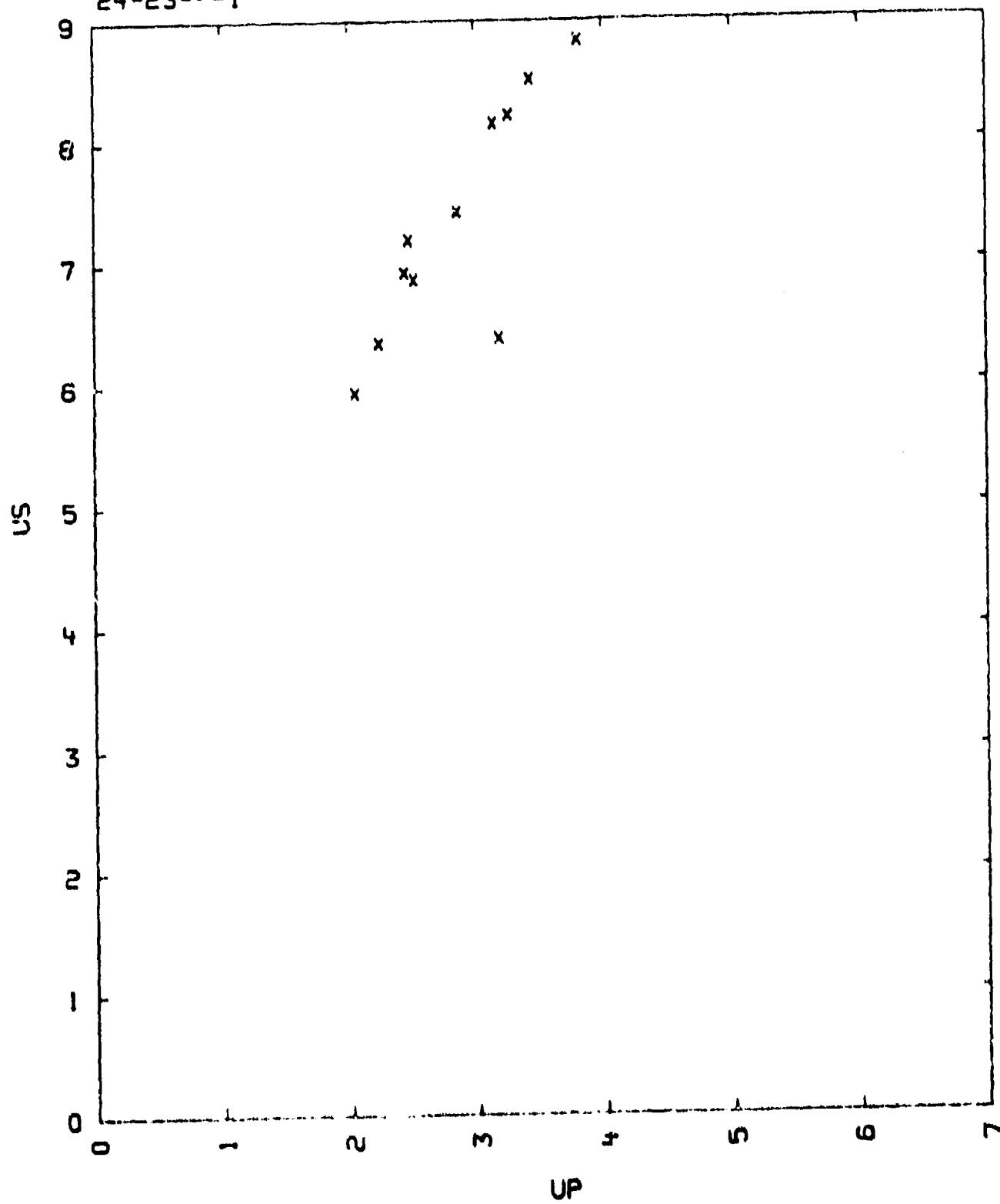


TABLE II

SILICON CARBIDE
24-23---1



24-23-2-1190-182-546-091---1
POLYDIMETHYLSILOXANE (SILICONE 210 FLUID)

H3-C1-S1(C-H3)2-O189-S1-(C-H3)3 + S190-C182-H546-089

T0 = -32 TO 296, DEG. C.
V0 = 0.983 TO 1.350 CC/G

CO(23.5 DEG.C.)=0.99 KM/SEC.

THE TABLE LISTS TEMPERATURE IN DEG. C., DENSITY IN G/CC., VELOCITY IN KM/SEC. AND PRESSURE IN KBAR

TABLE

T0	RHO0	US	UP	P	V/V0
-32	1.017	6.72	3.18	216.	0.527
-20	1.005	6.91	3.46	240.	0.500
-20	1.006	4.97	1.87	91.	0.615
-10	0.996	7.11	3.11	296.	0.492
158	0.849	6.47	3.56	195.	0.450
158	0.849	6.61	3.72	209.	0.438
159	0.848	6.16	3.28	171.	0.4665
256	0.770	4.08	1.94	61.	0.523
279	0.752	6.09	3.31	152.	0.456
296	0.741	6.39	3.91	184.	0.390

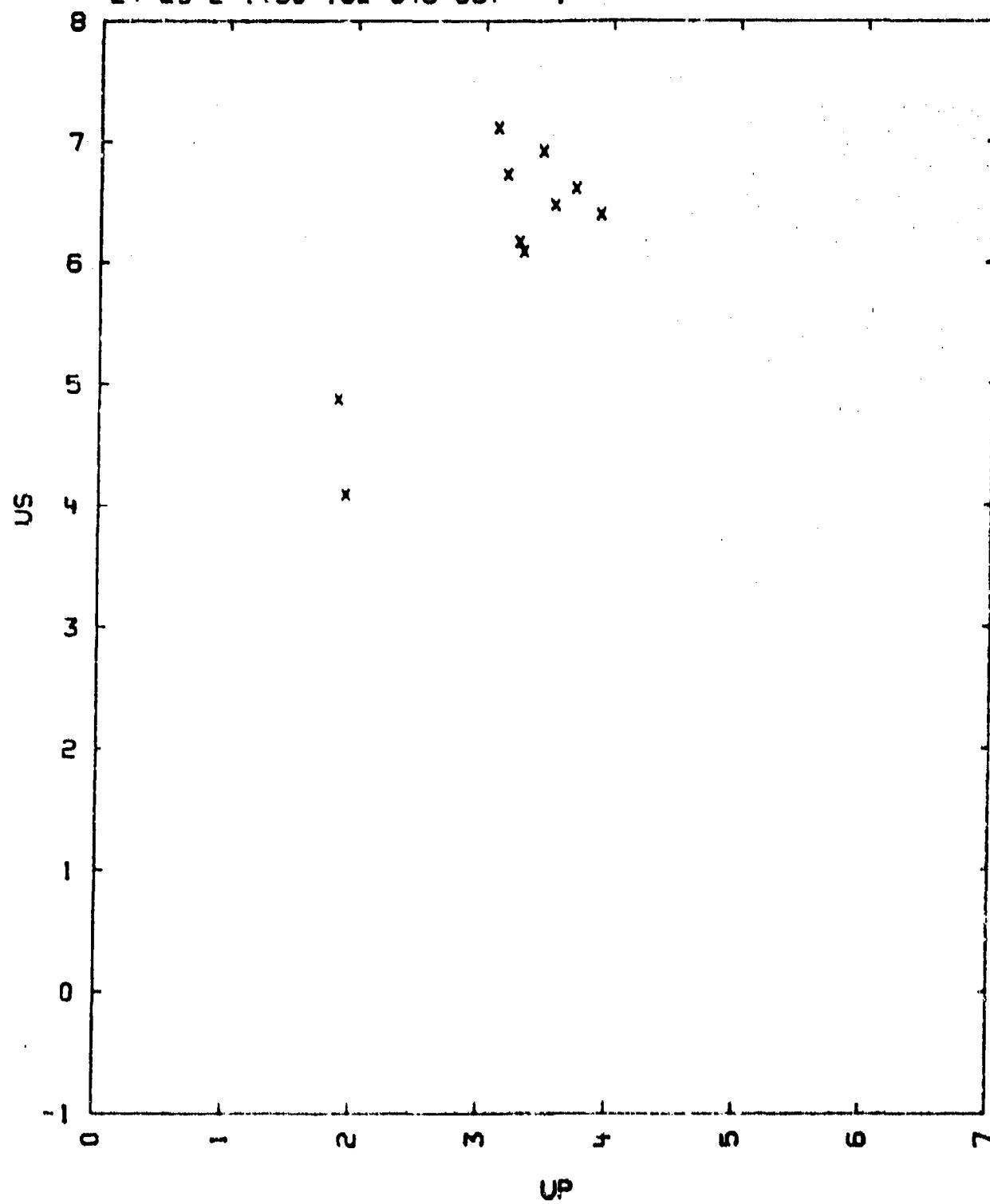
US =

COMMENTS

- 1) SOURCE: CONPERTHWAITE M. AND BLACKBURN J. H.
SRI TECHNICAL REPORT NO. 14
STANFORD RES. INST., MENLO PARK, CALIF. 94025, U.S.A.
- 2) EXPERIMENTAL TECHNIQUE: C1
DATA REDUCTION TECHNIQUE: B STANDARD MATERIAL, BRASS
- 3) ERROR ESTIMATES ARE BETWEEN 0.3 AND 1.5 PERCENT IN US AND UP.
- 4) THE STRUCTURE OF THIS FLUID HAS BEEN TAINED FROM
DOH CORNING ENG. PRODS. DIV. BULLETIN 05-10H, DEC. (1964) AND
F. M. LEWIS, RUBBER CHEM. AND TECHN., VOL. 35, P. 1222 (1962)
PROPERTIES USED FROM THESE SOURCES WERE: VISCOSITY=100 CENTISTOKES
MOL.WT.=6700 G/MOLE
THE ABOVE MOLECULAR WEIGHT (AND SIZE) IS ONLY NOMINAL. THE LIQUID IS
COMPOSED OF SOME UNKNOWN DISTRIBUTION OF MOLECULAR SIZES.
- 5) CO WAS MEASURED SEPARATELY BY REESE AND BLACKBURN, PRIVATE COMM.
THE TEMPERATURE DEPENDENCE MAY BE ESTIMATED FROM $CO = 1.09 \cdot 10^{10} e^{-0.005 T}$
SEE DATA TAKEN BY H. J. MUSKIMAN, J. ACOUST. SOC. AM., VOL. 29
P. 1185 (1957).

U06/14/71

TABLE I
POLYDIMETHYLSILOXANE (SILICONE 210 FLUID)
24-23-2-1 (90-182-546-89) --- |



26-1---1

CASSITERITE (TIN STONE) (TIN OXIDE)

SN-02

$$V_0 = 0.148 \text{ TO } 0.155 \text{ CC}/\text{O}$$

$$V_{01} = 0.1429 \text{ CC}/\text{O}$$

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE STANDARD SAMPLE HOLDER MATERIAL.

TABLE

RHO0	US	UP	P	V/V0	US(ST)
6.45	6.77	2.27	992	0.584	9.26
6.52	6.77	2.31	1021	0.599	9.33
6.75	6.94	2.95	1193	0.633	9.75
6.74	7.32	2.73	1348	0.627	10.10
6.51	7.31	2.68	1410	0.616	10.29

$$US = 3.881 + 1.248 \cdot UP \text{ KM/SEC.}$$

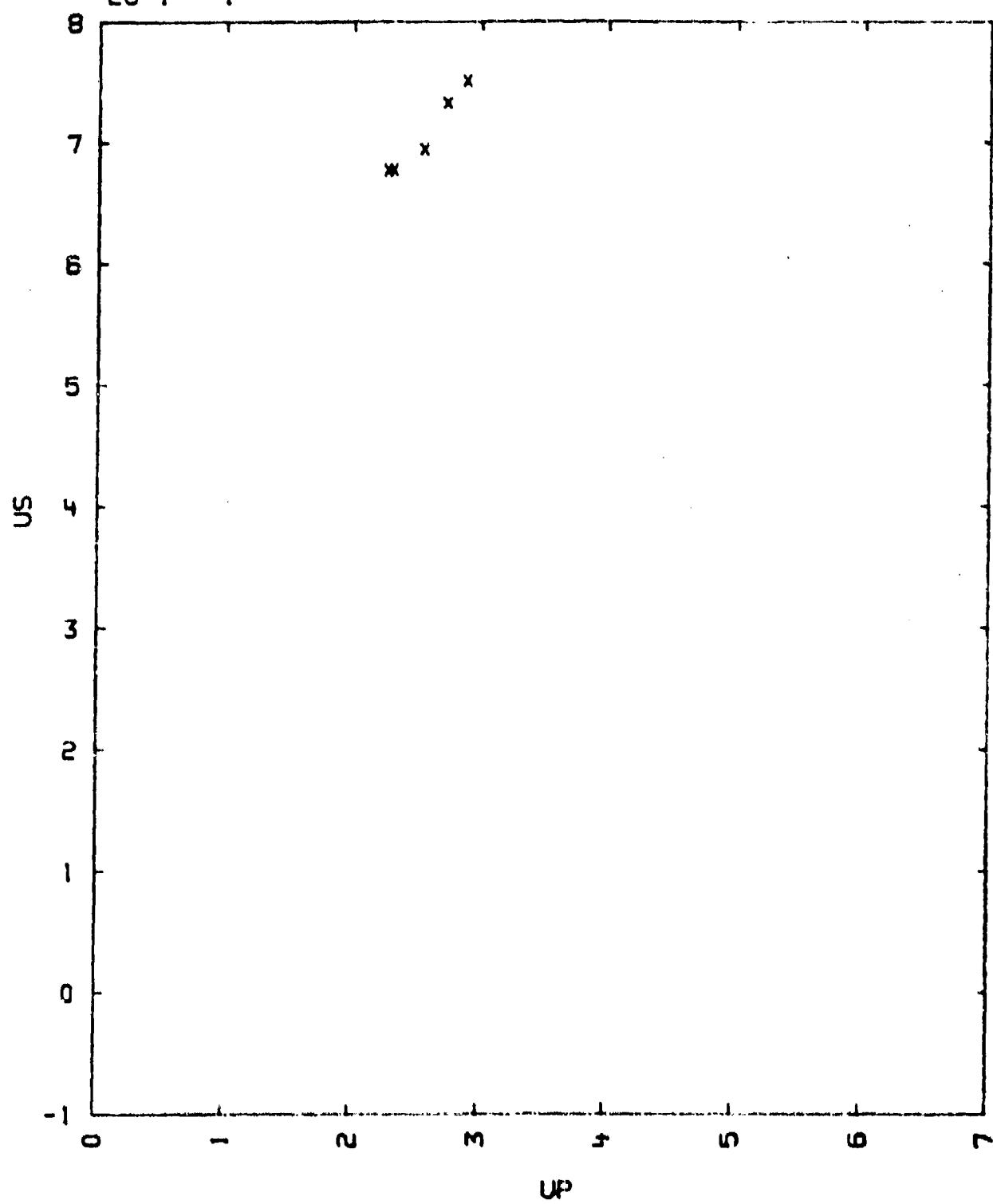
$$\text{SIGMA US} = 0.083 \text{ KM/SEC.}$$

COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.
PRIVATE COMMUNICATION
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) V01 WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED BY WYCKOFF
CRYSTAL STRUCTURES, VOL I (JOHN WILEY AND SONS, NEW YORK, 1963)
- 4) FURTHER WORK IS IN PROGRESS.

U06/14/77

TABLE I
CASSITERITE (TIN STONE) (TIN OXIDE)
26-1---1



2B-1B---1
BORON NITRIDE PYROLYTIC

B-N

$$V_0 = 0.468 \text{ CC/G}$$

$$V_{01} = 0.4389 \text{ CC/G}$$

$$C_L = 2.77 \text{ KM/SEC}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN KM/SEC., AND PRESSURE IN KILOBARS. X DENOTES THE SAMPLE THICKNESS IN MM.

TABLE

X	RHOO	SAMPLE				STANDARD		
		US	UP	UFS	P	V/V0	US	UFS
6.35	2.162	4.82	0.712		76	0.855	6.16	1.22
3.18	2.168	4.65	0.725	1.54	73	0.844	6.16	1.22
6.35	2.129	6.13	1.54		201	0.749	6.98	2.61
3.18	2.120	6.15	1.54	3.03	201	0.750	6.98	2.61
6.35	2.044	6.53	2.13		284	0.674	7.67	3.60
3.18	2.178	6.47	2.09	4.02	284	0.671	7.67	3.60
6.35	2.101	7.35	2.51		386	0.659	8.27	4.42
3.18	2.165	6.94	2.54	4.60	382	0.634	8.27	4.42
6.35	2.067	7.43	2.71		416	0.635	8.39	4.74
3.18	2.117	7.29	2.70	5.14	417	0.630	8.39	4.74
6.35	2.153	7.65	3.18		520	0.587	8.99	5.64
3.18	2.156	7.80	3.134	5.61	527	0.598	8.93	5.64
6.35	2.153	8.07	3.46		601	0.571	9.35	6.26
3.18	2.118	8.04	3.49	5.82	591	0.566	9.35	6.26
6.35	2.164	8.31	3.52		625	0.571	9.43	6.44
3.18	2.162	8.37	3.50	5.86	633	0.582	9.43	6.44

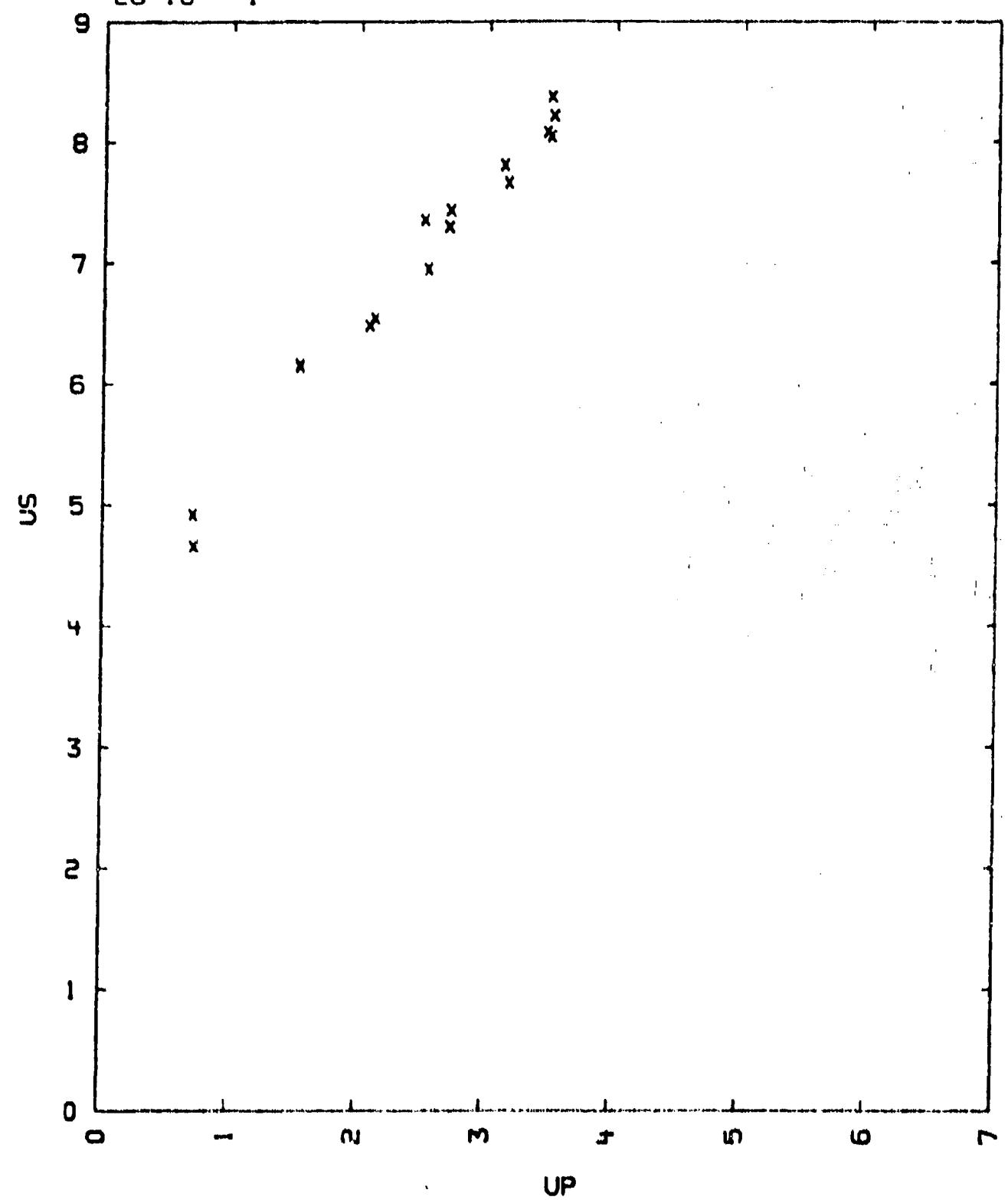
$$US = 3.82 + 1.54 \cdot UP - 0.088 \cdot UP^{1/2} \quad \text{SIGMA US} = 0.14 \text{ KM/SEC}$$

COMMENTS:

- 1) SOURCE: HORD, B. L.
PRIVATE COMMUNICATION (1966)
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA, USA.
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION TECHNIQUE B
STANDARD MATERIAL ALUMINUM 2024.
- 3) V_0 IS THE AVERAGE VOLUME OF ALL SAMPLES.
- 4) THE US-UP FIT WAS MADE WITH HEIGHTS OF 1.0 FOR THE 6.35-MM SAMPLES
AND HEIGHTS OF 0.5 FOR THE 3.18-MM-THICK SAMPLES.
- 5) THE SAMPLE MATERIAL HAS OBTAINED FROM HIGH TEMPERATURE MATERIALS,
INC., BRIGHTON, MASSACHUSETTS, USA.
- 6) V_{01} WAS CALCULATED FROM THE HEXAGONAL CELL STRUCTURE, WITH
 $a_0 = 0.50399$ AND $c_0 = 6.6612$ ANGSTROMS, AT 35 DEG. CENTIGRADE. THE
LATTICE CONSTANTS WERE OBTAINED FROM R. M. G. MYCKOFF, CRYSTAL
STRUCTURES, VOL. 1 (JOHN WILEY AND SONS, NEW YORK, N. Y., USA., 1965)
END ED.

TABLE I

BORON NITRIDE PYROLYTIC
28-18---1



28-18---2
BORON NITRIDE, PYROLYTIC.

B-N

$$V_0 = 0.459 \text{ CC}/\text{G}, \quad C_L = 2.743 \text{ KM}/\text{SEC}, \quad C' = 2.48 \text{ KM}/\text{SEC}, \\ V_{01} = 0.4389 \text{ CC}/\text{G}, \quad C_S = 1.048 \text{ KM}/\text{SEC}.$$

THE TABLE LISTS DENSITY IN G/CC., VELOCITIES IN KM/SEC. AND PRESSURE IN KBAR.

TABLE

RHO _G	U _S	U _P	P	V/V ₀
2.18	3.64	0.310	24.6	0.9148
-	3.62	0.309	24.4	0.9147
-	3.41	0.237	17.6	0.9304
-	3.43	0.234	17.5	0.9318
-	3.09	0.162	10.9	0.9475
-	2.86	0.077	4.8	0.9731
-	3.47	0.237	17.9	0.9314
-	3.47	0.239	18.1	0.9310
-	2.86	0.081	5.05	0.9717
-	2.86	0.083	5.20	0.9708

$$U_S = 2.58 + 3.50 \cdot U_P \text{ KM/SEC}$$

$$S10 \cdot U_S = 0.04 \text{ KM/SEC}$$

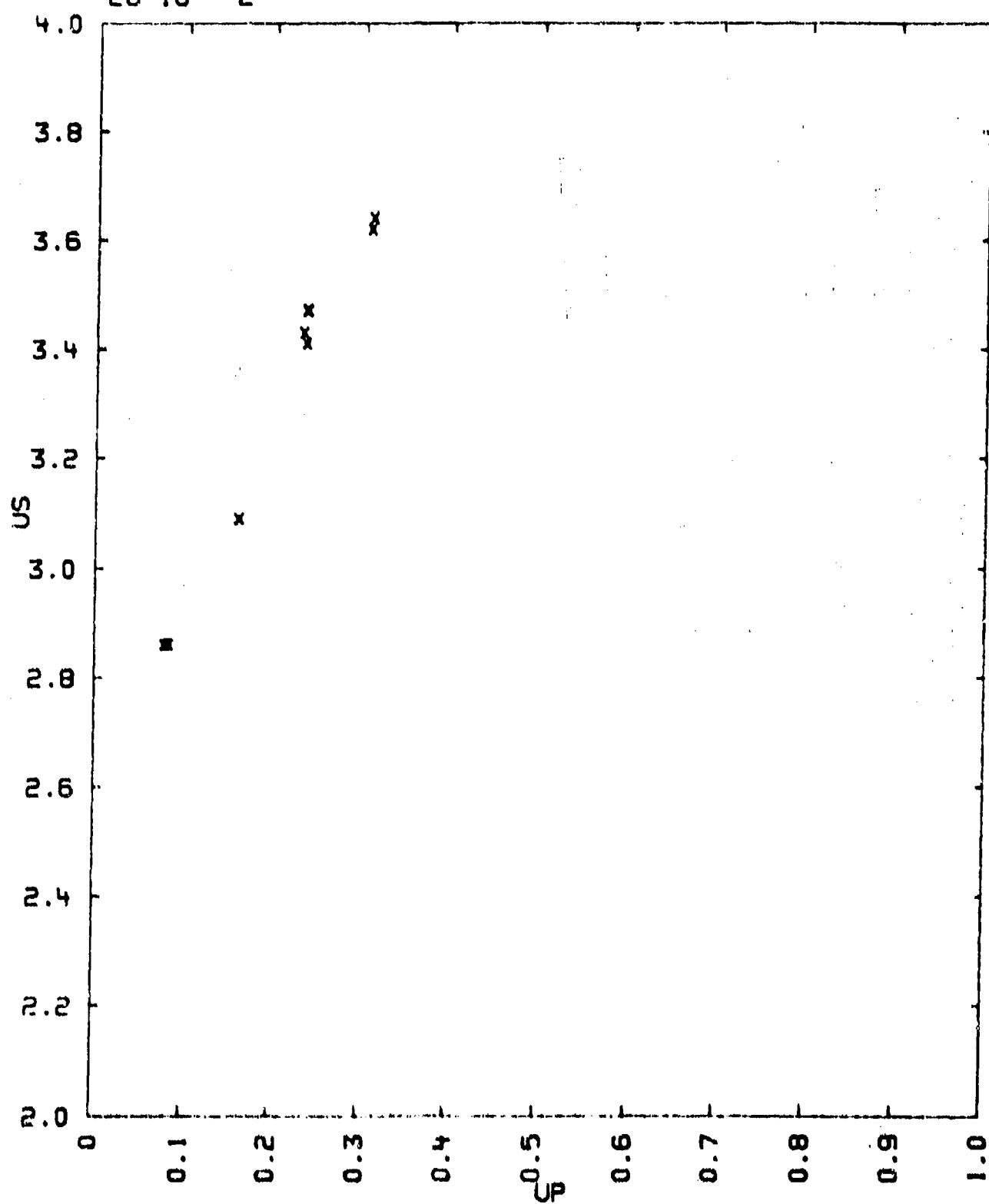
COMMENTS:

- 1) SOURCE: LEE L. H.
SANDIA LABORATORY REPORT SC-RR-2847 (1967)
SANDIA LABORATORY, ALBUQUERQUE, NEW-MEXICO, U.S.A.
- 2) EXPERIMENTAL TECHNIQUE: 12.
DATA REDUCTION TECHNIQUE: C (QUARTZ GAUGE)
- 3) THE SAMPLE FORMED PART OF THE BULLET AND IMPACTED THE QUARTZ GAUGE TO YIELD THE STRESS AT THE IMPACT SURFACE. IN THE REMAINING EXPERIMENTS THE GAUGE WAS PLACED ON THE SAMPLE SURFACE AND MEASURED TRANSMITTED PRESSURE. THEREFORE P AND U_P ARE THE MEASURED PARAMETERS IN THE FIRST 6 ENTRIES. P AND U_S WERE MEASURED IN ENTRIES 8 AND 10. U_S AND U_P (OBTAINED FROM THE PROJECTILE VELOCITY) WERE THE HUGONIOT PARAMETERS IN ENTRIES 7 AND 9.
- 4) NO WAVE ATTENUATION WAS OBSERVED HERE, BUT SEMISTATIC STRAIN RATE EXPERIMENTS SHOWED AN INCREASE OF 100 TO 110 BARS IN COMPRESSIVE STRESS BETWEEN STRAIN RATES OF 15 TO 10⁻³ INCH/(INCH SEC.)
- 5) THE SAMPLE IS POLYCRYSTALLINE WITH THE C AXIS OF THE CRYSTALLITES ORIENTED PERPENDICULAR TO THE SHOCK FRONT. SEE DATA SHEET FOR BORAL-LAY, FEB. 1 1965, HIGH TEMP MATERIALS INC., UNION CARBIDE CORP., LOVELL, MASS., U.S.A.
- 6) V_{O1} AS IN ENTRY 28-18---1

TABLE I

BORON NITRIDE, PYROLYTIC.

28-18---2



28-18---3

BORON NITRIDE, POROUS, ((PIN))

B-N

GRAIN SIZE 20 TO 100 ANGSTROM.

 $V_0 = 0.794 \text{ CC/G.}$ $V_{01} = 0.4389 \text{ CC/G.}$ THE TABLE LISTS DENSITY IN G/CC., VELOCITIES IN KM/SEC. AND PRESSURE
IN KBAR.

TABLE

RHO0	US1	UPI	P1	V1/V0	US2	UP2	P2	V2/V0
1.26	2.77	0.043	1.5	0.984	1.45	0.525	10.2	0.648
-	-	-	-	-	1.37	0.487	9.05	0.655
-	-	-	-	-	1.28	0.444	7.88	0.668
-	-	-	-	-	1.09	0.401	6.30	0.648
-	-	-	-	-	1.01	0.335	5.11	0.686
-	-	-	-	-	0.86	0.272	3.91	0.710
-	-	-	-	-	1.03	0.145	2.79	0.882
-	-	-	-	-	0.92	0.203	3.30	0.805
-	-	-	-	-	1.27	0.110	2.45	0.930

$$US2 = 2.03 + 2.57 \cdot UP \text{ KM/SEC.}$$

$$510 \cdot US2 = 0.04 \text{ KM/SEC. FOR UP BETWEEN } .27 \text{ AND } .35 \text{ KM/SEC.}$$

$$US2 = 2.77 - 19.1 \cdot UP + 49.0 \cdot UP^2 \text{ KM/SEC.}$$

$$510 \cdot US2 = 0.007 \text{ KM/SEC. FOR UP BELOW } 0.20 \text{ KM/SEC.}$$

COMMENTS:

- 1) SOURCE: LEE L. M.
 SANDIA LABORATORY REPORT SC-HR-68-2 (1968)
 SANDIA LABORATORY, ALBUQUERQUE, NEW MEXICO, U.S.A.
- 2) EXPERIMENTAL TECHNIQUE: 12
 DATA REDUCTION TECHNIQUE: C
- 3) BOTH STRESS PROFILES TRANSMITTED THROUGH THE SAMPLE AND INPUT STRESS
 WERE MEASURED. THE FORMER SHOWED A BROAD PRECURSOR PROFILE WHICH HAS
 INTEGRATED ASSUMING CONSTANT VELOCITY FOR EACH STRESS POINT, TO YIELD
 THE APPROPRIATE MAXIMUM COMPRESSION AND UPI. V2/V0 AND US2 WERE
 THEN CALCULATED FROM THE INPUT STRESS (P2) AND PARTICLE VELOCITY
 (UP2). USING THE JUMP CONDITIONS, WHICH WERE ALSO USED TO CALCULATE
 US1 IN THE TABLE. THE MEASURED VELOCITY AT THE FOOT OF THIS BROAD
 WAVE WAS 3.30 ± 0.18 KM/SEC. THE VALUE OF US1 IN THE TABLE IS THE
 EFFECTIVE VALUE THAT FITS THE JUMP CONDITIONS.
- 4) THE MAXIMUM UNCERTAINTY IN P IS NEAR 5 PERCENT. THE AGREEMENT BETWEEN
 A CALCULATED US2 AND A AVERAGE SHOCK PROFILE VELOCITY CAME TO 3 PER-
 CENT: 1.29 CALC. AND 1.33 KM/SEC. MEASURED.
- 5) THE SAMPLE HAS ISOTROPIC PYROLYTIC BORON NITRIDE, IMPERMEABLE TO HE
 AT ONE ATMOSPHERE DIFFERENTIAL ACROSS A 0.08 CM SLAB.
 IT WAS PRODUCED BY RAYTHEON CORPORATION.

TABLE I

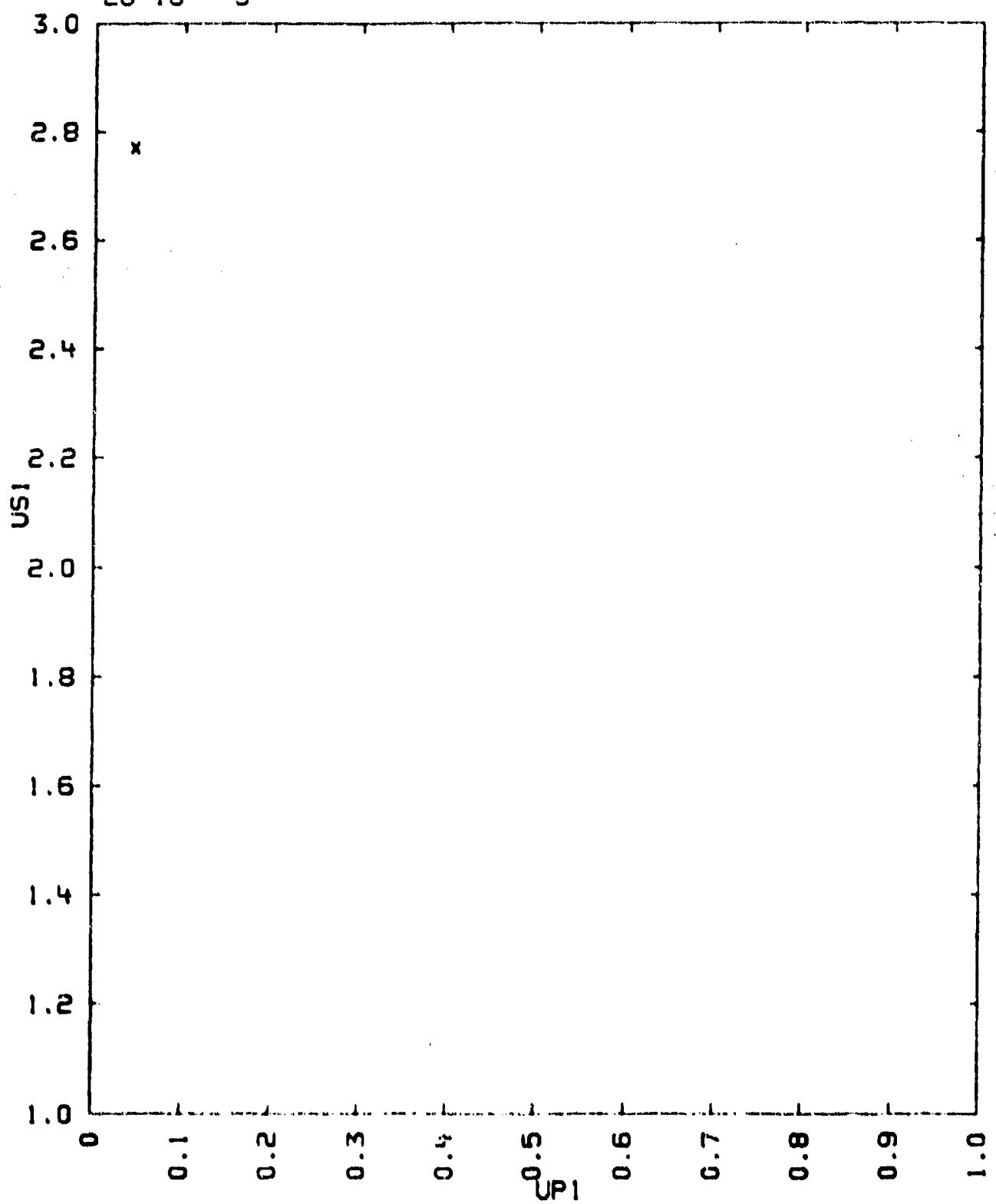
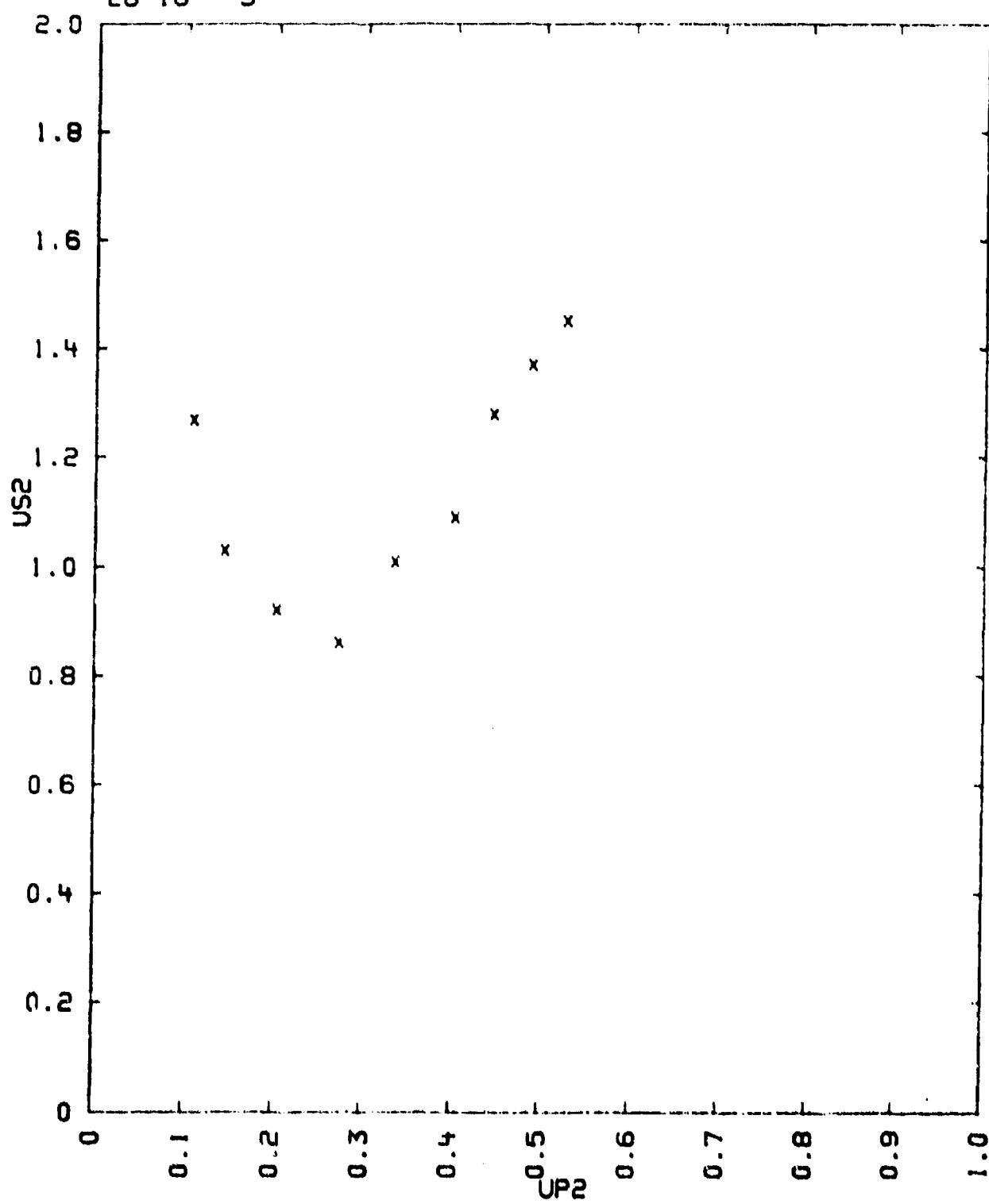
BORON NITRIDE, POROUS. (IPBN)
28-18---3

TABLE I

BORON NITRIDE, POROUS. (IPBN)
28-18---3



20-18---4

BORON NITRIDE, PYROLYTIC

B-N

$$V_0 = 0.459-0.476 \text{ CC/G} \quad C_L = 2.743 \text{ KM/SEC} \quad C_0 = 2.462 \text{ KM/SEC.}$$

$$V_0 = 0.4389 \text{ CC/G} \quad C_S = 1.648 \text{ KM/SEC}$$

THE TABLE LISTS DENSITY IN G/CC., VELOCITIES IN KM/SEC AND PRESSURE IN KBAR.

TABLE

RHO0	US	UP	P	V/V0
2.18	6.441	2.298	322.7	0.643
2.08	6.54	2.14	291.	0.67
2.12	6.47	2.07	265.	0.68
2.18	6.093	2.047	271.9	0.664
2.18	6.059	2.051	270.9	0.661
2.12	6.10	1.81	237.	0.70
2.149	5.91	1.63	206.0	0.72
2.149	5.71	1.40	171.0	0.76
2.149	5.63	1.38	167.0	0.76
2.10	5.371	1.468	165.6	0.727
2.12	5.59	1.40	166.	0.75
2.18	5.568	1.345	163.3	0.758
2.149	5.36	1.07	123.0	0.80
2.18	5.086	1.032	114.4	0.797
2.18	5.070	1.033	114.2	0.796
2.149	4.843	0.802	83.5	0.834
2.149	4.776	0.804	82.6	0.832
2.15	4.42	0.79	75.	0.82
2.12	4.57	0.77	74.	0.83
2.12	4.011	0.707	73.6	0.856
2.12	4.786	0.719	73.0	0.850
2.10	4.404	0.672	62.2	0.847
2.149	4.406	0.483	43.9	0.895

$$US = 3.83 + 1.20 \cdot UP \text{ KM/SEC}$$

$$\text{SIG US} = 0.17 \text{ KM SEC.}$$

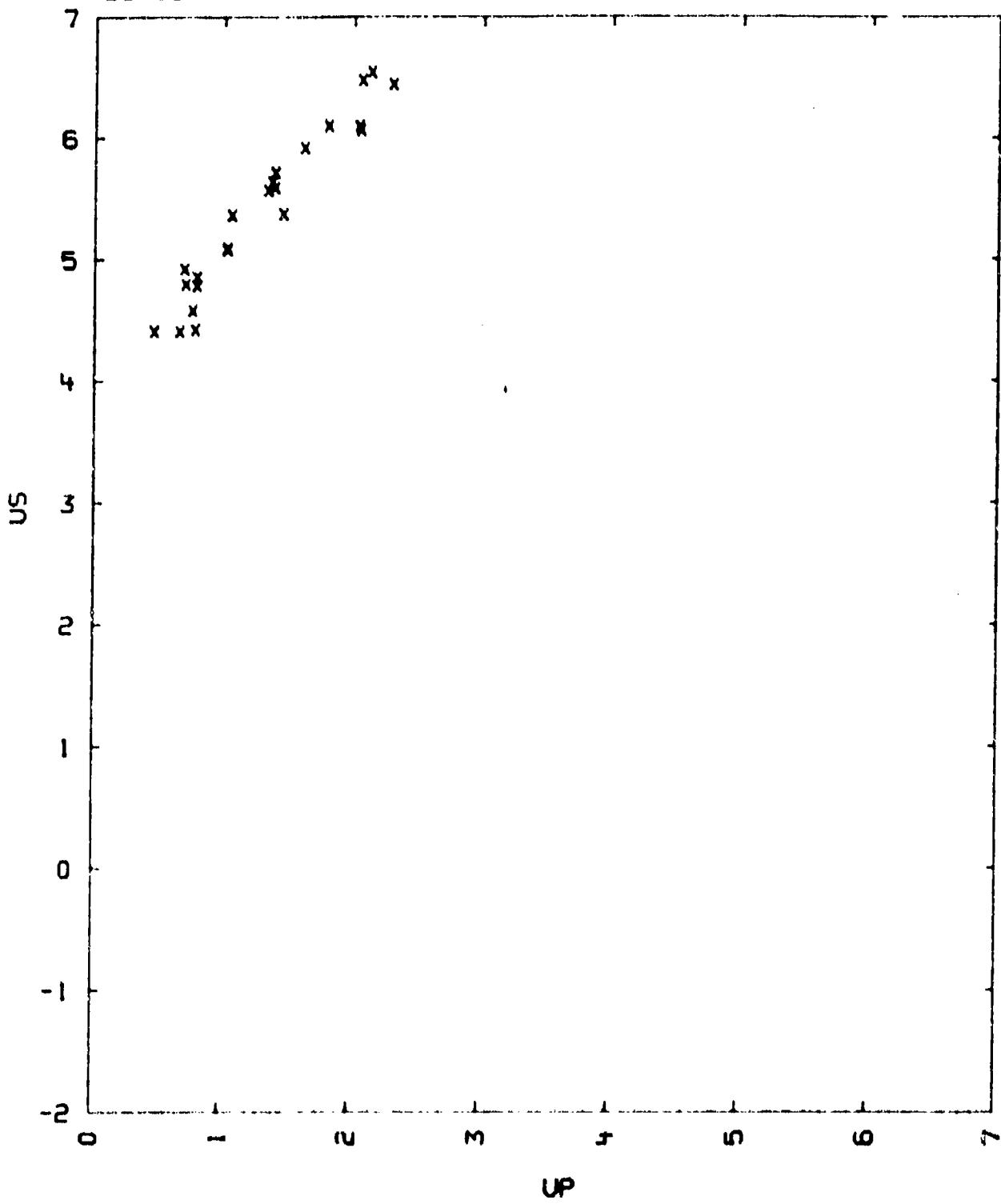
COMMENTS

- 1) SOURCE: MAY, R. P. AND KINSEY, C. H.
SANDIA LABORATORY REPORT SC-TM-67-534, JULY 1967.
SANDIA CORP., ALBUQUERQUE, NEW MEXICO
- 2) EXPERIMENTAL TECHNIQUE: A
DATA REDUCTION METHOD: B
- 3) POLYCRYSTALLINE, PURE HEXAGONAL BORON NITRIDE FROM CARRIAGE PRODUCTS
DIV OF UNION CARBIDE CORP. SAME MATERIAL AS 20-18---2
- 4) CL, CS AND CO MEASURED ALONG THE CRYSTALLOGRAPHIC C AXIS.
T. GUESS AND S. W. KEY, ELASTIC CONSTANTS AND GRUENFELD TENSOR FOR

PYROLYtic BORON NITRIDE. MEMO TO DISTRIBUTION, FEB. 28 (1967)
SANDIA LABORATORY, ALBUQUERQUE, NEW MEXICO, U.S.A.
5) VCI WAS CALCULATED AS IN 2B-1R---1
6) PRELIMINARY DATA. WORK IN PROGRESS.

U06/14/77

TABLE I

BORON NITRIDE, PYROLYTIC
28-18---4

2B-23---1
BORON CARBIDE

B₄C

$$V_0 = 0.5051 - 5.294 \text{ CC/G}$$

$$V_{01} = 0.4011 \text{ CC/G}$$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBARS AND DENSITY IN G/CC.

TABLE

-----SAMPLE-----					-----STANDARD-----		
RHO0	US	UP	P	V/V0	MATERIAL	US(ST)	
1.980	5.46	1.47	159.	0.7308	2024 AL	6.90	
1.978	5.72	2.10	275.	0.6873	2024 AL	6.75	
1.974	7.03	2.30	311.	0.6728	2024 AL	7.88	
1.970	7.77	2.50	383.	0.6782	2024 AL	8.19	
1.969	7.50	2.62	371.	0.6507	2024 AL	8.24	
1.944	8.43	2.90	475.	0.6560	2024 AL	8.67	
1.937	9.02	3.22	563.	0.6430	2024 AL	9.08	
1.903	9.01	3.38	581.	0.6449	2024 AL	9.22	
1.940	9.45	3.58	653.	0.6253	2024 AL	9.48	
1.903	9.78	3.94	733.	0.5971	2024 AL	9.88	

$$US = 1.506 + 2.943 \cdot UP - 0.207 \cdot UP^{1/2} \text{ KM/SEC}$$

$$\text{SIG US} = 0.18 \text{ KM/SEC}$$

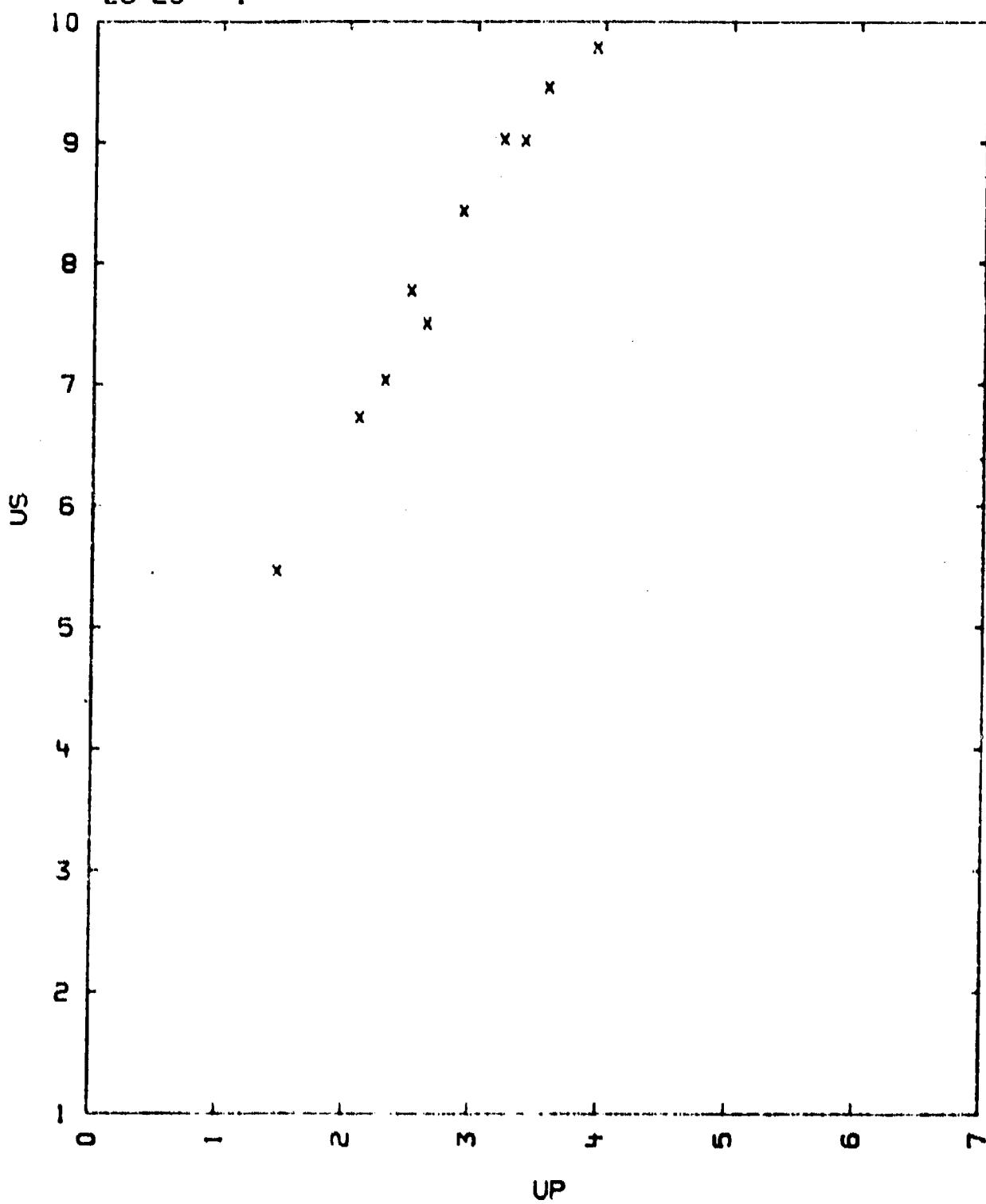
COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.H., FRITZ, J.M., AND CARTER, W.J.
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,
HIGH VELOCITY IMPACT PHENOMENA, KINGMAN (ED.), (ACADEMIC
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B
DATA REDUCTION TECHNIQUE: B (STANDARD BASE PLATE AS SHOWN)
- 3) V01 IS CALCULATED FROM THE HEXAGONAL CELL CONSTANTS A0 = 5.60 AND
C0 = 12.12 ANGSTROM. CRYSTAL DATA DETERMINATIVE TABLES, ED. J.D.H.
DONNAY AND H.M. ONDIK (U.S. DEP. OF COMM., N.B.S., MD., 1973) SRD. ED

006/14/77

TABLE I

BORON CARBIDE
28-23---1



29-1---1

CORUNDUM (ALUMINUM OXIDE CRYSTALLINE)

AL2-03

$$V_0 = 0.2506 \text{ CC}/\text{G}$$

$$V_{01} = 0.2515 \text{ CC}/\text{G}$$

$$C_0 = 7.93 \text{ KM}/\text{SEC.}$$

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBOARS AND DENSITY IN G/CC. ST DESIGNATES THE STANDARD SAMPLE HOLDER MATERIAL.

TABLE

RHO0	US	UP	P	V/V0	US(ST)
3.98	9.99	1.30	516	0.869	7.72
3.98	10.51	1.66	693	0.841	8.32
3.99	11.02	1.98	871	0.821	8.86
3.99	11.17	2.20	979	0.804	9.18
3.99	11.28	2.24	1006	0.803	9.26
3.99	11.24	2.27	1016	0.800	9.29
3.99	11.03	2.32	1019	0.790	9.33
3.99	11.81	2.78	1309	0.766	10.08
3.99	11.78	2.80	1315	0.763	10.11
3.99	11.69	2.95	1376	0.749	10.29
3.98	11.92	3.11	1480	0.738	10.54

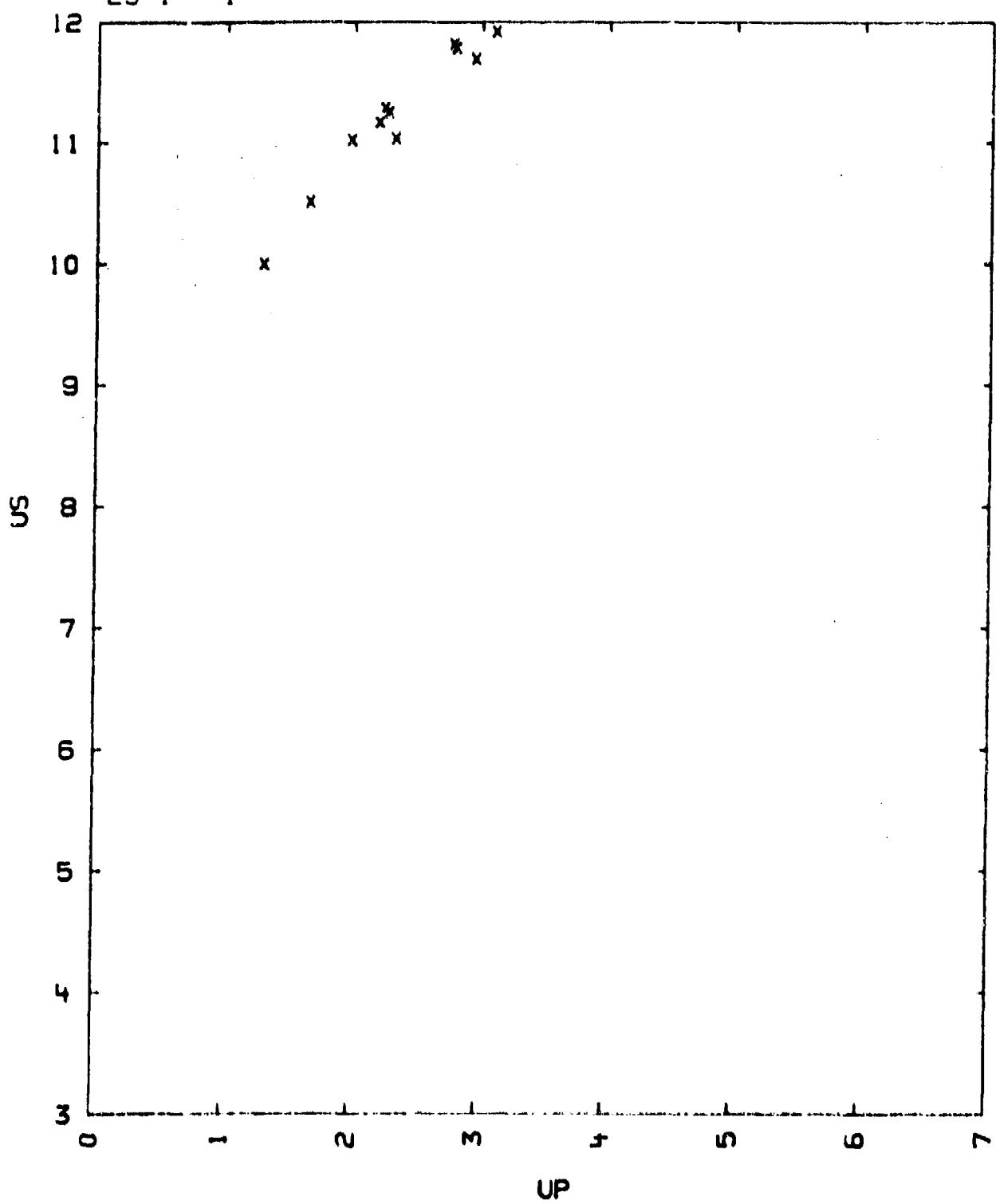
$$US = 7.916 + 1.897 \cdot UP - 0.195 \cdot UP^2 - 2 \text{ KM}/\text{SEC.}$$

$$\text{SIGMA US} = 0.12 \text{ KM}/\text{SEC.}$$

COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.
PRIVATE COMMUNICATION
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION METHOD B - STANDARD MATERIAL 2024 ALUMINUM
- 3) V01 WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED BY HYCKOFF,
CRYSTAL STRUCTURES, VOL. 2 (JOHN WILEY AND SONS, NEW YORK 1963)
- 4) FURTHER WORK IS IN PROGRESS.

TABLE I
CORUNDUM (ALUMINUM OXIDE CRYSTALLINE)
29-1---1



29-1--2
CORUNDUM (ALUMINUM OXIDE CERAMIC)

AL2-03

$$V_0 = 0.2611 \text{ CC/O}$$

$$V_{01} = 0.2515 \text{ CC/O}$$

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE STANDARD SAMPLE HOLDER MATERIAL.

TABLE

RHO0	US	UP	P	V/V0	US1ST1
3.83	8.63	0.94	310	0.891	7.00
3.83	8.68	1.22	405	0.859	7.42
3.83	8.92	1.37	469	0.845	7.67
3.83	9.43	1.76	635	0.813	8.29
3.83	9.62	1.77	653	0.815	8.32
3.83	9.56	1.78	652	0.813	8.32
3.83	10.26	2.21	870	0.783	9.01
3.83	10.27	2.31	909	0.774	9.15
3.83	11.17	2.90	1240	0.741	10.06
3.83	11.25	3.03	1312	0.731	10.29

$$US = 6.956 + 1.449 \cdot UP \text{ KM/SEC.}$$

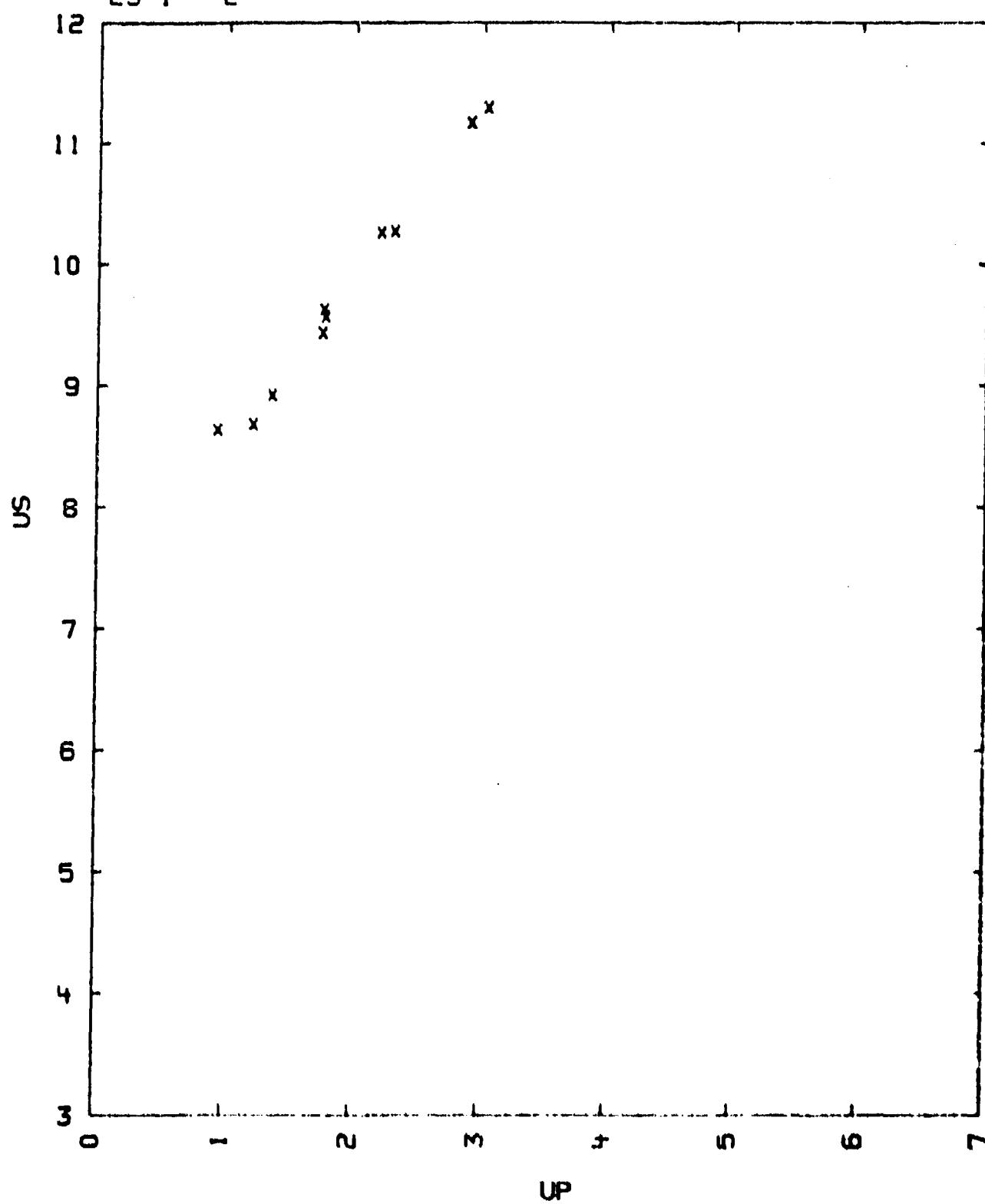
$$\text{SIGMA US} = 0.069 \text{ KM/SEC.}$$

COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.
PRIVATE COMMUNICATION
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) V01 WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED BY WYCKOFF.
CRYSTAL STRUCTURES, VOL. 2 (JOHN WILEY AND SONS, NEW YORK 1963)
- 4) FURTHER WORK IS IN PROGRESS.

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TABLE I

CORUNDUM (ALUMINUM OXIDE CERAMIC)
29-1---2

29-1---3

ALUMINUM OXIDE, CERAMIC

HE500 AL-995 (TABLE III)

AL2-03 99.5 WT. PERCENT MINIMUM
 MG-0 MAJOR IMPURITY
 SI-02 -
 POROSITY 3.5-4.3 PERCENT MAX

LUCALOX (TABLE III):

AL2-03 99.8 WT. PERCENT
 POROSITY 0.2 PERCENT MAX

$$V_0 = 0.2513 - 0.2626 CC/0 \quad CL = 10.3 \text{ KM/SEC} \quad C_D = 7.55 \text{ KM/SEC}$$

$$V_{01} = 0.2515 \text{ CC/0} \quad CS = 6.12 \text{ KM/SEC.}$$

IN THE TABLES BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN KM/SEC., AND PRESSURE IN KILOBARS. BP DENOTES THE BASE PLATE MATERIAL. SUBSCRIPTS 1 AND 2 DENOTE THE ELASTIC WAVE AND THE FIRST SHOCK WAVE RESPECTIVELY.

TABLE I

RHO0	US1	UP1	P1	V1/V0	US2	UP2	P2	V2/V0	BP
3.814	10.07	0.26	100.	0.974	6.75	0.29	107.	0.970	LU
3.810	10.38	0.21	84.	0.980	7.83	0.31	113.	0.967	LU
3.814	10.32	0.20	79.	0.981	7.26	0.87	263.	0.893	AL
3.809	9.82	0.18	67.	0.982	7.54	0.05	259.	0.895	AL
3.810	10.07	0.22	85.	0.978	8.62	1.28	432.	0.857	AL
3.809	10.05	0.21	81.	0.979	8.59	1.26	424.	0.858	AL
3.837					11.03	2.677	1131.	0.756	BR
3.839					10.9	2.687	1121.	0.753	BR
3.808					9.08	1.36	736.	0.802	AL

$$US = 6.43 + 1.70 \cdot UP - 0.32 \cdot UP^{+2} \text{ KM/SEC} \quad \text{SIGMA US} = 0.08 \text{ KM/SEC}$$

TABLE II

SAMPLE										STANDARD	
RHO0	US1	UP1	P1	V1/V0	US2	UP2	UFS2	P2	V2/V0	BP	UFS
3.98	10.98	0.368	161.	0.9663	9.80	0.477	1.174	199.	0.9544	AL	1.543
-	-	0.262	114.	0.9759	8.79	0.495	0.974	195.	0.9497	-	-
-	10.90	0.284	123.	0.9739	8.53	0.495	0.957	195.	0.9492	-	-
-	10.98	0.253	111.	0.9771	9.60	0.93	1.67	369.	0.9062	-	2.694
-	10.88	0.229	99.	0.9791	9.36	0.90	1.57	386.	0.9003	-	-

US =

COMMENTS:

(1) SOURCE: AHRENS T.J., GUST H.H. AND ROYCE E.B.

J. APPL. PHYS., VOL. 39, P. 4610, (1968)

2) EXPERIMENTAL TECHNIQUE C1 WAS USED FOR ALL ENTRIES EXCEPT FOR THE LAST ENTRY OF TABLE I, WHICH HAS OBTAINED WITH TECHNIQUE B

DATA REDUCTION TECHNIQUE D UFS-2-UP. TABLE I, FIRST 6 ENTRIES

B TABLE I, LAST 3 ENTRIES AND TABLE II

BASE PLATE MATERIALS: LUCITE(LU), 2024 ALUMINUM(Al) AND LOW LEAD
BRASS(BR)

3) SAMPLE MATERIALS: WESGO AL-995, TABLE I (WESTERN GOLD AND PLATINUM CO.
BELMONT, CALIF., USA.)

LUCALOX, TABLE II (GENERAL ELECTRIC CO., OHIO)

4) CL AND CS ABOVE ARE FOR WESGO AL-995 (H. DUNEGAN, PRIVATE COMMUNICATION, (1968))

CL = 10.845 KM/SEC FOR LUCALOX (E. SCHREIBER AND O. L. ANDERSON, J. AM. CER SOC., VOL. 46, P. 184, (1963))

5) VOL WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED BY WYCKOFF,
CRYSTAL STRUCTURES, VOL. 2 (JOHN WILEY AND SONS, NEW YORK, N. Y.,
USA, 1963).

6) THE DATA OF TABLE II WHICH WERE TAKEN WITH 3.2 TO 12.7 MM. THICK SAMPLES INDICATE 4 TO 5 KBAR DECAY OF SHOCK STRENGTH OVER THAT THICKNESS RANGE.

7) * INDICATES LESS RELIABLE DATA ON THE SECOND HAVE WHICH WERE NOT USED IN FIT.

TABLE I

ALUMINUM OXIDE, CERAMIC

29-1---3

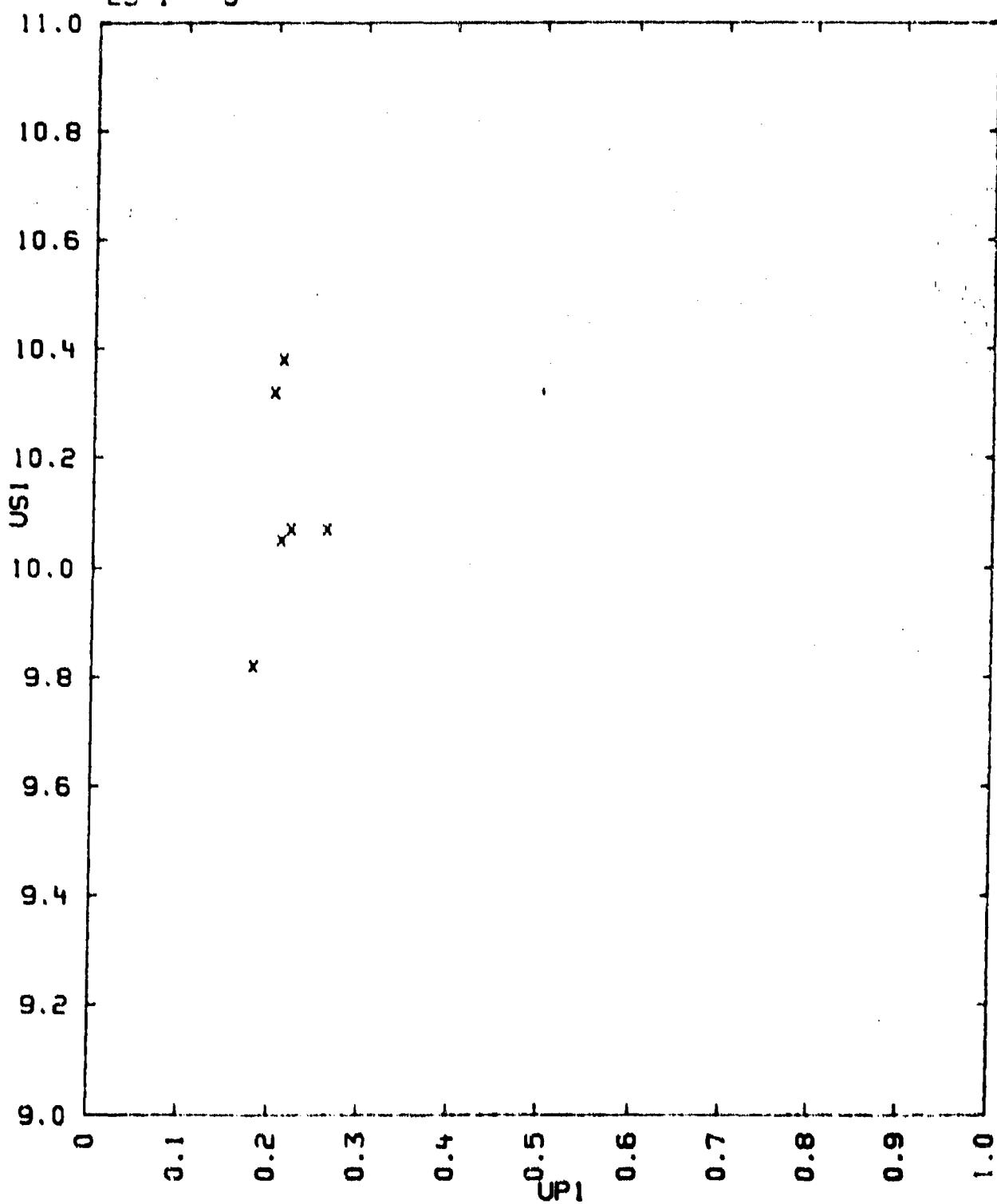


TABLE I
ALUMINUM OXIDE, CERAMIC
29-1---3

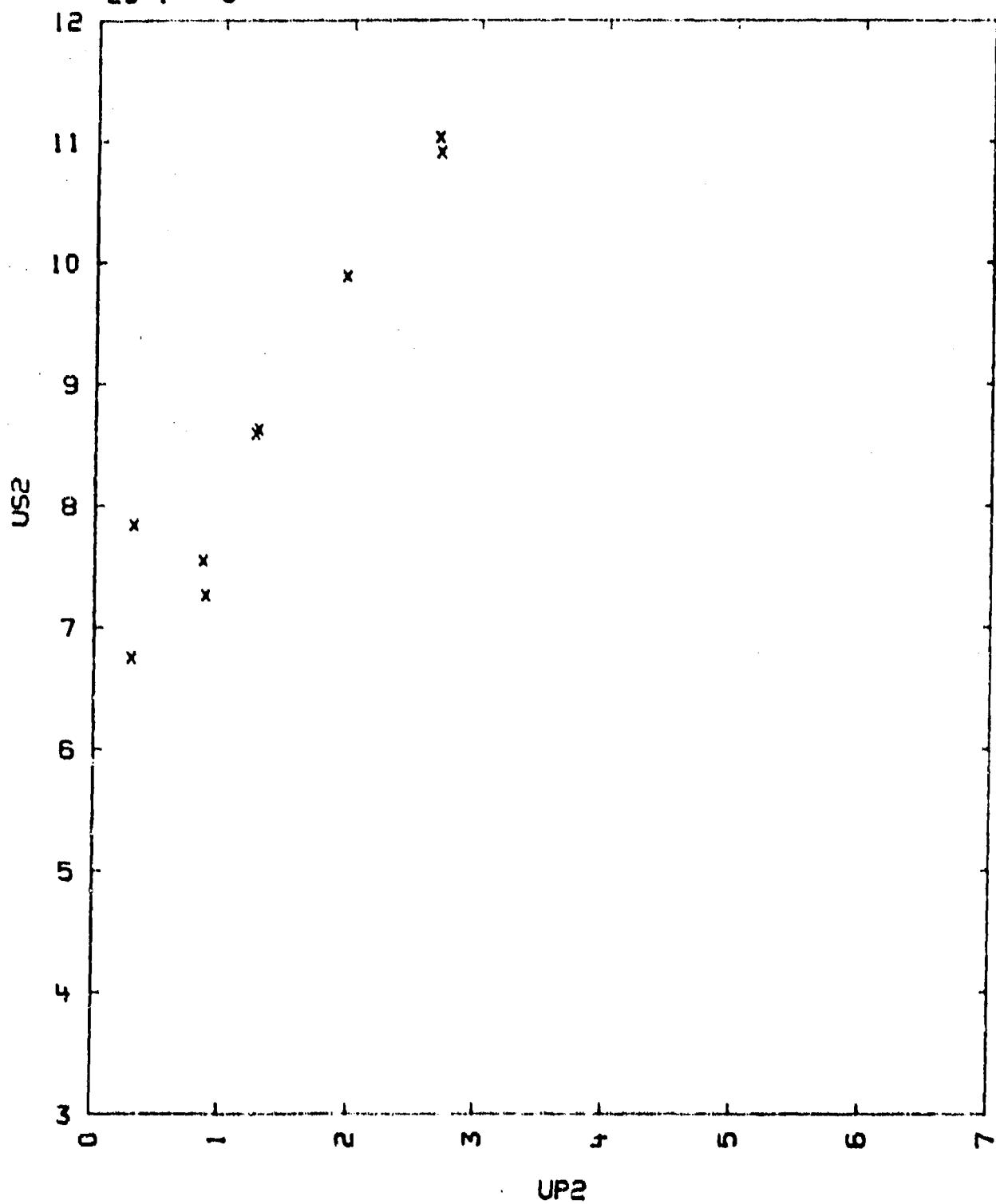


TABLE II

ALUMINUM OXIDE, CERAMIC

29-1---3

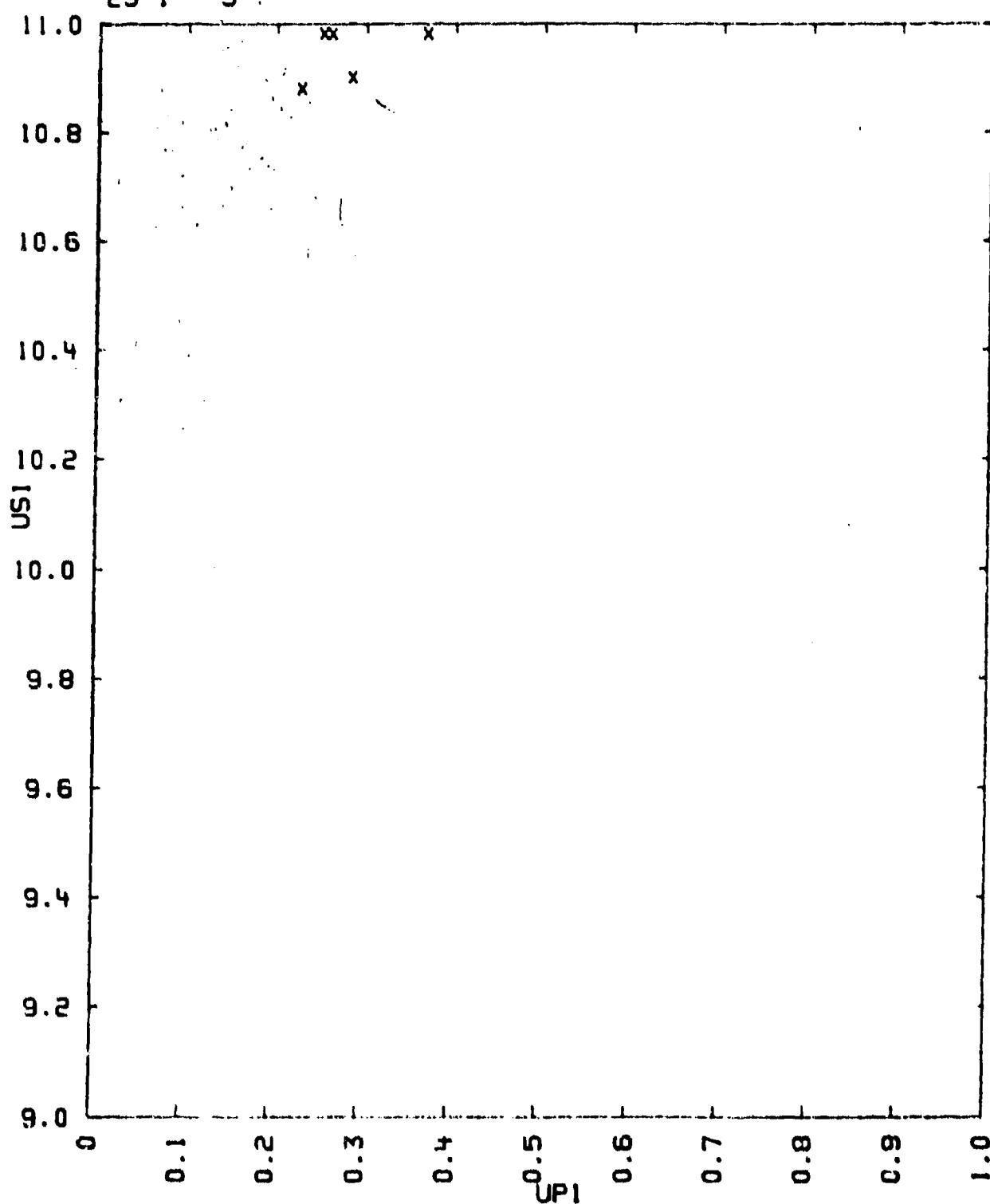
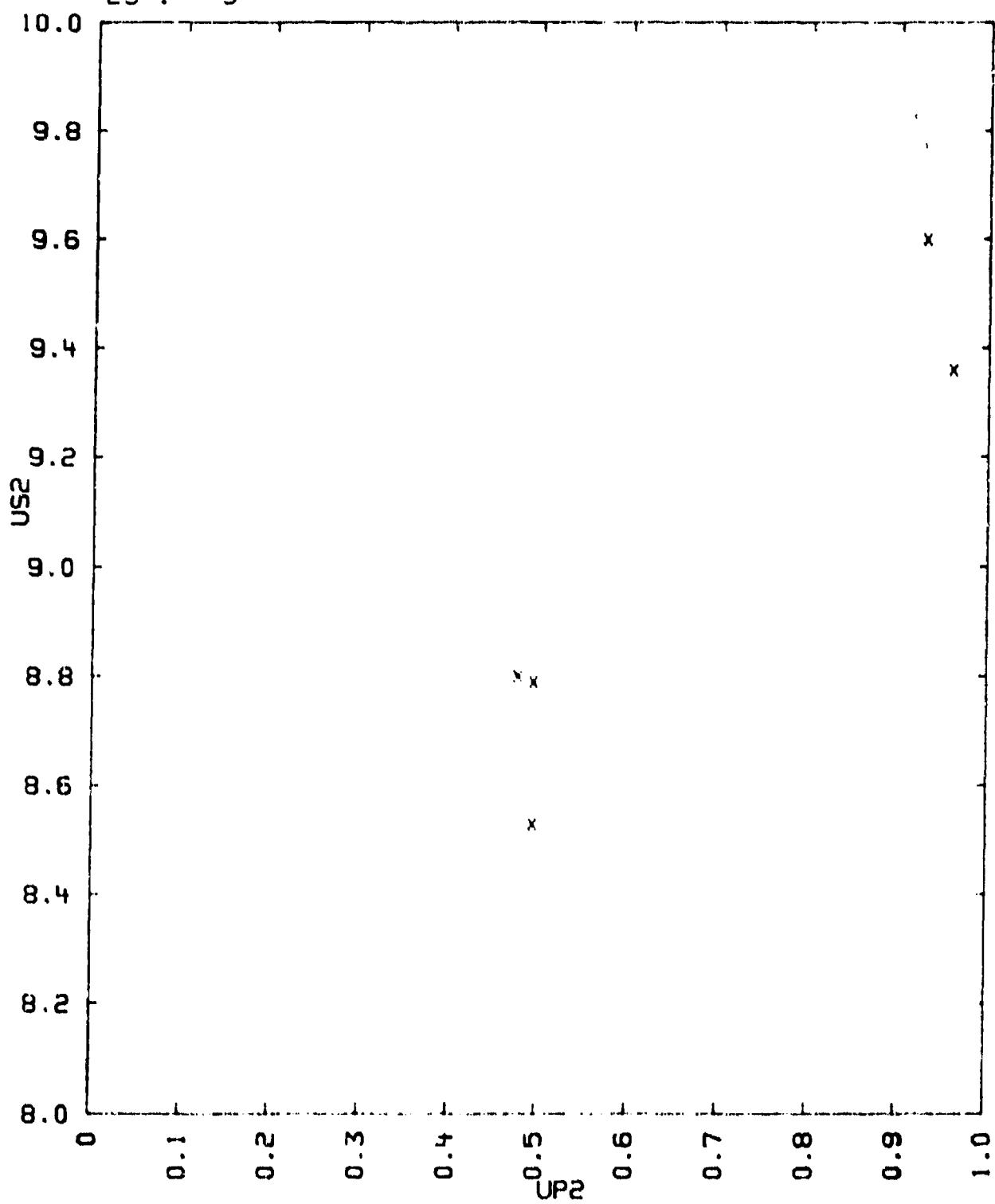


TABLE II

ALUMINUM OXIDE, CERAMIC
29-1---3

29-24-1---1

ANDALUSITE NATURAL (ALUMINUM SILICATE)

AL2-SI-05

$$V_0 = 0.325 \text{ CC/G}$$

$$V_{01} = 0.318 \text{ CC/G}$$

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE SAMPLE HOLDER AND STANDARD MATERIAL.

TABLE

RHO0	US	UP	P	V/V0	US(ST)
3.08	7.74	2.49	594	0.678	8.68
3.06	7.91	2.53	613	0.688	8.75
3.10	7.94	2.67	657	0.694	8.93
3.07	7.94	2.76	673	0.687	9.02
3.06	7.94	2.68	701	0.683	9.16
3.09	8.32	2.97	763	0.690	9.33
3.06	8.04	3.20	867	0.683	9.67
3.08	9.20	3.50	993	0.683	10.08
3.07	9.36	3.63	1042	0.668	10.25
3.06	9.59	3.65	1049	0.667	10.27
3.09	9.52	3.70	1089	0.572	10.37
3.04	9.87	3.80	1158	0.572	10.54

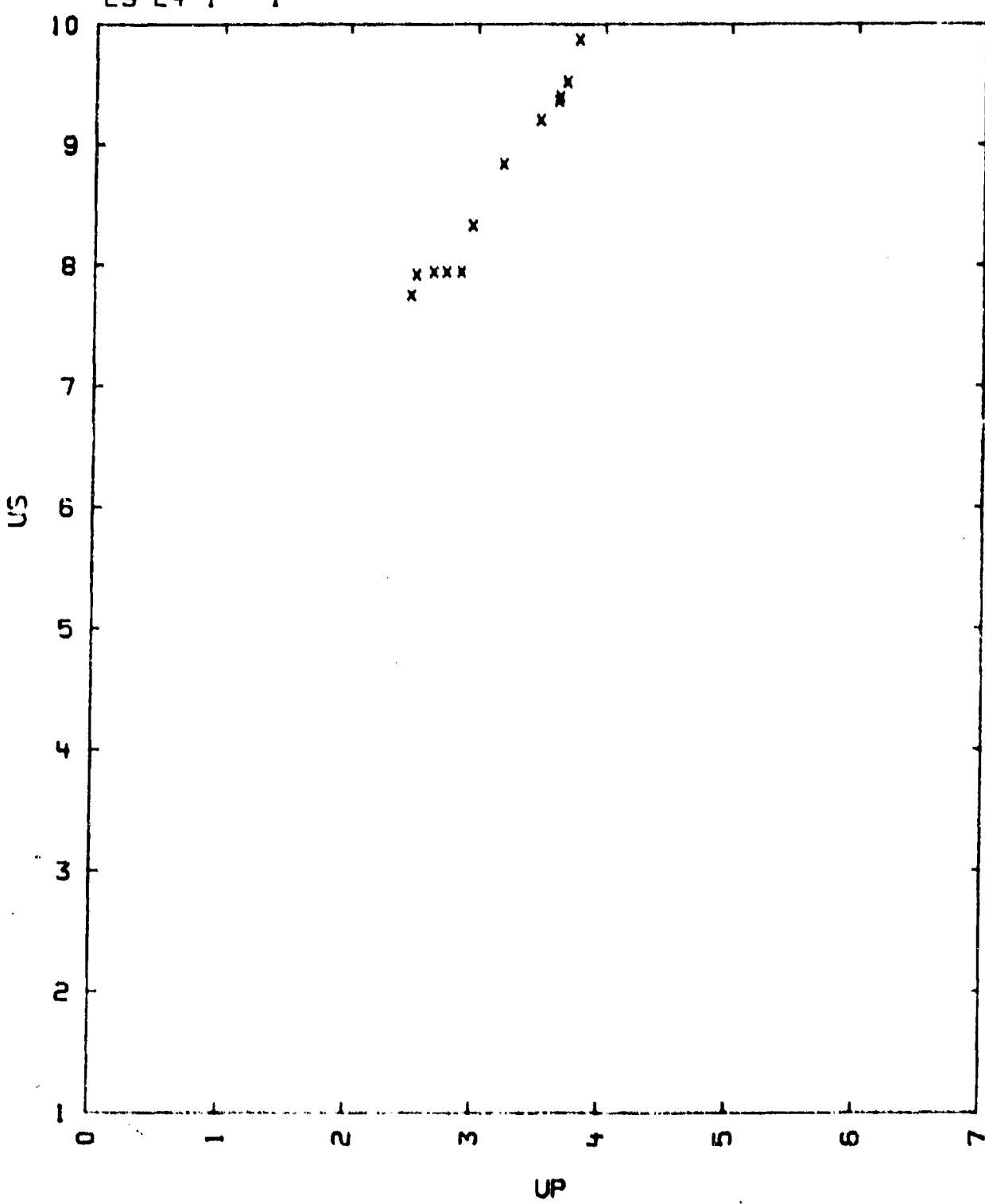
$$US = 2.869 + 1.811 \cdot UP \text{ KM/SEC.}$$

$$SIUNA US = 0.12 \text{ KM/SEC.}$$

COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.
 PRIVATE COMMUNICATION
 LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE: B
 DATA REDUCTION METHOD: B STANDARD MATERIAL 20% ALUMINUM
- 3) V01 WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED IN CRYSTAL DATA DETERMINATIVE TABLES (AMERICAN CRYST. ASSN. MONOGRAPH 5, 1963) AND LD
- 4) FURTHER WORK IN PROGRESS

TABLE I
ANDALUSITE NATURAL (ALUMINUM SILICATE)
29-24-1---1



29-24-1---2
SILLIMANITE (ALUMINUM SILICATE)

AL2-51-05

$$V_0 = 0.319 \text{ CC/G}$$

$$V_{01} = 0.3080 \text{ CC/G}$$

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE SAMPLE HOLDER AND STANDARD MATERIAL.

TABLE

RHO0	US	UP	P	V/V0	US(ST)
3.07	7.54	2.52	584	0.686	8.68
3.12	7.83	2.52	616	0.678	8.75
3.13	8.01	2.65	664	0.670	8.93
3.13	8.05	2.70	680	0.665	9.00
3.10	7.94	2.75	676	0.654	9.02
3.09	8.15	2.84	715	0.652	9.16
3.13	8.48	2.93	778	0.655	9.33
3.13	8.89	3.16	881	0.644	9.67
3.15	9.29	3.45	1012	0.627	10.08
3.13	9.42	3.59	1080	0.619	10.25
3.13	9.55	3.68	1099	0.615	10.37

$$US = 3.58 + 1.64 \cdot UP \text{ KM/SEC.}$$

$$\text{SIGMA US} = 0.11 \text{ KM/SEC.}$$

COMMENTS :

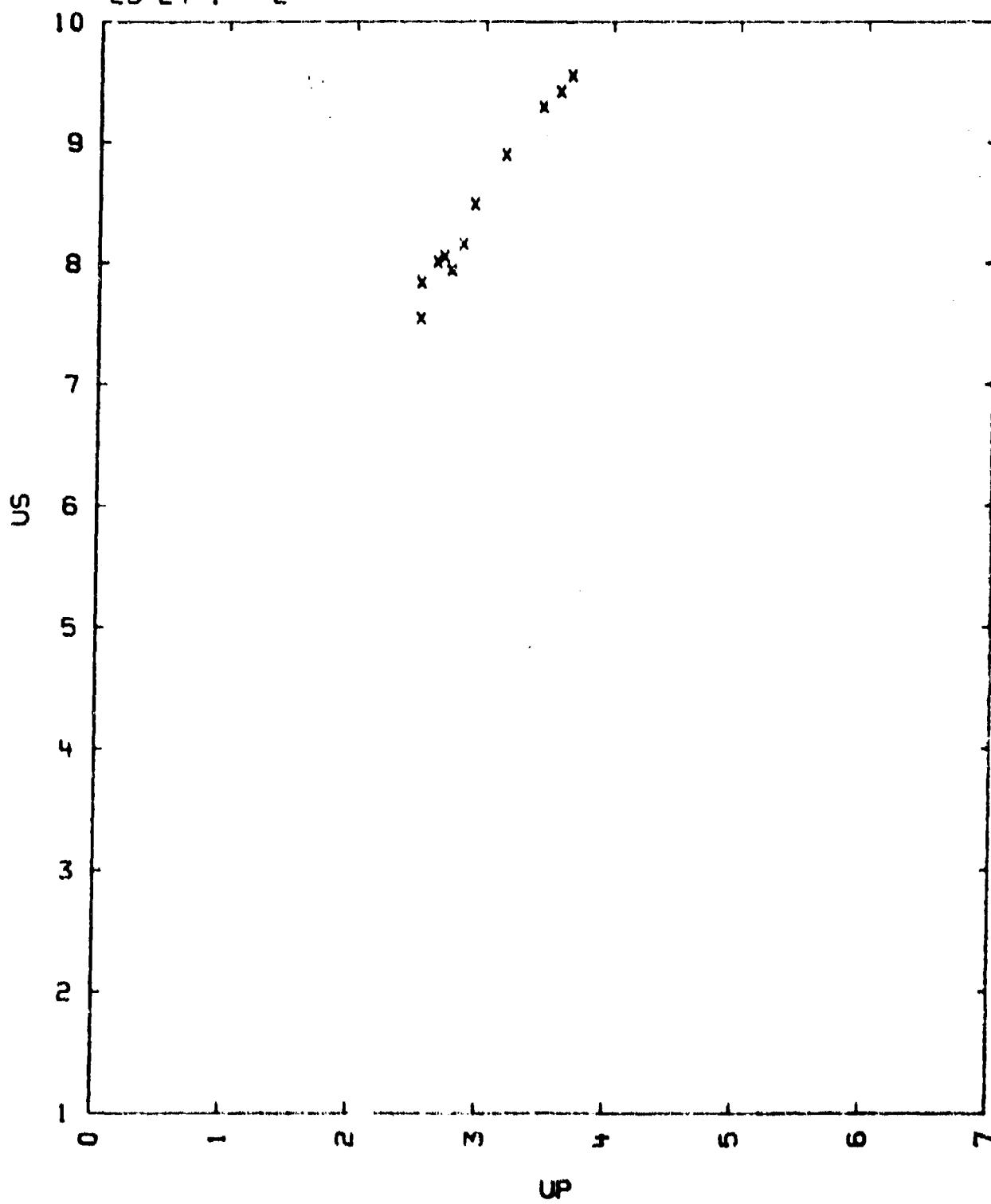
- 1) SOURCE : MCQUEEN R.G. AND MARSH S.P.
PRIVATE COMMUNICATION
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) V01 HAS OBTAINED FROM THE DENSITY LISTED IN THE HANDBOOK OF CHEM. AND PHYS. (THE CHEMICAL PUBLISHER CO., CLEVELAND 1964-1965) 45TH ED.
- 4) FURTHER WORK IN PROGRESS

106/14/77

TABLE I

SILLIMANITE (ALUMINUM SILICATE)

29-24-1---2



33-27-1---1
LEAD ZIRCONATE

PB-ZR-03 WITH NB AND Ti DOPING :
 LEAD Pb 0.987 MOLE PER 3 MOLE OXYGEN
 ZIRCONIUM ZR 0.927 - - - - -
 NIOBIUM Nb 0.025 - - - - -
 TITANIUM Ti 0.048 - - - - -

$V_0 = 0.127 - 0.130 \text{ CC}/\text{G}$ $C_L = 3.93 - 4.27 \text{ KM}/\text{SEC}$
 $V_{01} = 0.1225 \text{ CC}/\text{G}$

THE TABLES LIST DENSITY IN G/C, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS. D = THICKNESS IN MM. EM = EXPERIMENTAL METHOD. MAT = MATERIAL.

TABLE I

EXPNO	D	US1	UP1	US2	UP2	EM
8413	12.5	4.14	0.123	3.5	0.235	C2
8445	8.7	4.28	0.127			C2
8662	12.5			4.15	0.448	C2
8468	5.3			4.24	0.435	C2
8703	5.1	4.38	0.129	4.04	0.323	C2
8705	6.5	4.26	0.145	4.00	0.355	O
8748	5.4	4.22	0.0073	3.55	0.042	O
8883	3.6	4.26	0.0062	3.62	0.072	O
-	4.5	4.15	0.0046	3.59	0.0725	O
8884	5.4	4.26	0.0060			O
8903	3.4	3.9	0.010			O

$US = 3.12 + 8.2 \cdot UP \text{ KM}/\text{SEC}$ FOR UP FROM 0.04 TO 0.13 KM/SEC
 $US = 2.38 + 4.8 \cdot UP \text{ KM}/\text{SEC}$ FOR UP FROM 0.22 TO 0.45 KM/SEC

TABLE II

EXPNO	SAMPLE				STANDARD		
	P _{M00}	P ₁	V ₁ /V ₀	P ₂	V ₂ /V ₀	P	MAT
8413	7.81	4	0.970	70	0.938	65	BRASS
8445	7.82	41	0.970			7.9	IRON
8662	7.68			142	0.8425	156	AL
8468	7.73			142	0.8973	150	BRASS
8703	7.80	43	0.9713	106	0.9222	117	LUCITE
8705	7.89	48	0.9657	115	0.9130		LUCITE
8748	7.80	12.4	0.9983	12.1	0.989	18	STEEL
8883	7.80	2.04	0.9986	21.1	0.9811	19	STEEL
-	7.74	1.5	0.9989	20.8	0.9803	21	STEEL
8884	7.80	2.0	0.9986			2.5	LUCITE
8903	7.80	3.1	0.9975			5.6	AL

COMMENTS:

108/14.77

- 1) SOURCE: DORAN, D. G.
REPORT NO SC-DC-64-348 (1962)
STANFORD RES. INST., MENLO PARK, CALIF.
- 2) EXPERIMENTAL TECHNIQUE C2 AND D
DATA REDUCTION METHOD D WITH 2UP = UFS.
- 3) THE DATA SHOW A DECREASE OF US WITH PRESSURE BETWEEN 2 AND 5 KBAR.
THIS WAS NOT OBSERVED BY REYNOLDS AND SEAY, J. APPL. PHYS., VOL. 33,
P. 2234 (1962).
THEY GIVE A FIT FOR AN ELASTIC WAVE AND A PLASTIC WAVE
 $US_1 = 2.99 + 19.2 \cdot UP_1 \text{ KM/SEC}$ $UP_{1\text{MAX}} = 0.060$ - $US_{1\text{MAX}} = 4.15 \text{ KM/SEC}$
 $SIG UP_1 = 0.004$ - $SIG US_1 = 0.05 \text{ KM/SEC}$
 $US_2 = 1.63 + 3.53 \cdot UP_2 \text{ KM/SEC}$ FOR UP_2 BETWEEN 0.06 AND 1.1 KM/SEC
WITH 2UP=UFS
FOR A ZIRCONATE-TITANATE OF COMPOSITION, PB-ZRO.52-TIO.48-O3
WITH $V_0 = 0.132 \text{ CC/G}$.
- 4) THE CURIE TEMPERATURE OF THE ZIRCONATE IS 215 DEG. C.
- 5) DENSITY UNIFORMITY OF THE SAMPLES WAS 0.08 G/CC MAXIMUM.
- 6) FOR THE EXPERIMENT NO. 8705 THE TABLE LISTS A THICKNESS OF SAMPLE
WHICH IS THE MAXIMUM THICKNESS OF A 9 DEG. WEDGE.

006/14/77

TABLE I

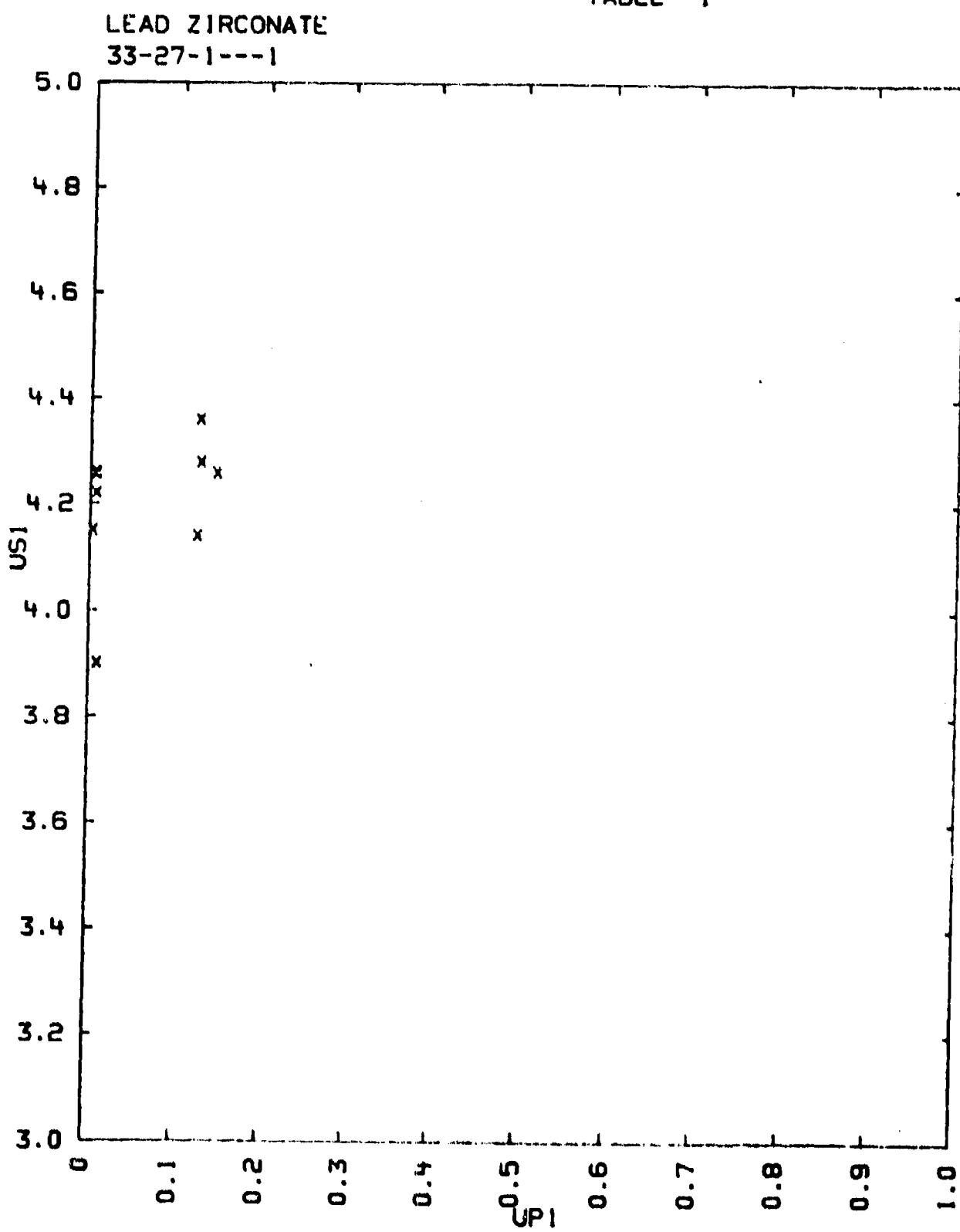
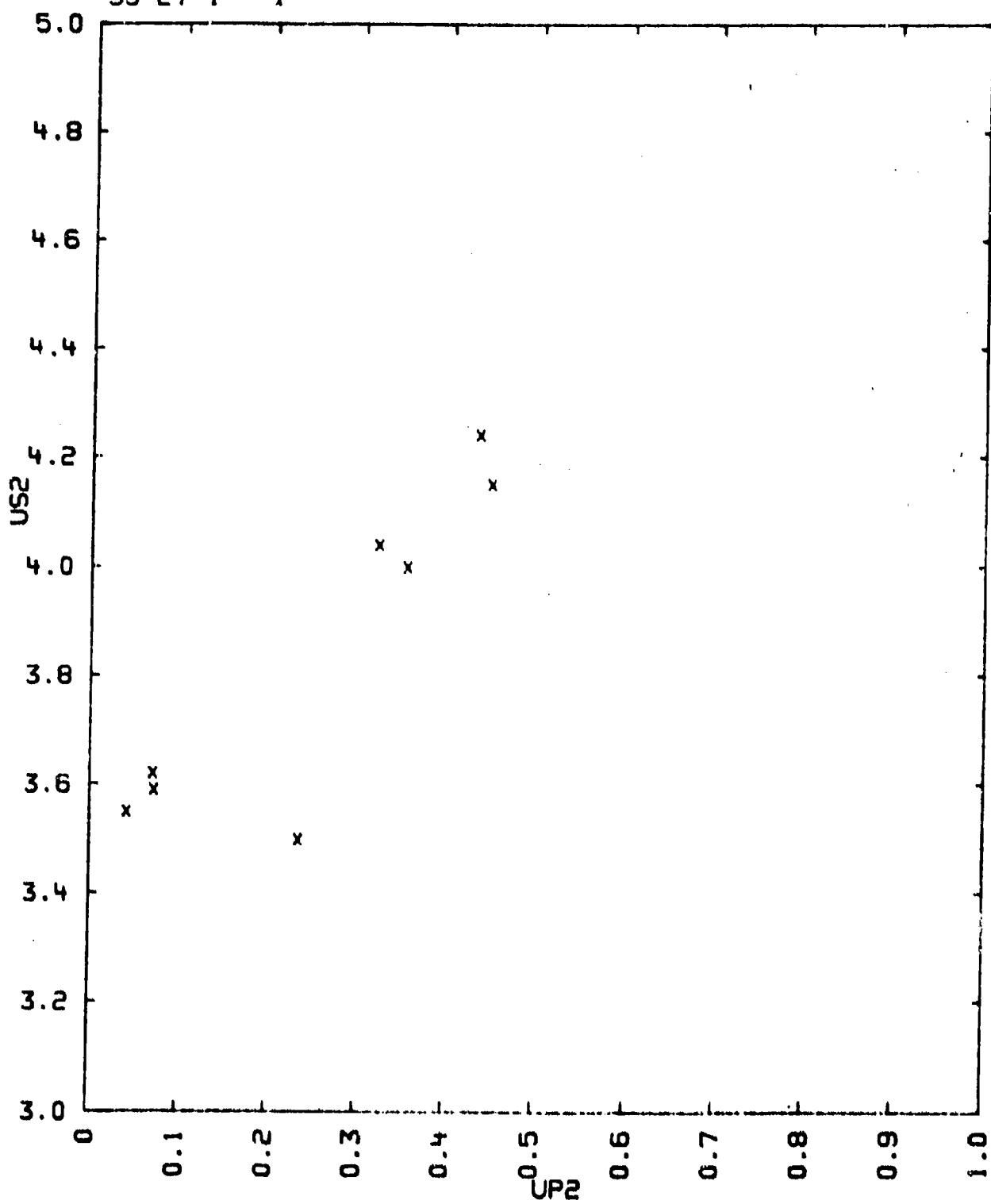


TABLE I

LEAD ZIRCONATE
33-27-1---1



41-1--1
HEMATITE NATURAL (IRON OXIDE)

FE2-03

$$V_0 = 0.204 \text{ TO } 0.198 \text{ CC}/\text{O}$$

$$V_{01} = 0.1893 \text{ CC}/\text{O}$$

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE STANDARD SAMPLE HOLDER MATERIAL.

TABLE

RHO0	US	UP	P	V/V0	US(ST)
5.01	7.62	2.34	896	0.692	9.15
4.90	7.67	2.39	900	0.687	9.18
4.98	7.77	2.44	944	0.687	9.29
5.01	7.86	2.45	964	0.688	9.33
5.01	8.49	2.92	1243	0.657	10.08
5.02	8.47	2.92	1243	0.654	10.08
5.01	8.47	2.93	1241	0.654	10.08
5.05	8.48	2.93	1253	0.655	10.11
5.05	8.45	2.93	1253	0.652	10.11
4.97	8.84	3.23	1421	0.634	10.54

$$US = 4.385 + 1.393 \cdot UP \text{ KM/SEC.}$$

$$\text{SIGMA US} = 0.037 \text{ KM/SEC.}$$

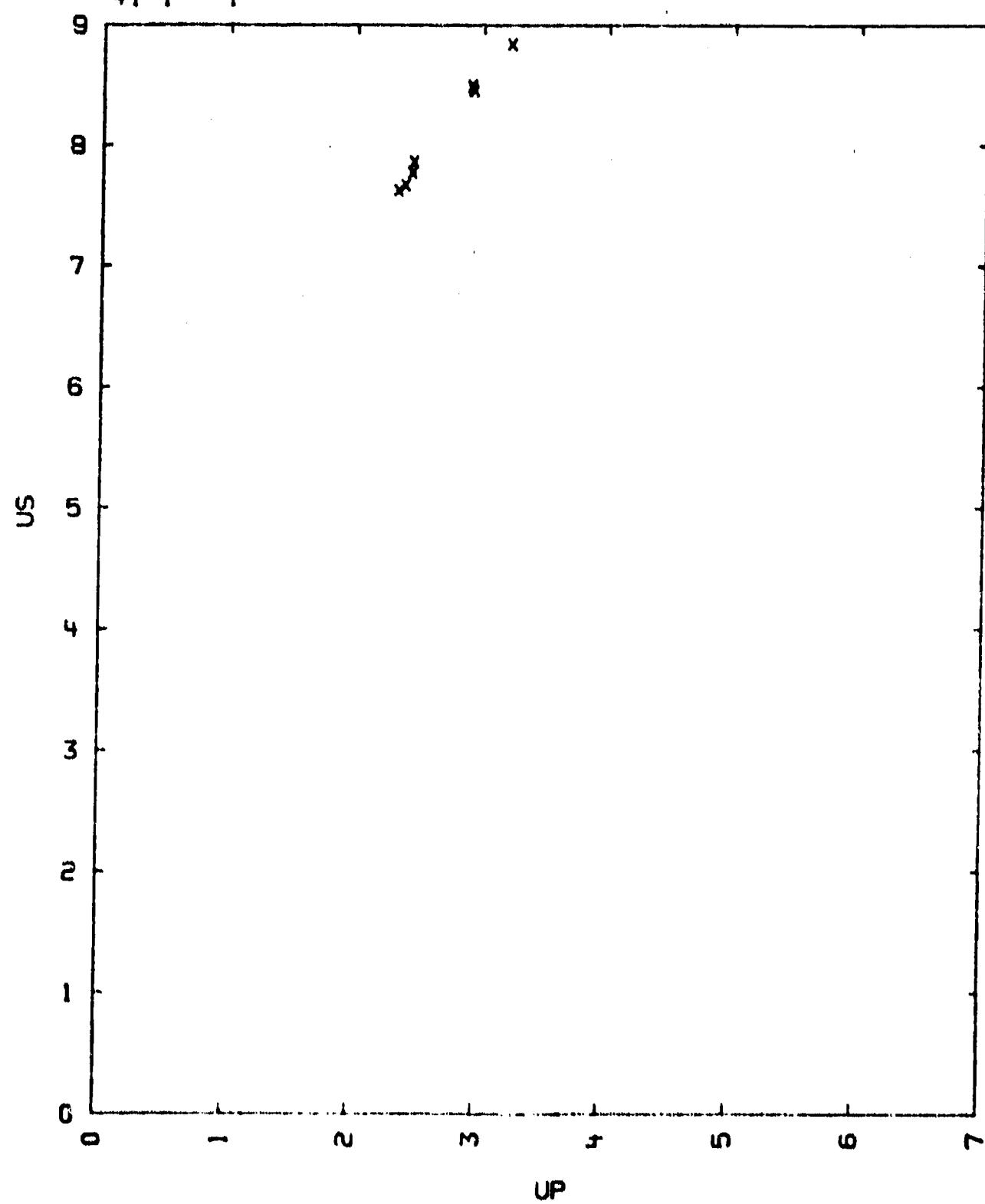
COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.
 PRIVATE COMMUNICATION
 LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B
 DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) V01 WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED BY WYCKOFF
 CRYSTAL STRUCTURES, VOL. 2 (JOHN WILEY AND SONS, NEW YORK 1963)
- 4) FURTHER WORK IS IN PROGRESS.

TABLE I

HEMATITE NATURAL (FERRIC OXIDE)

41-1---1



41-1-2

MAGNETITE NATURAL (FERROSOFERRIC OXIDE)

FE3-04

 $V_0 = 0.200 \text{ TO } 0.194 \text{ CC}/\text{O}$ $V_{01} = 0.1924 \text{ CC}/\text{O}$

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN Kbars AND DENSITY IN G/CC. ST DESIGNATES THE STANDARD SAMPLE HOLDER MATERIAL.

TABLE

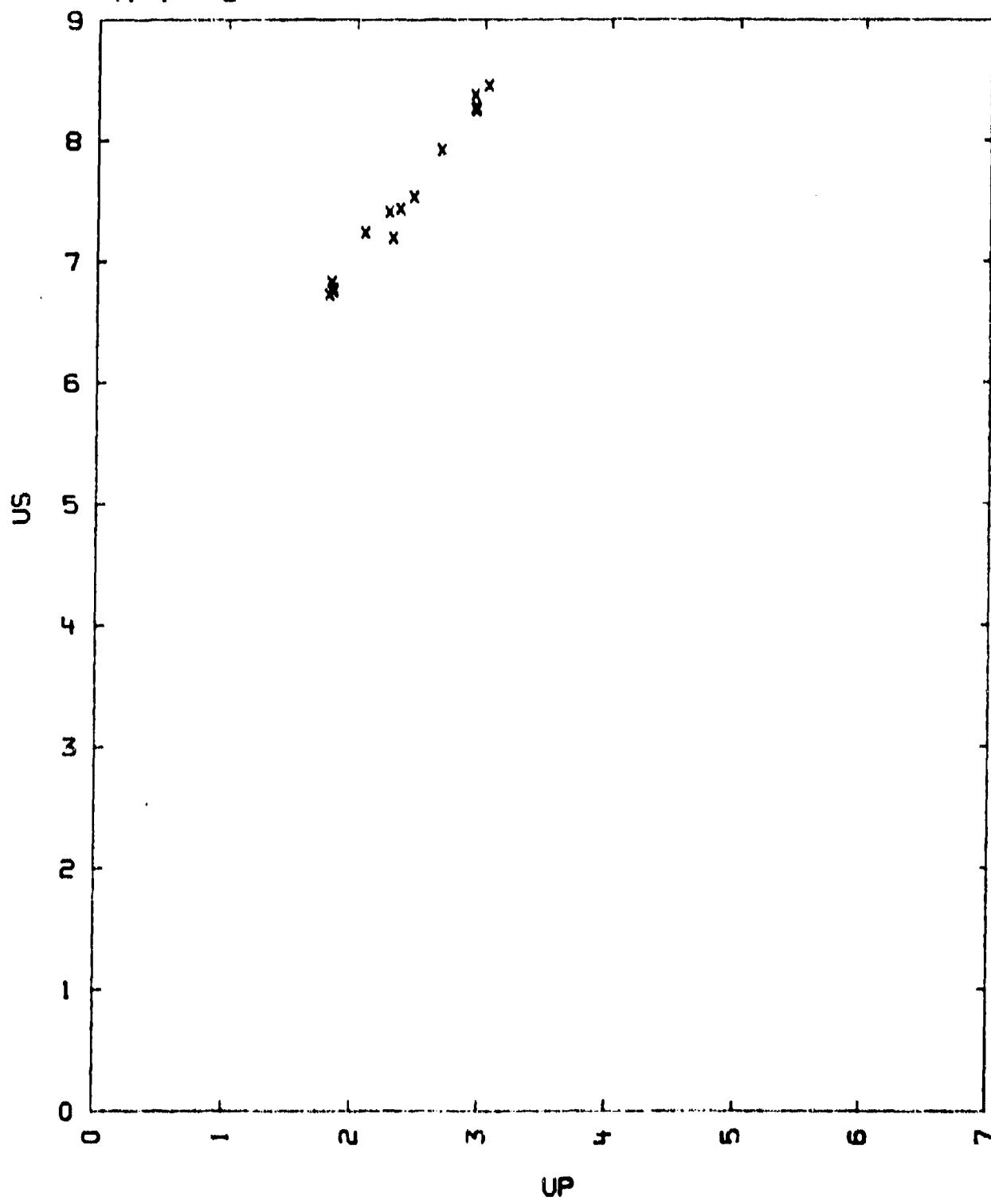
RHO0	US	UP	P	V/V0	US(ST)
5.11	6.72	1.80	620	0.731	8.28
5.14	6.82	1.82	637	0.734	8.32
5.13	6.77	1.83	634	0.731	8.32
5.14	6.74	1.83	634	0.728	8.32
5.13	7.23	2.08	771	0.713	8.75
5.11	7.40	2.26	853	0.695	9.01
5.13	7.19	2.29	845	0.682	9.02
5.13	7.43	2.35	894	0.685	9.15
5.11	7.53	2.45	942	0.675	9.29
5.13	7.92	2.67	1083	0.664	9.67
5.14	8.26	2.93	1241	0.646	10.08
5.01	8.37	2.93	1227	0.651	10.06
5.10	8.25	2.94	1235	0.645	10.08
5.13	8.27	2.94	1248	0.645	10.11
5.13	8.45	3.03	1310	0.642	10.25

 $US = 4.259 + 1.368 \cdot UP \text{ KM/SEC.}$ $\text{SIGMA US} = 0.082 \text{ KM/SEC.}$

COMMENTS :

- 1) SOURCE: MCQUEEN R.O. AND MARSH S.P.
PRIVATE COMMUNICATION
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) V01 WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED BY WYCKOFF
CRYSTAL STRUCTURES VOL. 2 (JOHN WILEY AND SONS, NEW-YORK 1963)
- 4) FURTHER WORK IS IN PROGRESS.

TABLE I
MAGNETITE NATURAL (FERROSOFERRIC OXIDE)
41-1--2



41-24-1---1
FAYALITE (IRON ORTHOSILICATE)

FE2-SI-04

$V_0 = 0.232 \text{ TO } 0.239 \text{ CC/O}$
 $\text{VOL} = 0.2314 \text{ CC/O}$

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE STANDARD SAMPLE HOLDER MATERIAL.

TABLE

RHO0	US	UP	P	V/V0	US(ST)
4.30	6.65	2.02	577	0.697	8.33
4.29	7.06	2.30	696	0.675	8.76
4.23	7.23	2.37	729	0.671	8.86
4.18	7.56	2.65	839	0.648	9.26
4.29	7.96	2.96	1013	0.627	9.75
4.28	8.32	3.19	1137	0.617	10.10

$US = 3.862 + 1.395 \cdot UP \text{ KM/SEC.}$
 $SIGMA US = 0.038$

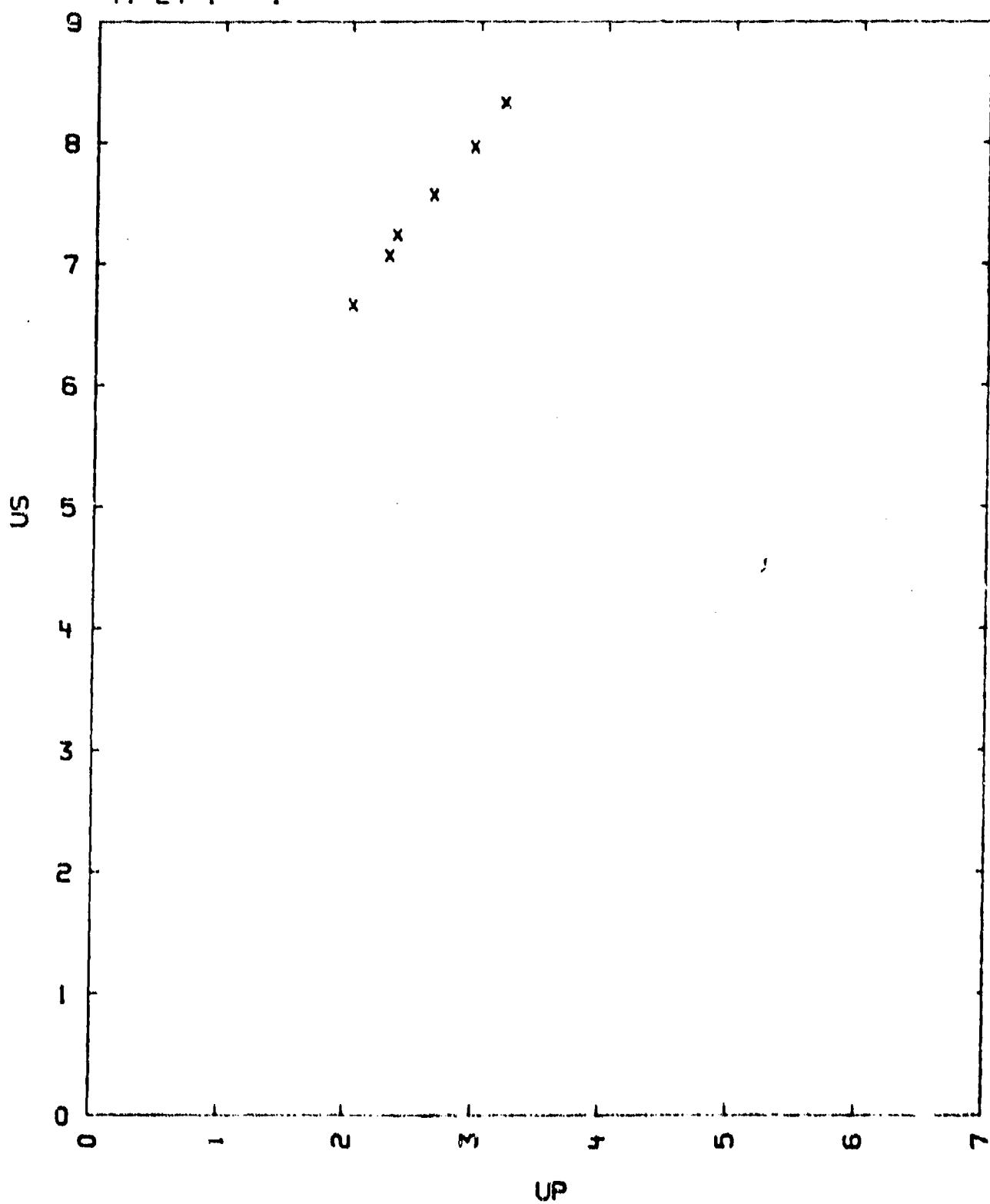
COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.
PRIVATE COMMUNICATION
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION METHOD B - STANDARD MATERIAL 2024 ALUMINUM
- 3) VOL HAS OBTAINED FROM THE LATTICE PARAMETERS LISTED IN CRYSTAL DATA DETERMINATIVE TABLES (AM. CRYST. ASSN 1963) 2ND ED.
- 4) FURTHER WORK IS IN PROGRESS.

TABLE I

FAYALITE (IRON ORTHOSILICATE)

41-24-1---1



4B-1---1
PYROLUSITE (MANGANESE DIOXIDE)

MN-02

$V_0 = 0.226 \text{ TO } 0.248 \text{ CC}/0$
 $\text{VOL} = 0.1922 \text{ CC}/0$

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. SI DESIGNATES THE SAMPLE HOLDER AND STANDARD MATERIAL.

TABLE

RHO0	US	UP	P	V/V0	US(SI)
4.42	5.11	0.81	183	0.842	6.56
4.39	5.49	1.12	270	0.797	7.01
4.06	5.20	1.41	298	0.729	7.28
4.37	5.91	1.48	381	0.750	7.54
4.33	6.00	1.48	385	0.753	7.55
4.24	5.82	1.57	388	0.730	7.62
4.19	5.83	1.64	402	0.717	7.70
4.24	6.10	1.70	439	0.722	7.82
4.37	6.85	1.98	591	0.712	8.33
4.30	7.08	2.23	681	0.685	8.68
4.36	7.26	2.25	713	0.690	8.76
4.32	7.49	2.31	747	0.691	8.86
4.26	7.39	2.45	771	0.689	9.00
4.30	7.98	2.94	1023	0.632	9.75
4.34	8.37	3.16	1149	0.623	10.10
4.29	8.90	3.31	1263	0.620	10.37
4.31	8.40	3.32	1202	0.604	10.29

$US = 3.632 + 1.520 \cdot UP \text{ KM/SEC.}$

SIGMA US = 0.25 KM/SEC.

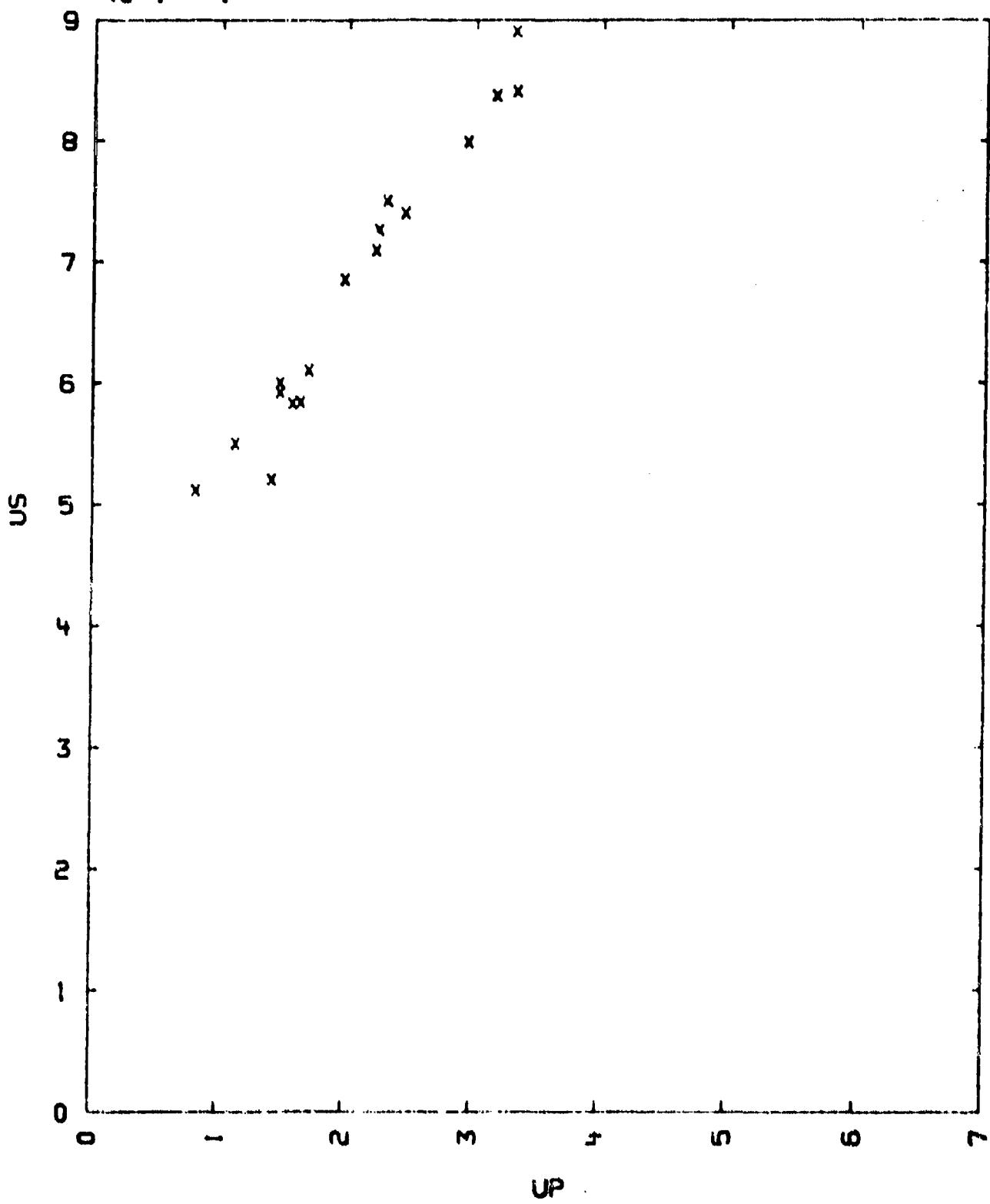
COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.
PRIVATE COMMUNICATION
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) VOL WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED BY WYCKOFF
CRYSTAL STRUCTURES, VOL. 1 (JOHN WILEY AND SONS, NEW-YORK 1965)
- 4) FURTHER WORK IN PROGRESS

TABLE I

PYROLUSITE (MANGANESE DIOXIDE)

48-1---1



53-23---1
TUNGSTEN CARBIDE

H-C

$$V_0 = 0.06653 - 0.06671 \text{ CC/G} \quad C_L = 6.89 \text{ KM/SEC} \quad C_D = 4.92 \text{ KM/SEC}$$

$$V_{01} = 0.06381 \text{ CC/G} \quad C_S = 4.18 \text{ KM/SEC}$$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBARS AND DENSITY IN G/CC.

TABLE

-----SAMPLE-----					-----STANDARD-----	
RHO0	US	UP	P	V/V0	MATERIAL	US(ST)
15.050	5.57	0.22	184.	0.9605	CU	4.44
15.010	5.71	0.35	300.	0.9387	CU	4.71
15.010	5.67	0.37	315.	0.9347	CU	4.74
15.000	5.73	0.44	378.	0.9232	CU	4.87
15.060	5.72	0.44	378.	0.9231	CU	4.88
15.020	5.95	0.68	609.	0.8859	CU	5.33
14.990	6.01	0.71	640.	0.8819	CU	5.39
14.990	5.97	0.75	674.	0.8744	CU	5.45
14.990	6.86	1.44	1481.	0.7901	CU	6.70
15.030	6.93	1.48	1942.	0.7864	CU	6.77
15.020	6.91	1.49	1946.	0.7844	CU	6.78
15.000	7.11	1.71	1824.	0.7995	CU	7.15
15.010	7.17	1.75	1883.	0.7959	CU	7.22
15.010	7.33	1.82	2002.	0.7917	CU	7.35

US = 4.820 + 1.339 * UP KM/SEC UP GREATER THAN 0.65 KM/SEC
 510 US = .086 KM/SEC

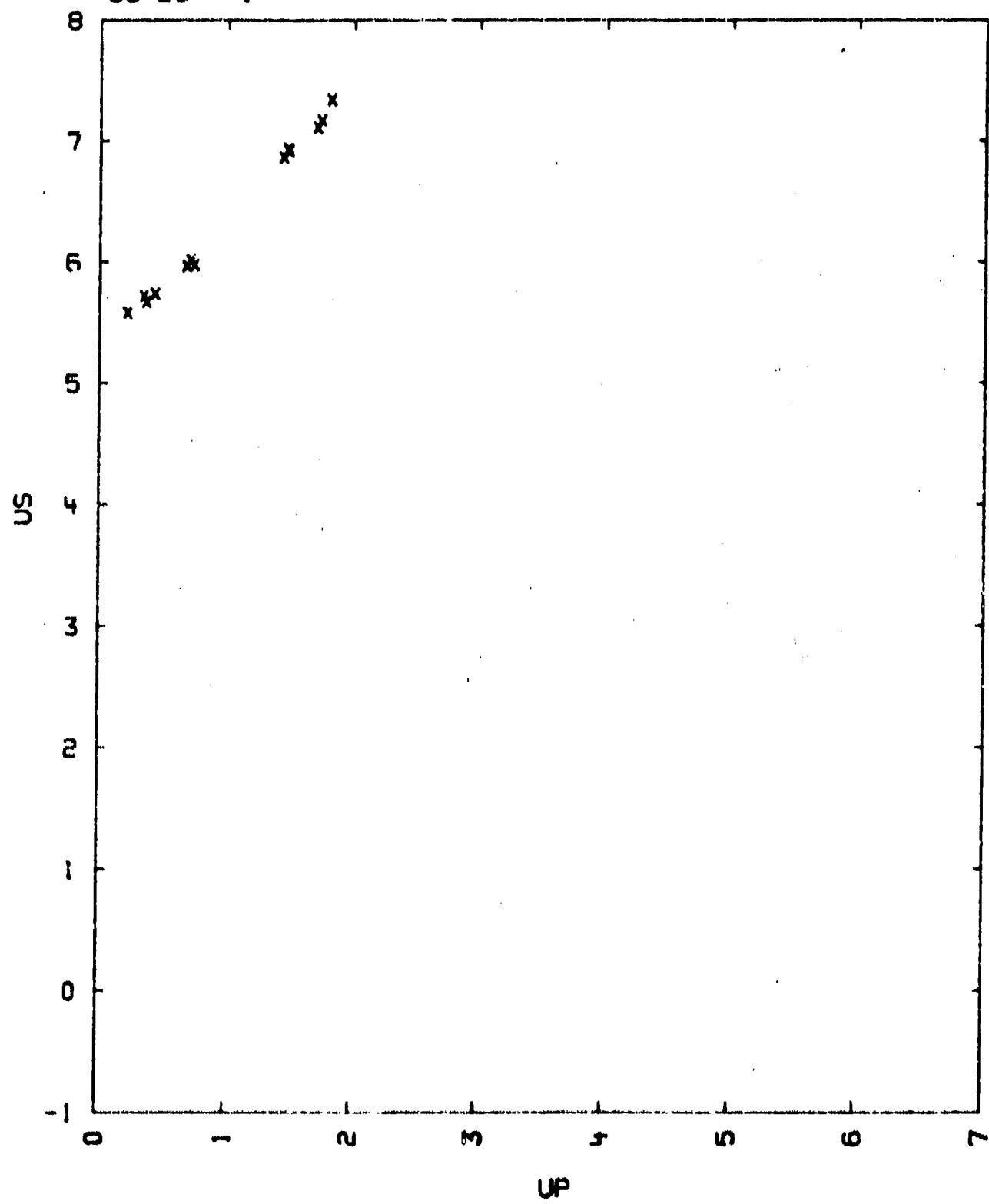
COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M., AND CARTER, W.J.
 THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,
 HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC
 PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B
 DATA REDUCTION TECHNIQUE: B
- 3) FROM WYCKOFF, CRYSTAL STRUCTURES (JOHN WILEY AND SONS, N.Y., 1963)
 VOL. 1
- 4) V(TOP, C.E) = 1.5, HEL = 40. KBAR
- 5) HUNDRED OF ELASTIC LIMIT 40. KBAR

UN6/14/71

TABLE I

TUNGSTEN CARBIDE
53-23---1



57-1---1

RUTILE, CRYSTAL AND NATURAL (TITANIUM OXIDE)

T1-02

 $V_0 = 0.235 \text{ TO } 2.38 \text{ CC}/\text{O}$ $V_{01} = 0.2353 \text{ CC}/\text{O}$

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE STANDARD SAMPLE HOLDER MATERIAL.

TABLE

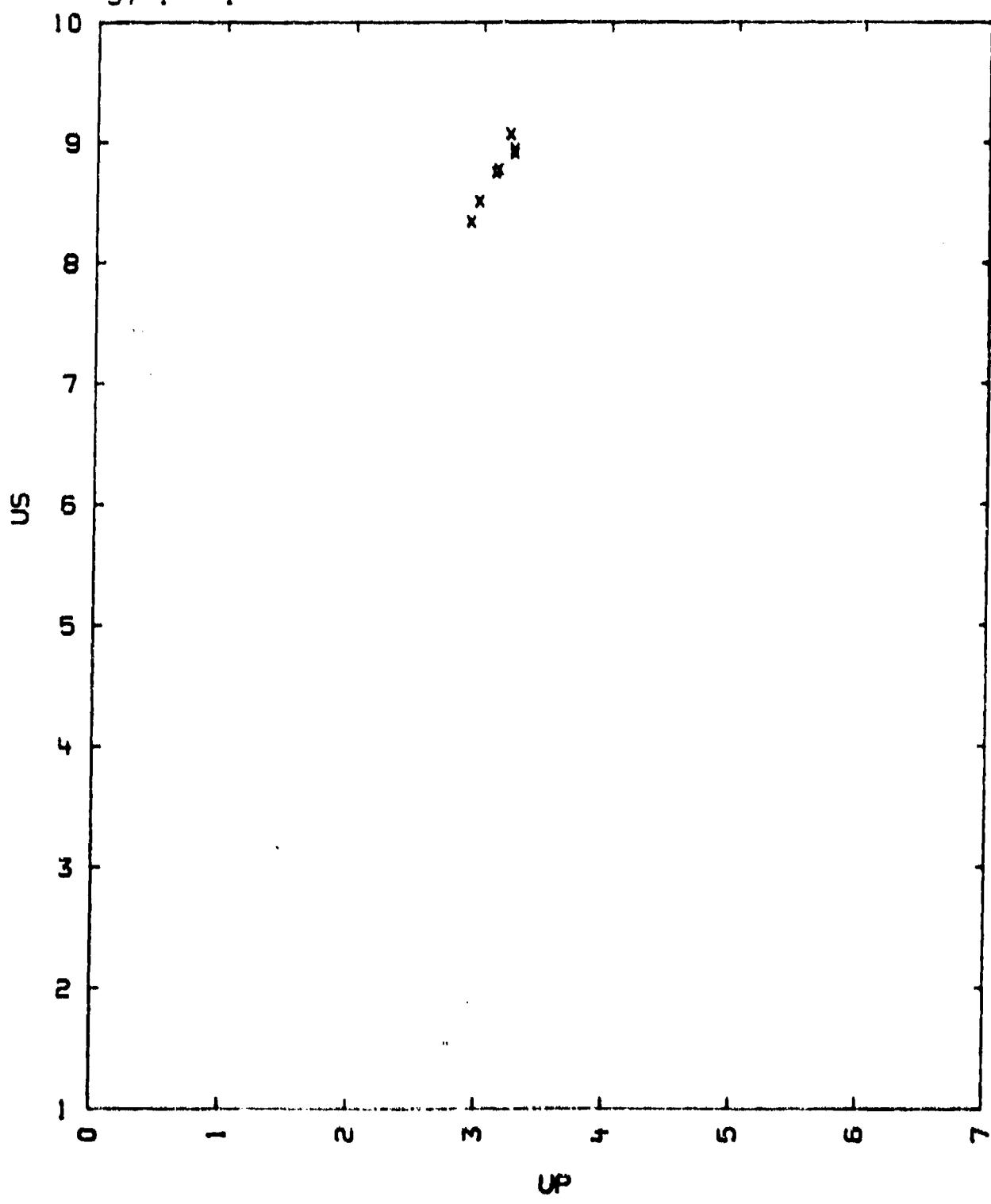
RHO0	US	UP	P	V/V0	US(ST)
4.25	8.33	2.92	1033	0.650	9.75
4.21	8.51	2.98	1068	0.650	9.86
4.25	8.74	3.11	1157	0.644	10.08
4.25	8.77	3.13	1165	0.644	10.10
4.25	8.76	3.13	1165	0.643	10.11
4.25	9.06	3.22	1242	0.644	10.28
4.20	9.90	3.25	1213	0.635	10.25
4.25	8.94	3.25	1235	0.636	10.29

 $US = 2.926 + 1.865 \cdot UP \text{ KM/SEC.}$ $\text{SIGMA US} = 0.070 \text{ KM/SEC.}$

COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.
PRIVATE COMMUNICATION
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) VOI WAS OBTAINED FROM 1 LATTICE PARAMETERS LISTED BY HYCKOFF
CRYSTAL STRUCTURES VOL. I (JOHN WILEY AND SONS, NEW-YORK, 1963)
- 4) FURTHER WORK IS IN PROGRESS.

TABLE I
RUTILE, CRYSTAL AND NATURAL (TITANIUM OXIDE)
57-1---1



57-41-1---
ILMENITE (IRON METATITANATE)

FE-TI-03

$$V_0 = 0.260 \text{ TO } 0.265 \text{ CC/O}$$

$$V_{01} = 0.2075 \text{ CC/O}$$

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE STANDARD SAMPLE HOLDER MATERIAL.

TABLE

RHO0	US	UP	P	V/V0	US(ST)
3.84	7.41	2.36	673	0.681	8.78
3.78	7.44	2.47	692	0.689	8.88
3.77	7.43	2.47	691	0.688	8.88
3.77	7.93	2.72	814	0.657	9.26
3.84	8.43	3.04	983	0.640	9.75
3.83	8.88	3.26	1106	0.632	10.10

$$US = 3.317 + 1.691 \cdot UP \text{ KM/SEC.}$$

$$\text{SIGMA US} = 0.069$$

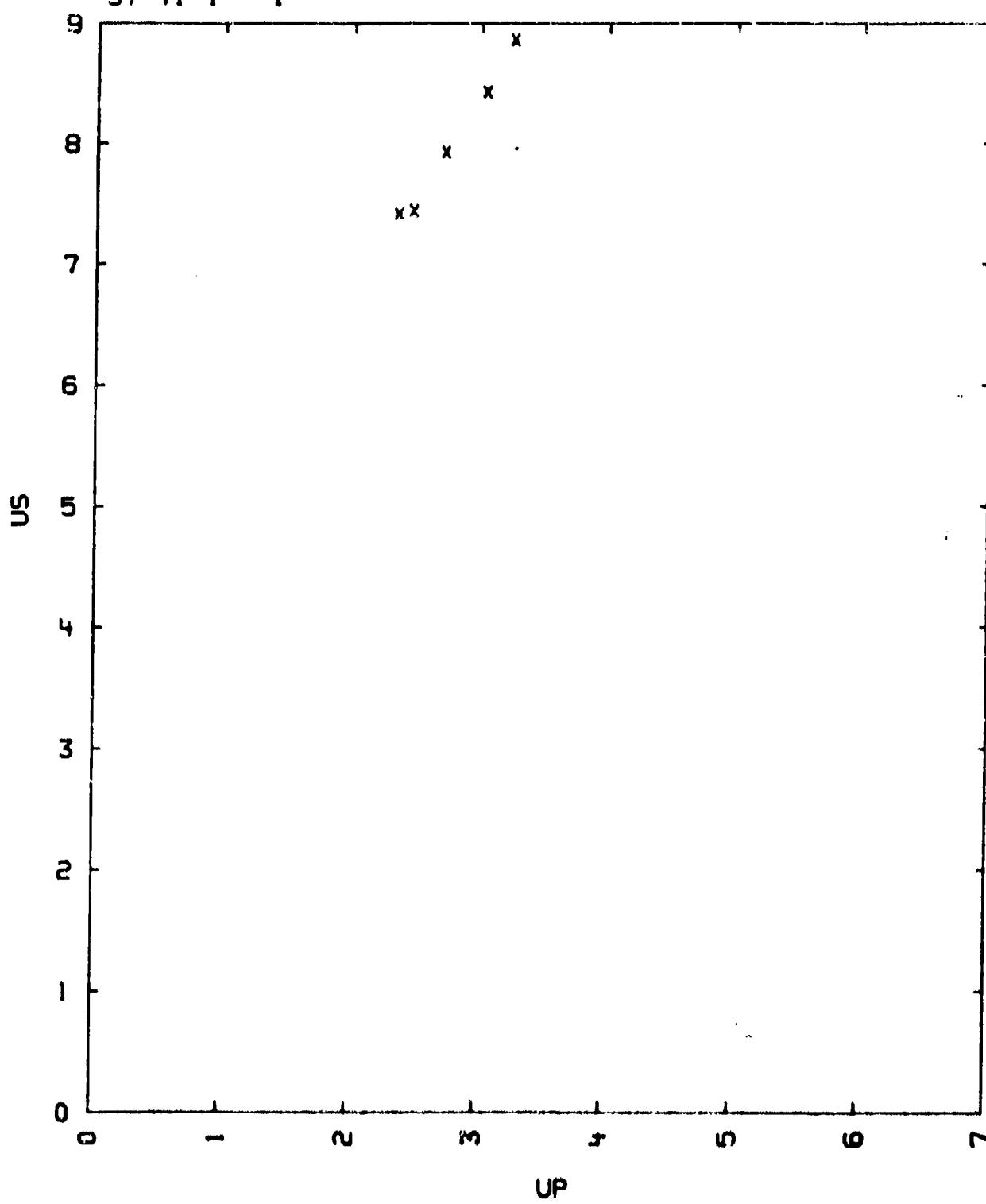
COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.
PRIVATE COMMUNICATION
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) V01 HAS OBTAINED FROM THE LATTICE PARAMETERS LISTED BY WYCKOFF,
CRYSTAL STRUCTURES, VOL. 2 (JOHN WILEY AND SONS, NEW-YORK 1963)
- 4) FURTHER WORK IS IN PROGRESS.

TABLE I

ILMENITE (IRON METATITANATE)

57-41-1---1



92-1---1
BERYLLIUM OXIDE POROUS

BE-0

$$V_0 = 0.342 - 0.498 \text{ CC/G}$$

$$V_{01} = 0.3342 \text{ CC/G}$$

THE TABLES BELOW LIST DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN Kbars

TABLE I

RH00	SAMPLE				AL BASE PLATE	
	US	UFS	UP	P	V/V0	PRESSURE
2.908	8.85	1.57	0.78	197	0.812	168
2.827	8.5		0.82	151	0.828	133
2.88	9.07	2.02	1.04	271	0.884	238
2.905	9.29	2.47	1.23	338	0.866	304
2.853	8.71	1.55	0.77	192	0.81	168
2.908	9.62	2.95	1.56	437	0.838	378
2.919	10.15	3.69	1.91	566	0.812	493
2.914	10.22	4.09	2.06	613	0.798	537
2.926	11.26	6.75	2.74	903	0.757	796
2.910	10.85	5.10	2.42	765	0.777	670

US = 7.72 + 1.27 UP KM/SEC

SIGMA US = 0.071 KM/SEC

TABLE II

RH00	SAMPLE				AL BASE PLATE	
	US	UFS	UP	P	V/V0	PRESSURE
2.60	7.01	1.97	1.25	228	0.822	238
2.863	10.85	6.17	3.48	1030	0.681	970
2.778	11.26	6.83	3.71	1161	0.671	1100
2.086	5.04	2.57	1.98	208	0.607	317
2.168	5.70	3.02	2.05	254	0.640	359
2.01	5.83	3.02	2.01	236	0.656	339

US =

COMMENTS:

1) SOURCE: COMPILER

L.R.L. EQUATION OF STATE FILE

LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.

2) EXPERIMENTAL TECHNIQUE B. STANDARD MATERIAL 2024 AL ALLOY.

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- DATA REDUCTION TECHNIQUE B.
- 3) THE VALUE OF VOI WAS OBTAINED FROM A. TAYLOR AND BRENDA J. KAGLE,
CRYSTALLOGRAPHIC DATA ON METAL AND ALLOY STRUCTURES
(DOVER PUBLICATIONS, INC., NEW YORK, N.Y., 1963).

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TABLE I

BERYLLIUM OXIDE POROUS
92-1---1

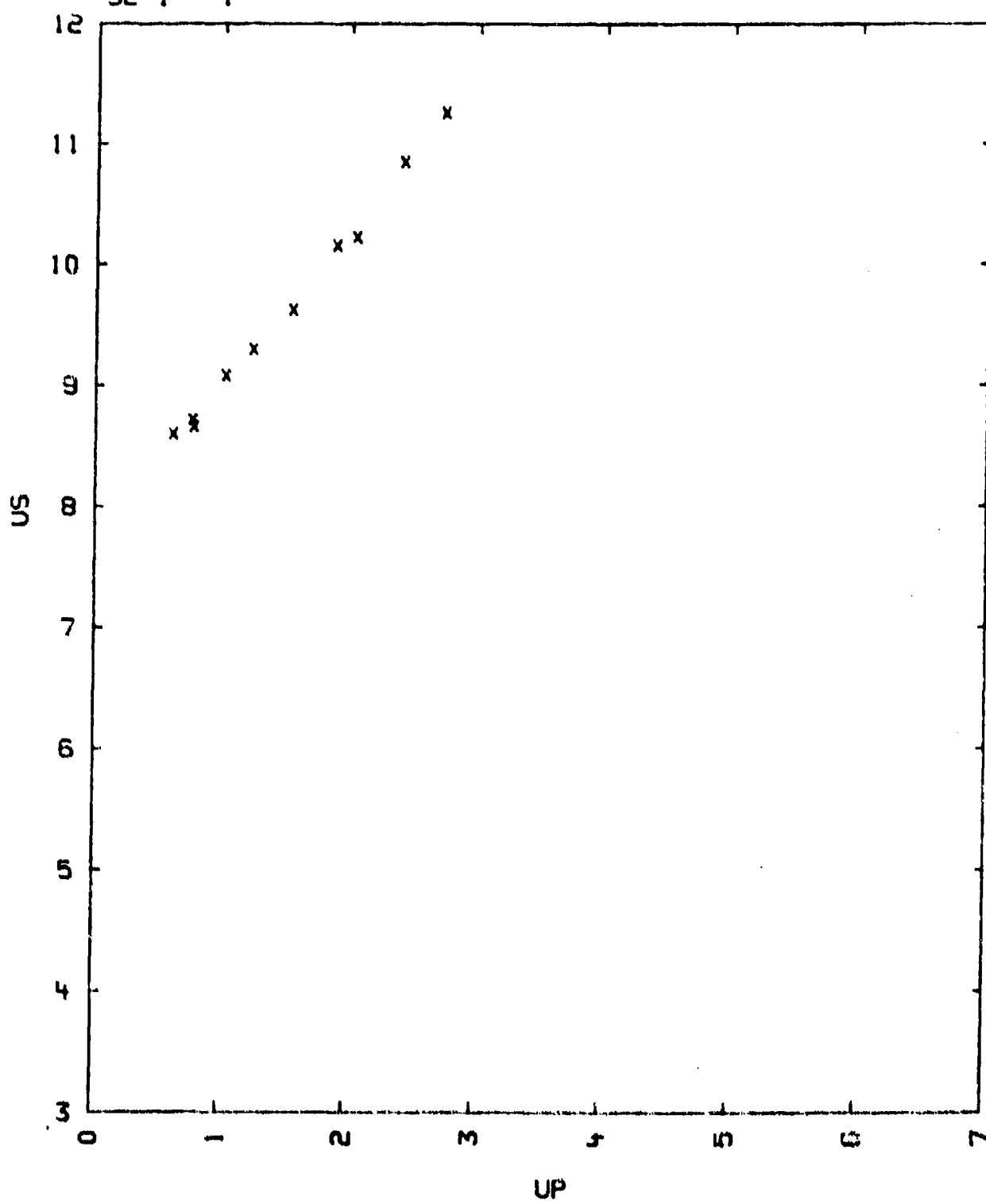
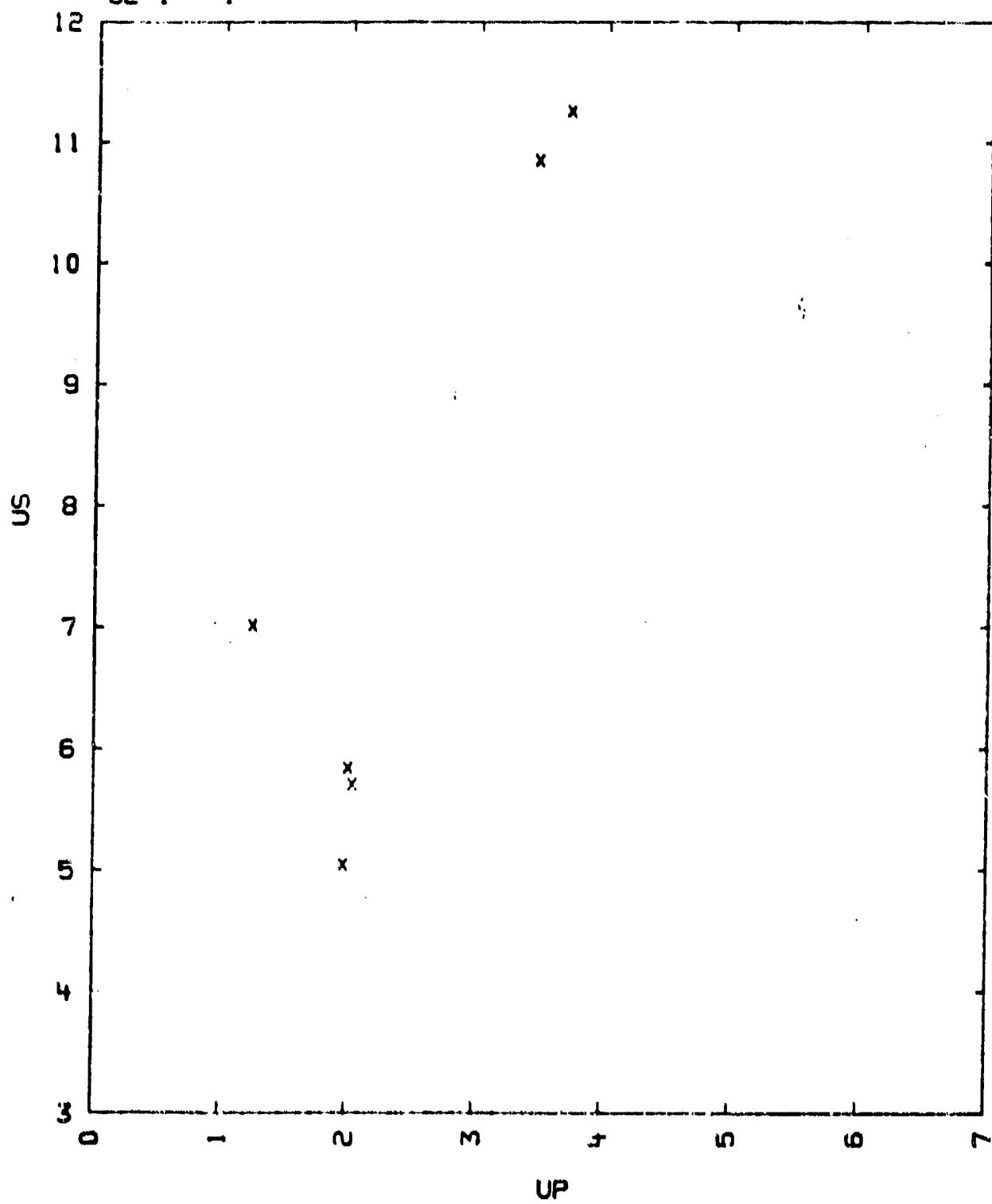


TABLE II

BERYLLIUM OXIDE POROUS

92-1---1



93-1--1

PERICLASE (MAGNESIUM OXIDE CRYSTALLINE)

MO-0

$V_C = 0.2793 \text{ CC}/\text{O}$
 $V_OI = 0.2782 \text{ CC}/\text{O}$

 $C_0 = 6.58 \text{ KM}/\text{SEC}$

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE STANDARD SAMPLE HOLDER MATERIAL.

TABLE

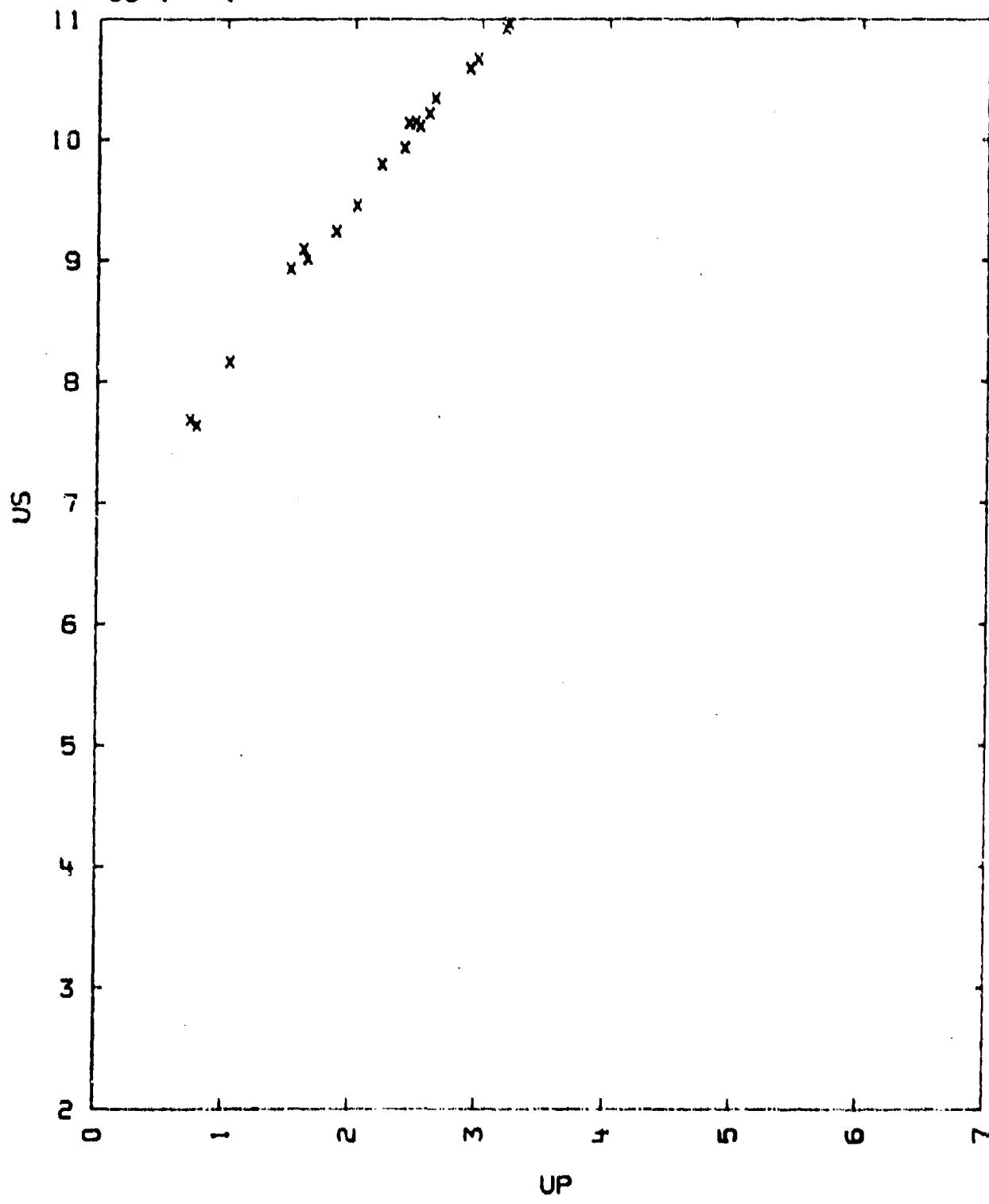
RHO0	US	UP	P	V/V0	US(ST)
3.58	7.60	0.73	202	0.904	6.57
3.58	7.63	0.78	214	0.897	6.63
3.58	8.15	1.04	304	0.871	7.05
3.58	8.93	1.51	484	0.831	7.79
3.58	9.08	1.60	521	0.823	7.93
3.58	9.01	1.84	528	0.817	7.98
3.58	9.23	1.86	616	0.797	8.31
3.58	9.45	2.02	683	0.785	8.54
3.58	9.79	2.02	780	0.772	8.86
3.58	9.93	2.40	856	0.757	9.12
3.58	10.13	2.43	884	0.758	9.18
3.58	10.14	2.49	904	0.754	9.26
3.58	10.11	2.52	913	0.751	9.29
3.58	10.21	2.59	950	0.744	9.40
3.58	10.33	2.64	980	0.743	9.49
3.58	10.59	2.90	1102	0.725	9.86
3.58	10.67	2.97	1137	0.720	9.96
3.58	10.92	3.18	1244	0.708	10.25
3.58	10.96	3.26	1258	0.708	10.29

$US = 6.535 + 1.643 \cdot UP - 0.083 \cdot UP^{1.2} \text{ KM/SEC.}$
 $\Sigma \text{SIGMA } US = 0.067 \text{ KM/SEC.}$

COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.
PRIVATE COMMUNICATION
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE &
DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) V0I WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED BY HYCKOFF,
CRYSTAL STRUCTURES VOL. I (JOHN WILEY AND SONS, NEW-YORK 1963)
- 4) FURTHER WORK IS IN PROGRESS.

TABLE I
PERICLASE (MAGNESIUM OXIDE CRYSTALLINE)
93-1---1



93-1--2

PERICLASE CERAMIC (MAGNESIUM OXIDE)

MO-O

$$\rho_0 = 3.2920 \text{ g/cc}$$

$$\rho_{01} = 3.2789 \text{ g/cc}$$

THE TABLE LISTS DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KBARS.

TABLE

ρ_{00}	US	UP	P	V/V ₀
3.425	7.63	1.32	345	0.827
-	9.31	2.52	803	0.739
-	13.42	3.62	2381	0.581

$$US = 5.89 + 1.34 UP \text{ KM/SEC}$$

$$\sigma US = 0.051 \text{ KM/SEC}$$

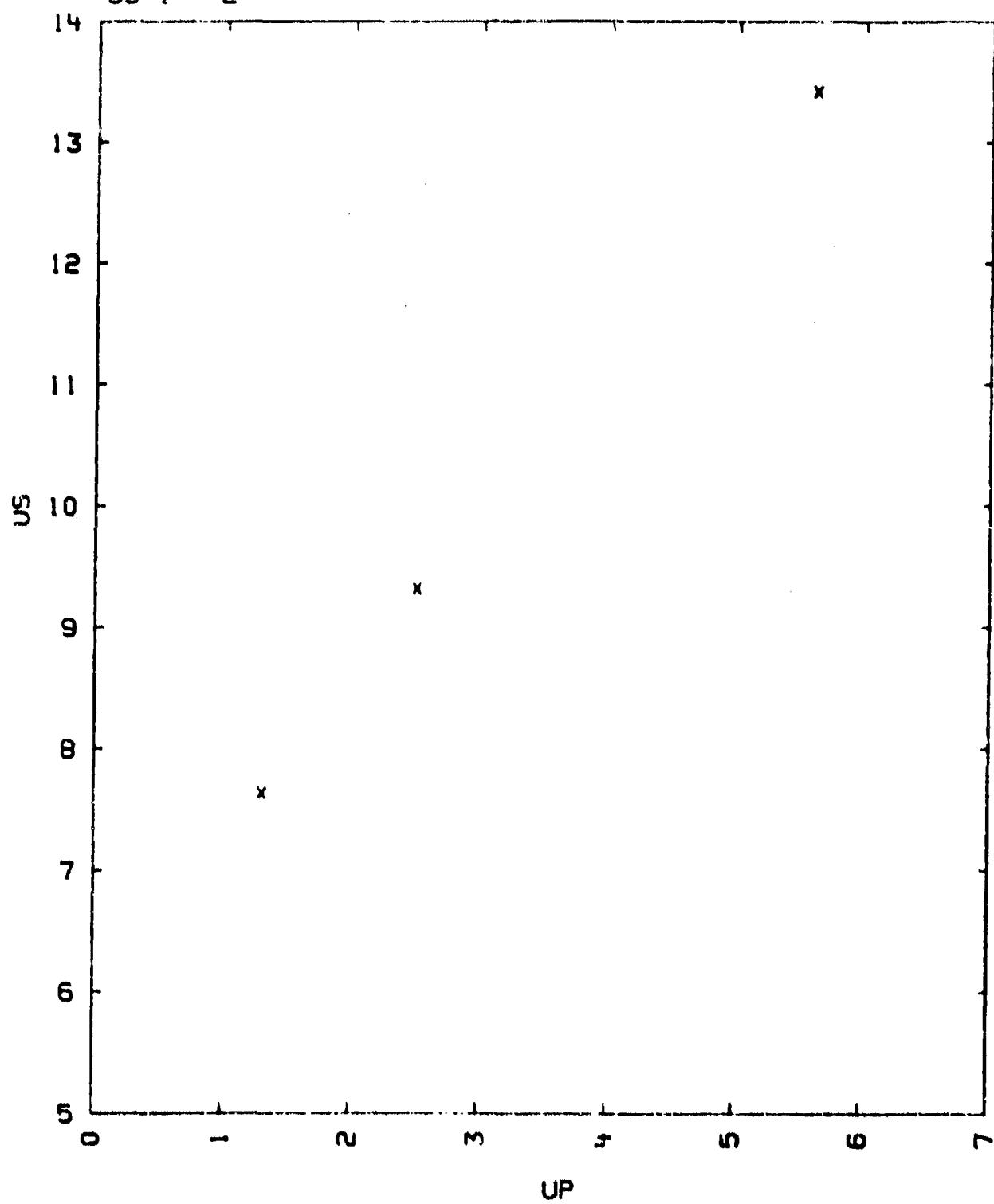
COMMENTS:

- 1) SOURCE: AL'TSHULER, L. V., TRUNIN, R. F., SIMAKOV, G. V.
IZV. AKADEMII NAUK SSSR. FIZIKA ZEMLI NO. 10, 1965 P.1-6.
- 2) EXPERIMENTAL TECHNIQUE - UNKNOWN.
- 3) DATA REDUCTION TECHNIQUE - UNKNOWN.
- 4) V01 WAS OBTAINED FROM A CUBIC LATTICE CONSTANT A=4.2112 ANGSTROM:
WYCKOFF, CRYSTAL STRUCTURES VOL. 1 (JOHN WILEY AND SONS, N. Y. 1963)
- 5) ISOTHERMS AT 0 DEG. K AND AT 4000 DEG. K. WERE OBTAINED USING A
GRUNEISEN GAMMA OF 1.0 AND HUGONIOT DENSITIES LISTED IN THE TABLE
BELOW.

P	$\rho_{00}(\text{HUG})$	$\rho_{010} \text{ DEG. K}$	$\rho_{01}(\text{4000 DEG. K})$
00	3.62	3.62	3.495
20	3.95	3.968	3.806
40	4.245	4.257	4.11
60	4.482	4.517	4.37
80	4.721	4.762	4.615
100	4.93	4.976	4.84
120	5.105	5.17	5.05
140	5.27	5.34	5.23
160	5.41	5.508	5.40
180	5.535	5.658	5.555
200	5.658	5.805	5.71
220	5.785	5.95	5.853
240	5.881	6.092	5.994
260	5.998	6.23	6.13

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TABLE I
PERICLASE CERAMIC (MAGNESIUMOXIDE)
93-1---2



93-1---3
MAGNESIUM OXIDE, SINGLE-CRYSTAL (MAGNETITE)

RH-0

$$V_0 = 0.2795 \text{ CC}/\text{G}$$

$$V_{01} = 0.2789 \text{ CC}/\text{G}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC,
AND PRESSURE IN KILOBARS.

TABLE

RH001	U _{S1}	U _{P1}	P ₁	V ₁ /V ₀	U _{S2}	U _{P2}	U _{F5}	P ₂	V ₂ /V ₀
3.576	9.191	0.1215	39.9	0.987	7.016	0.626	1.348	168	0.9147
-	9.142	0.1054	34.5	0.989	6.984	0.635	1.217	166	0.9122
-	10.068	0.2476	89.0	0.976	8.503	1.35	2.459	423	0.8456
-	-	-	-	-	8.893	0.633	1.256	166	0.9104
-	-	-	-	-	7.085	0.632	1.195	166	0.9133
-	-	-	-	-	7.801	1.229	2.678	390	0.879
-	-	-	-	-	9.61	1.92	3.733	660	0.801

$$U_{S2} = 6.15 + 1.85 \cdot U_{P2} \text{ OR } 0.3 \text{ KM/SEC}$$

COMMENTS:

- 1) SOURCE: AMRENS, T. J.
JOURNAL OF APPLIED PHYSICS, VOL. 37, P. 2932 (1966).
- 2) EXPERIMENTAL TECHNIQUE C1
DATA REDUCTION METHOD A, WHERE $U_{P2} = U_{F5}$
INTERACTION OF THE ELASTIC WAVE WITH THE SECOND SHOCK WAS CORRECTED.
FOR
- 3) THE TABLE BELOW GIVES THE CALCULATED HUGONIOT TEMPERATURE (T) IN
DEG. KELVIN AND HUGONIOT PRESSURE (P) IN KILOBARS.
- T = 307, 323, 349, 375, 419, 485, 584, 733, 959, 1313
P = 42.9, 96.1, 163, 247, 354, 493, 674, 913, 1249, 1710
- 4) V_{01} WAS OBTAINED FROM A CUBIC LATTICE CONSTANT $A = 4.2112$ ANGSTROM:
WYCKOFF, CRYSTAL STRUCTURES VOL. I (JOHN WILEY AND SONS, N. Y. 1963).
- 5) THE MAGNETITE SINGLE-CRYSTALS WERE OBTAINED FROM NORTON CO., NIAGARA
FALLS, N. Y., U.S.A.
- 6) THE ACCURACY OF THE SHOCK AND PARTICLE VELOCITY MEASUREMENTS ARE
WITHIN 1 PERCENT.

TABLE I
MAGNESIUM OXIDE, SINGLE-CRYSTAL (MAGNORITE)
93-1---3

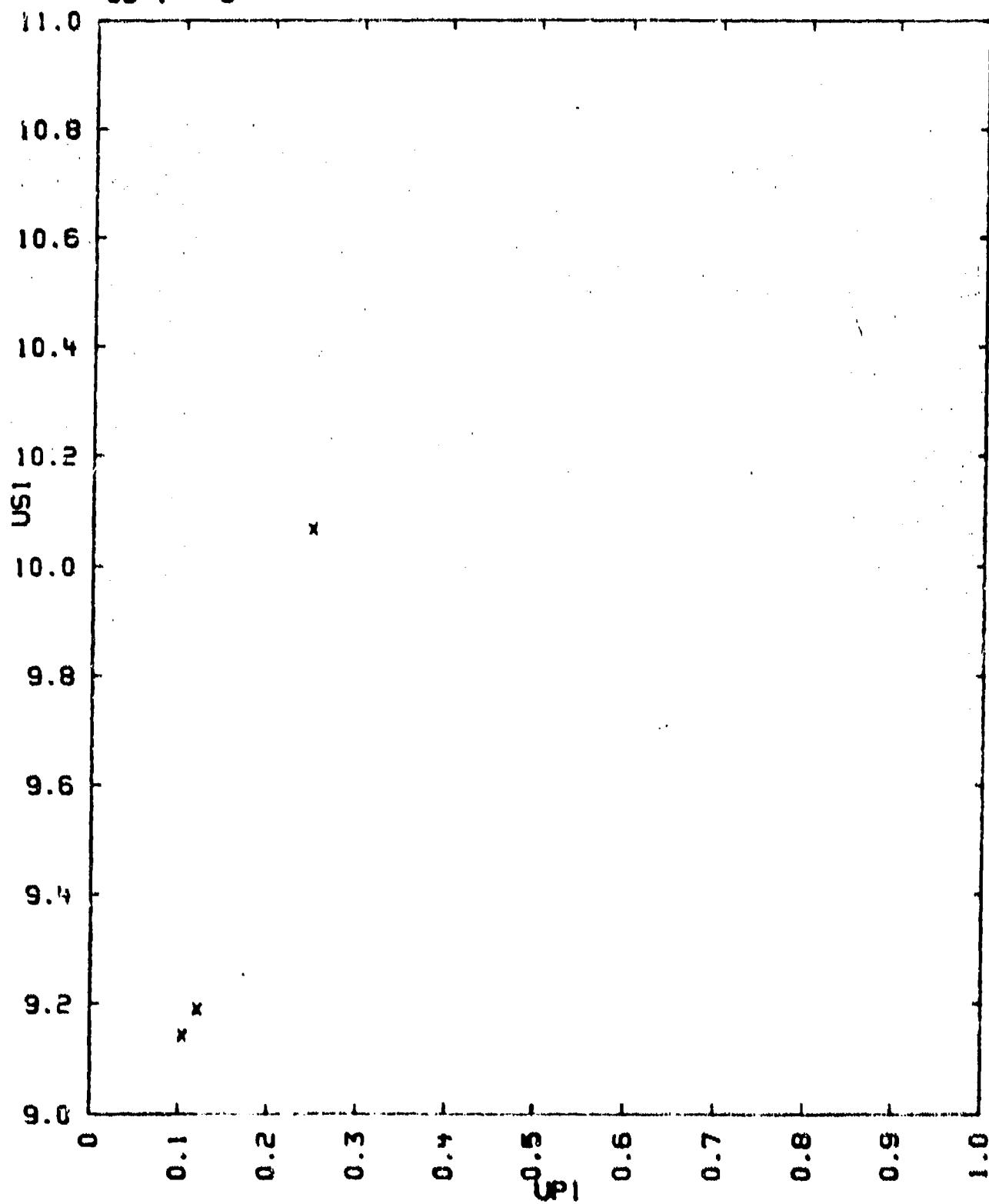
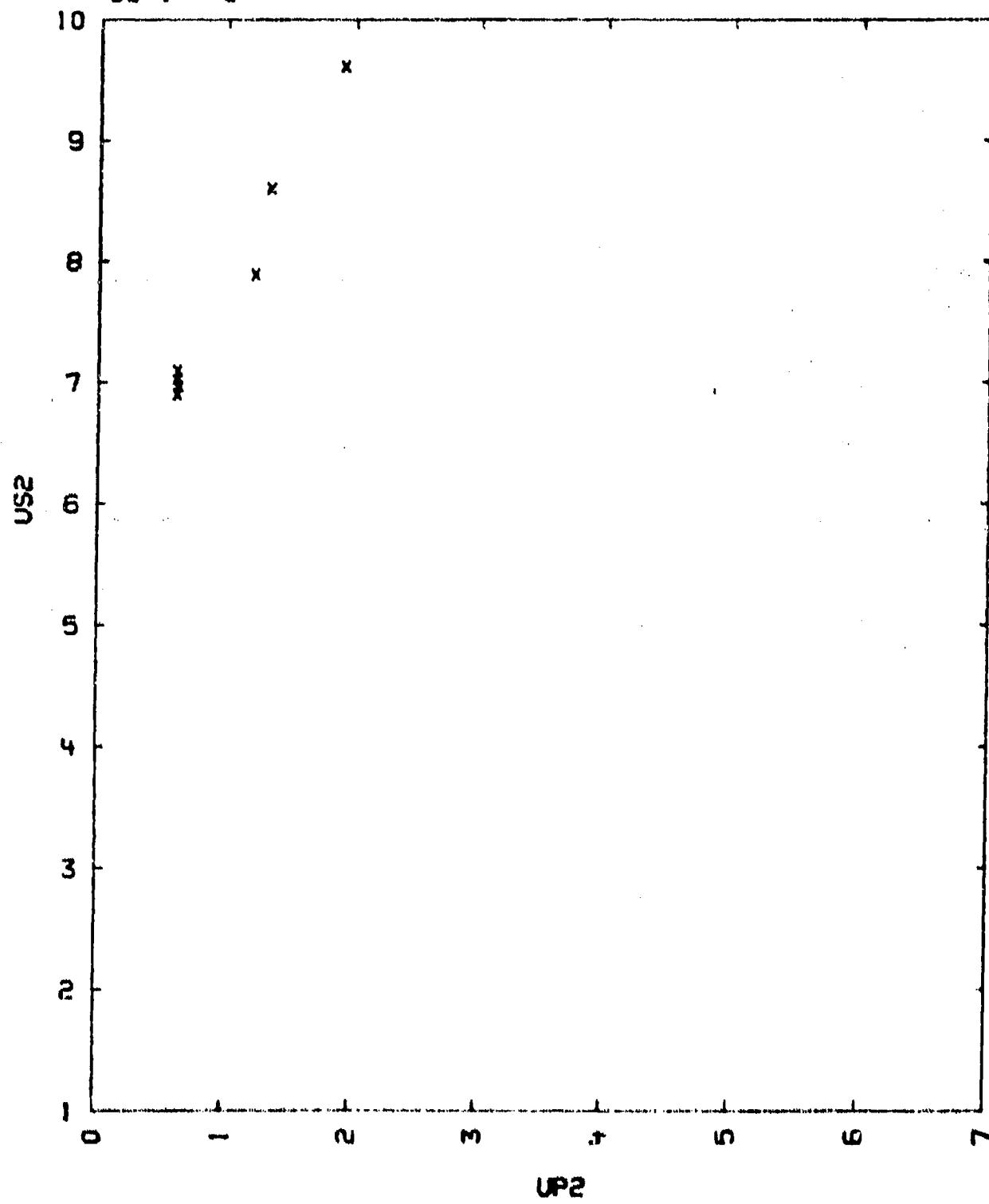


TABLE I
MAGNESIUM OXIDE, SINGLE-CRYSTAL (MAGNORITE)
93-1--3



93-24-1---1

ENSTATITE CERAMIC (MAGNESIUM METASILICATE)

MO-51-03

$$V_0 = 0.369 \text{ CC}/\text{O}$$

$$V_{01} = 0.3119 \text{ CC}/\text{O}$$

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE SAMPLE HOLDER AND STANDARD MATERIAL.

TABLE

RHO0	US	UP	P	V/V0	US(ST)
2.71	5.37	2.06	300	0.616	7.72
2.71	6.07	2.53	416	0.583	8.32
2.71	6.74	3.07	559	0.545	9.00
2.72	7.03	3.33	637	0.526	9.33

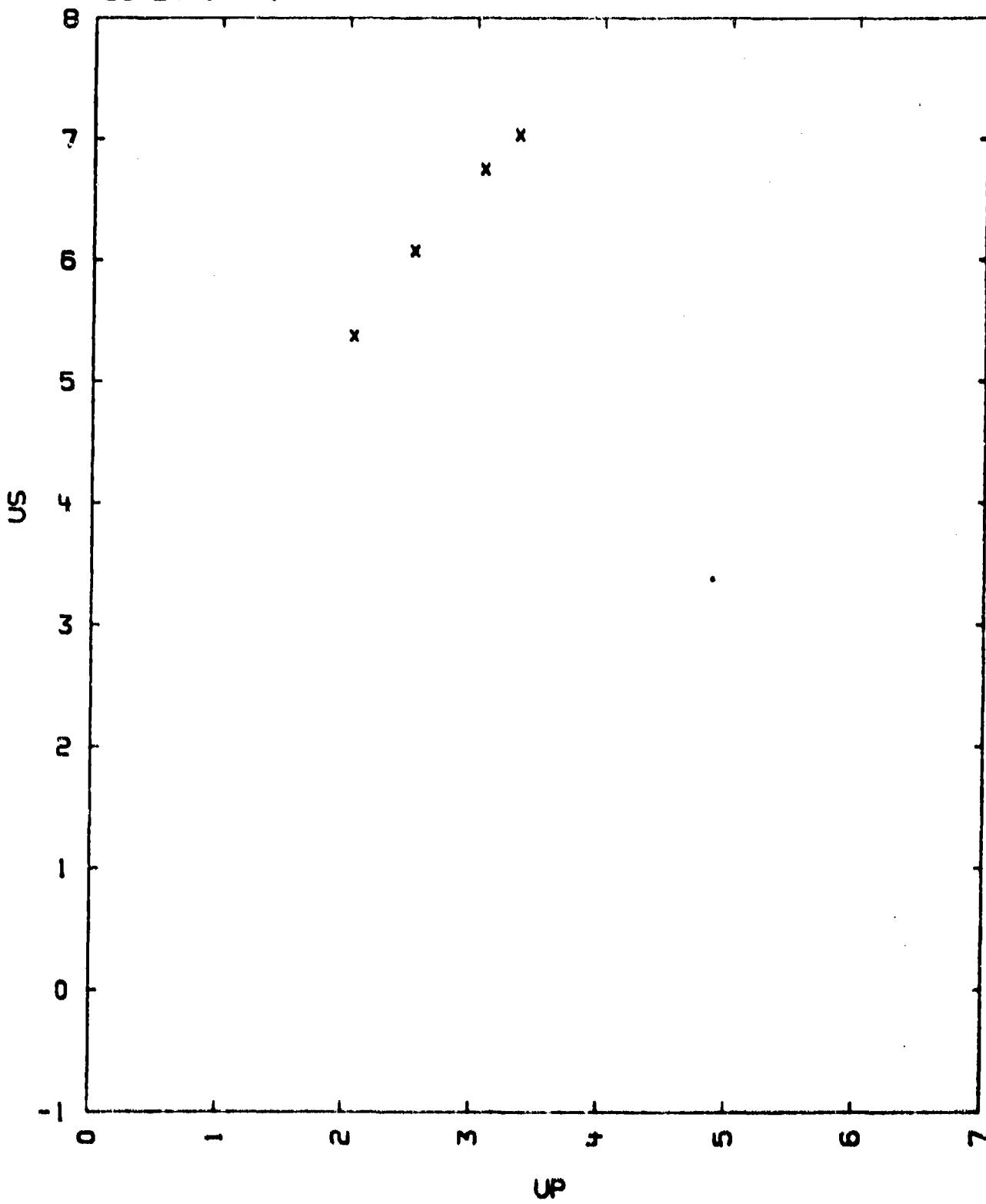
$$US = 2.710 + 1.304 \cdot UP \text{ KM/SEC.}$$

$$\text{SIGMA US} = 0.051 \text{ KM/SEC.}$$

COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.
PRIVATE COMMUNICATION
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) V01 WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED IN CRYSTAL DATA DETERMINATIVE TABLES (AMERICAN CRYSTALLOGRAPHIC ASSN. MONOGRAPH 5, 1963) 2ND ED.
- 4) FURTHER WORK IN PROGRESS

TABLE I
ENSTATITE CERAMIC (MAGNESIUM METASILICATE)
93-24-1---1



93-24-1---2

FORSTERITE CERAMIC (MAGNESIUM ORTHOSILICATE)

M02-51-04

V0 = 0.527 CC/G

VO1 = 0.3103 CC/G

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE SAMPLE HOLDER AND STANDARD MATERIAL.

TABLE

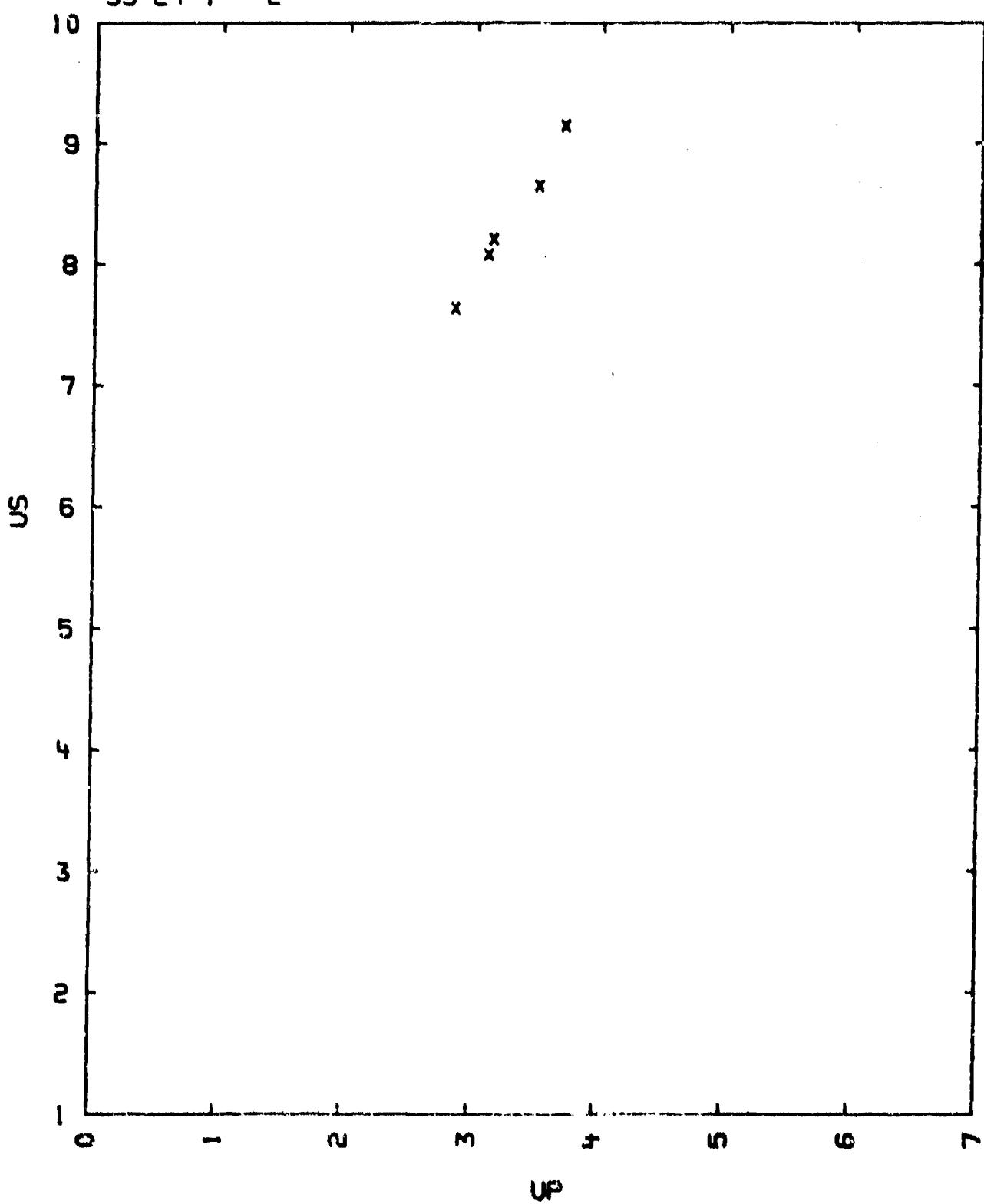
RHO0	US	UP	P	V/V0	US(ST)
3.07	7.63	2.84	664	0.629	9.05
3.03	8.07	3.10	758	0.616	9.40
3.03	8.07	3.10	758	0.616	9.40
3.07	8.20	3.14	788	0.618	9.48
3.04	8.64	3.50	919	0.595	9.95
3.06	9.14	3.70	1035	0.594	10.28

US = 2.884 + 1.674*UP KM/SEC.
 SIGMA US = 0.067 KM/SEC.

COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.
 PRIVATE COMMUNICATION
 LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B
 DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) VO1 HAS OBTAINED FROM THE LATTICE PARAMETERS LISTED IN CRYSTAL DATA DETERMINATIVE TABLES (AMERICAN CRYSTALLOGRAPHIC ASSN. MONOGRAPH 5, 1963) 2ND ED. THE ORTHOROMBIC CELL WITH A = 5.980 B = 10.20 AND C = 4.756 ANGSTROM WAS USED.
- 4) FURTHER WORK IN PROGRESS

TABLE I
FORSTERITE CERAMIC (MAGNESIUM ORTHOSILICATE)
93-24-1---2



93-24-1---3

FORSTERITE (OLIVINE) POLYCRYSTALLINE

MO2-51-04

$$V_0 = 0.321 - 3.81 \text{ CC}/\text{G}$$

$$V_{01} = 0.3103 \text{ CC}/\text{G}$$

THE TABLES LIST RHO0 IN G/CC., VELOCITIES IN KM/SEC AND P IN KBAR. MAT IS THE IMPACTOR AND STANDARD MATERIAL. THE DU AND DUS VALUES ARE UNCERTAINTIES

TABLE IA

NO	SAMPLE						IMPACTOR	
	US1	DUS1	UP1	US2	DUS2	UP2	U	DU
1	5.91	0.03	0.031	4.19	0.05	1.01	1.201	0.005
2	5.82	0.08	-	4.21	0.04	1.03	1.17	0.04
3	5.83	0.05	-	4.98	0.08	1.21	1.42	

US =

TABLE IB

NO	SAMPLE						IMPACTOR	
	RHO0	P1	V1/V0	P2	V2/V0	D	MAT	
1	2.634	4.8	0.9948	113.	0.761	4.8	FS	
2	2.627	4.7	0.9947	116.	0.757	4.83	-	
3	2.633	4.7	0.9947	159.	0.7548	4.83	-	

TABLE II

RHO0	SAMPLE						IMPACTOR		
	US	DUS	UP	P	V/V0	D	MAT	U	DU
3.093	6.83	0.12	0.855	181.	0.875	6.27	FS	1.11	0.04
3.094	6.48	0.06	0.894	172.	0.868	6.26	-	1.107	0.005
3.087	6.74		0.897	187.	0.867	4.20	-	1.161	0.008
3.117	7.13	0.14	0.995	221.	0.860	4.54	-	1.305	0.01
3.119	7.28		0.975	222.	0.866	4.20	-	1.285	0.007
3.104	7.47	0.04	1.16	269.	0.845	6.25	-	1.53	0.02
3.102	7.33	0.09	1.35	307.	0.816	4.57	-	1.77	0.02
3.115	7.34	0.06	1.63	373.	0.778	4.54	-	2.132	0.007

$$U_0 = 7.28 + 0.036 \cdot UP \quad \text{FOR UP BETWEEN 1.35 AND 1.63}$$

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COMMENTS:

- 1) SOURCE: AHRENS, T.J., LOWER, J.H. AND LAGUS, P.L.
J. GEOPHYS. RES. VOL 78 P.518 (1971)
- 2) EXPERIMENTAL TECHNIQUE C1
DATA REDUCTION TECHNIQUE B
- 3) DATA REDUCTION IS BASED ON IMPEDENCE MATCH WITH TUNGSTEN ALLOY (90.4 PER CENT W, 4.65 PER CENT NI, 4.9 PER CENT CU) BASE PLATE. SYMMETRIC IMPACT WAS USED BY FIRING THE SAME ALLOY FLYER PLATE FROM A PROPELLANT GUN.
- 4) LOW DENSITY MATERIAL WAS PRESSED AGGREGATE OF FORSTERITE FROM ATOMERIC CORP. SMALL AMOUNTS OF AN AL BEARING PHASE, PROBABLY MO-AL₂-O₄ WERE INFERRED FROM MICROPROBE ANALYSIS OF THIS MATERIAL. THIS IMPURITY INCREASES RHO_D BY ABOUT 0.02 G/CC.
- 5) HIGH DENSITY MATERIAL WAS FUSED FROM OXIDES BY MUSCLE SHOALS ELECTROCHEMICAL CORP. IT CONTAINED 0.04 WT. PERCENT FE-SI, BUT LESS THAN 0.5 PER CENT FE IN THE FORSTERITE PHASE.
- 6) THE WEAK PRECURSOR OBSERVE IN THE SHOTS OF TABLE II WAS IGNORED IN THE DATA REDUCTION SINCE ITS STRESS WAS LESS THAN 5. KBAR AND UNCERTAIN
- 7) FOR THE HIGH DENSITY MATERIAL THE SECOND WAVE WAS ASSUMED TO BE INCIDENT ON MATERIAL WITH ZERO INITIAL VELOCITY AND PRESSURE.

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TABLE IA
FORSTERITE (OLIVINE) POLYCRYSTALLINE
93-24-1--3

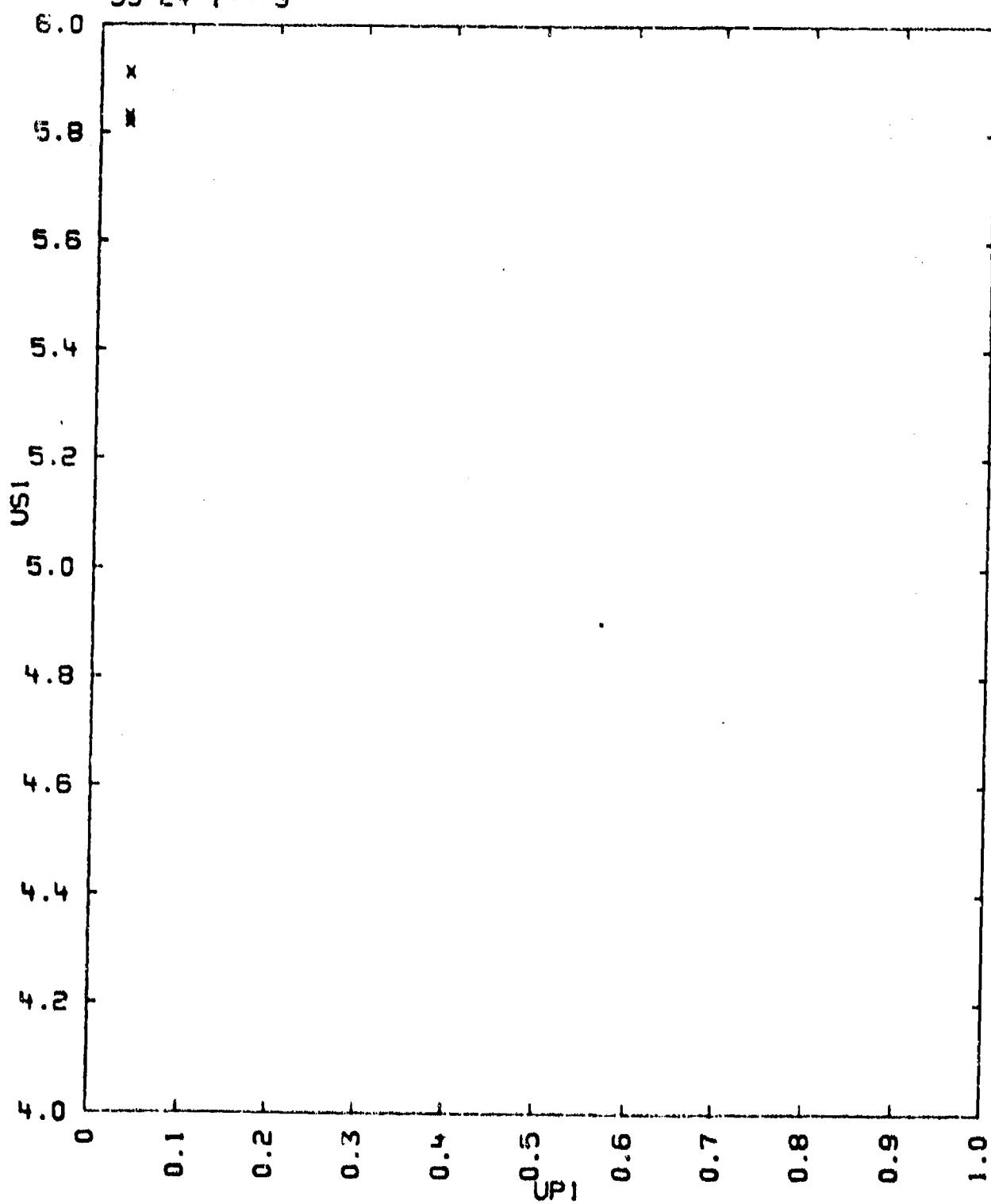


TABLE IA
FORSTERITE (OLIVINE) POLYCRYSTALLINE
93-24-1---3

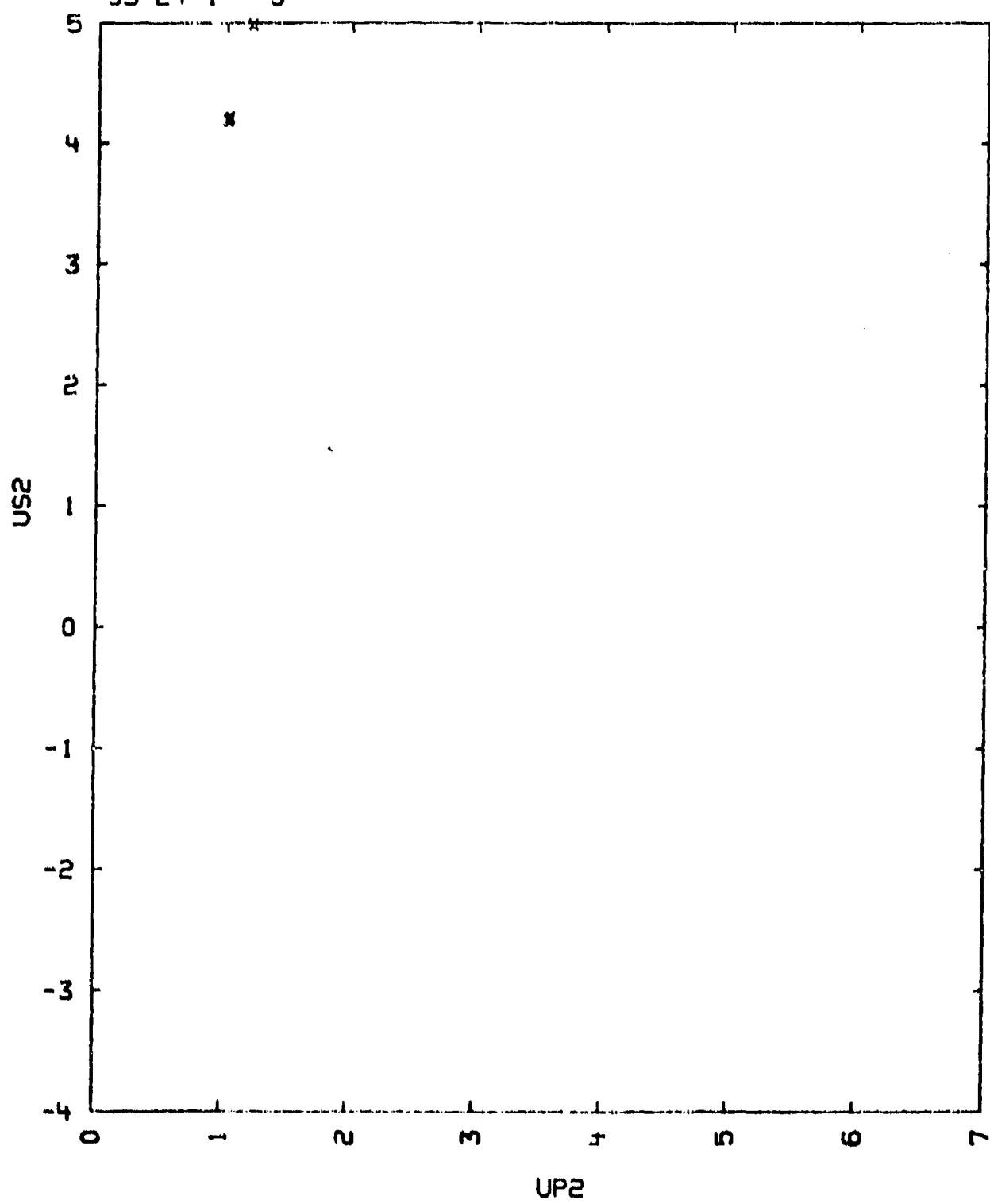
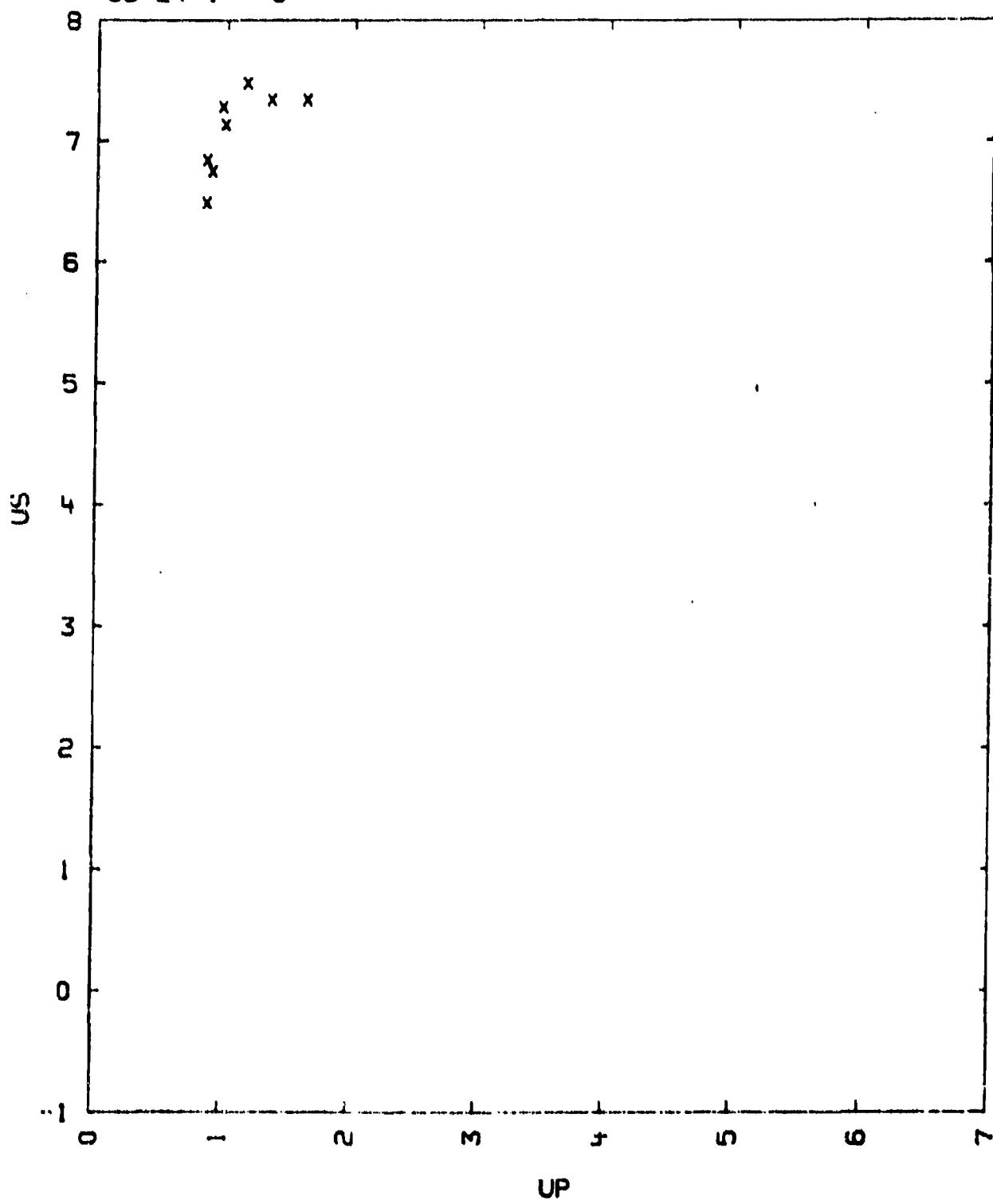


TABLE II
FORSTERITE (OLIVINE) POLYCRYSTALLINE
93-24-1---3



93-24-2-1-1-1

SERPENTINE, VER-MYEN (MAGNESIUM SILICATE-HYDROUS)

M06-S14-H8-018 = M06-S14-010-10-H18

$$V_0 = 0.357 \text{ CC/G}$$

$$V_{01} = 0.377 \text{ CC/G}$$

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN Kbars AND DENSITY IN G/CC. ST DESIGNATES THE SAMPLE HOLDER AND STANDARD MATERIAL.

TABLE

RH00	US	UP	P	V/V0	US(ST)
2.78	7.60	2.72	575	0.542	9.80
2.79	8.44	3.25	768	0.615	9.52
2.80	8.43	3.35	792	0.602	9.64
2.78	8.63	3.40	809	0.607	9.70
2.83	9.01	3.53	901	0.607	9.95
2.84	9.12	3.63	940	0.602	10.08

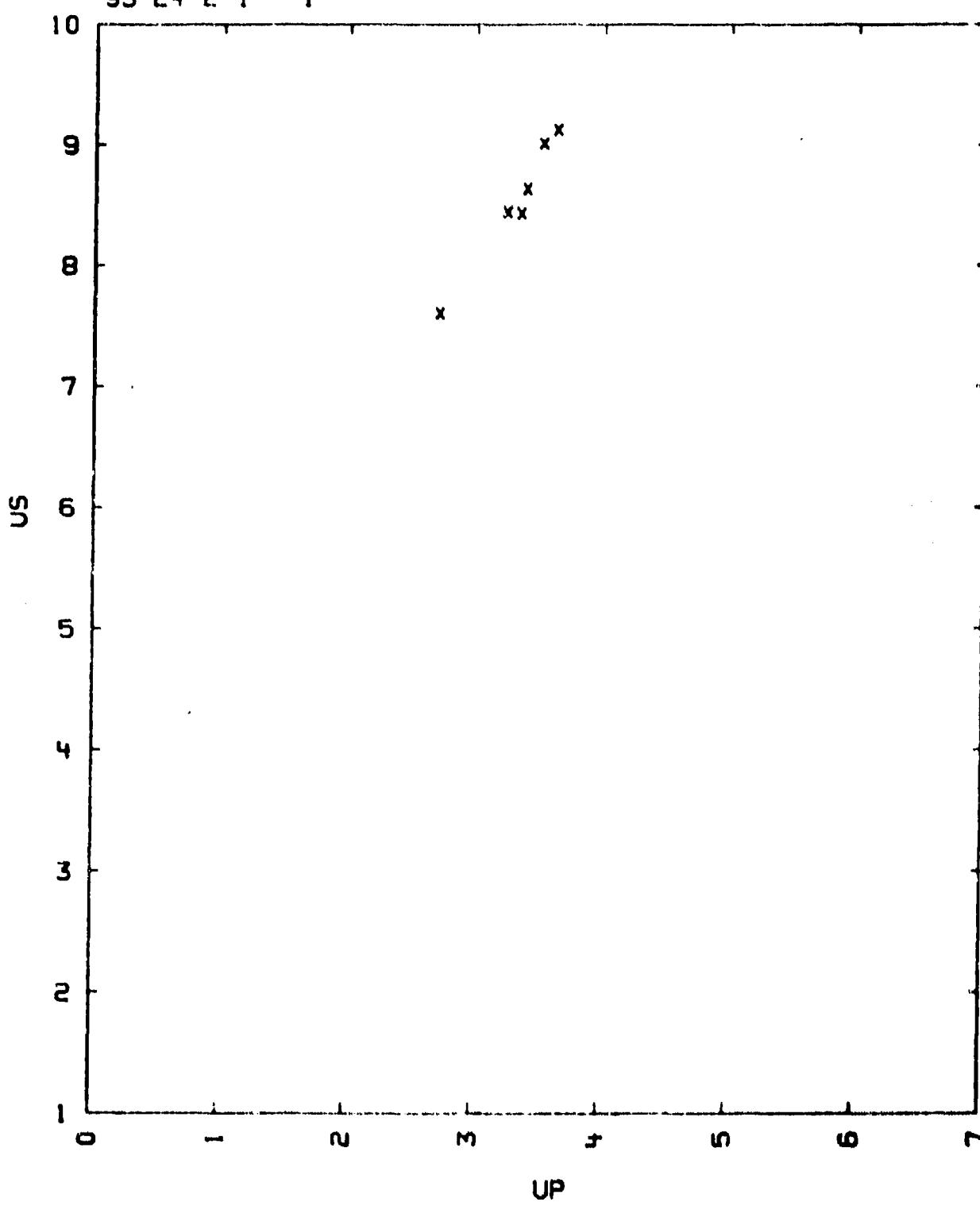
$$US = 3.017 + 1.666 \cdot UP \text{ KM/SEC.}$$

$$\text{SIGMA US} = 0.11 \text{ KM/SEC.}$$

COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.
PRIVATE COMMUNICATION
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) V01 WAS OBTAINED FROM DANAS MANUAL OF MINERALOGY (JOHN WILEY AND SONS INC. NEW-YORK, 1959)
- 4) FURTHER WORK IN PROGRESS

TABLE I
SERPENTINE, VER-MYEN (MAGNESIUM SILICATE-HYDROUS)
93-24-2-1---1



93-28-1--1

SPINEL (MAGNESIUM ALUMINATE CERAMIC)

MO-AL2-04

$V_0 = 6.294 \text{ TO } 6.292 \text{ CC}/\text{O}$
 $V_{01} = 6.2792 \text{ CC}/\text{O}$

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE STANDARD SAMPLE HOLDER MATERIAL.

TABLE

RHO0	US	UP	P	V/V0	US(ST)
3.41	8.46	2.35	678	0.722	8.76
3.42	8.54	2.53	740	0.762	9.00
3.43	9.08	2.79	871	0.763	9.40
3.43	9.09	2.80	871	0.763	9.40
3.43	9.16	2.85	896	0.763	9.49
3.43	9.13	2.86	894	0.762	9.49
3.41	9.41	3.05	979	0.631	9.78
3.42	9.62	3.19	1046	0.632	9.96
3.41	9.81	3.25	1098	0.631	10.08
3.40	9.76	3.29	1093	0.628	10.10
3.41	9.95	3.41	1158	0.629	10.20

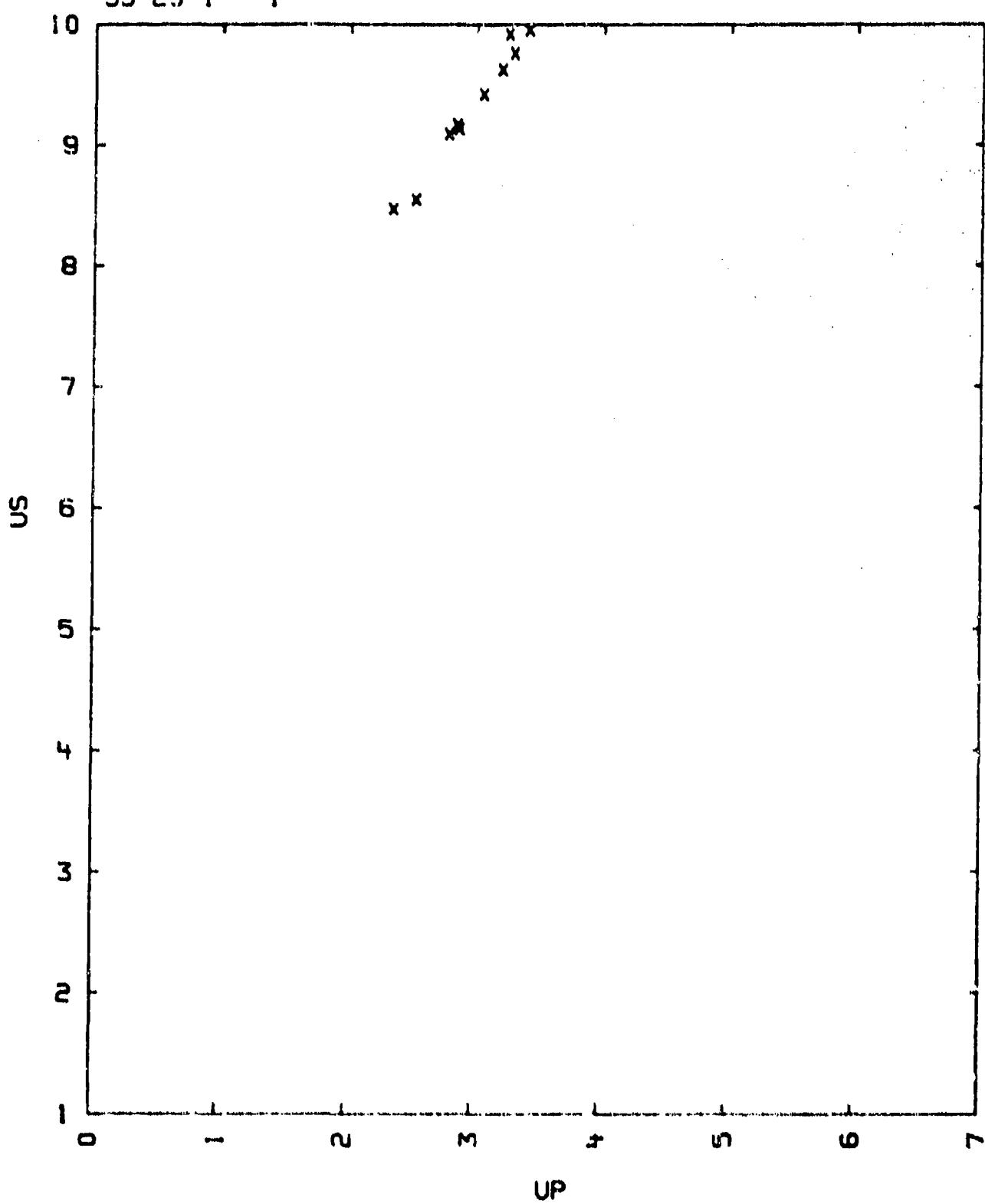
US = $4.838 + 1.511 \cdot UP$ KM/SEC.

SIGMA US = 0.078 KM/SEC.

COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.
PRIVATE COMMUNICATION
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) V01 WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED BY HYCKOFF,
CRYSTAL STRUCTURES, VOL. 3 (JOHN WILEY AND SONS, NEW YORK 1963)
- 4) FURTHER WORK IS IN PROGRESS.

TABLE I
SPINEL (MAGNESIUM ALUMINATE CERAMIC)
93-29-1---1



94-23-1---0
CALCIUMCARBONATE SUMMARY (CALCITE SUMMARY)

CA(C-03)

$$V_0 = 0.370 + 0.571 \text{ CC}/0$$

$$V_{01} = 0.3689 \text{ CC}/0$$

THE TABLE LISTS MUONIOT POINTS CALCULATED FROM THE FITS GIVEN BELOW.
UNITS ARE G/CC, KM/SEC, KBAR AND KBAR.CC/G FOR THE ENERGY DIFFERENCE.

TABLE

FIT	RHO0	US	UP	P	V/V0	E-E0
1	2.70	4.234	.4	45.7	0.805	.80
1	-	4.772	.7	90	0.853	2.45
1	-	5.310	1.0	143	0.912	5.0
2	-	5.397	1.1	160	0.796	6.05
2	-	5.818	1.4	220	0.759	9.8
2	-	6.238	1.7	286	0.727	14.4
2	-	6.656	2.0	359	0.700	20.0
1	2.58	3.834	.4	39	0.896	.80
1	-	4.390	.8	95	0.826	3.20
1	-	5.347	1.2	165	0.775	7.20
2	-	5.666	1.5	219	0.735	11.2
2	-	6.086	1.8	282	0.704	16.2
2	-	6.505	2.1	352	0.677	22.0
1	1.75	1.321	.5	11.5	0.621	1.25
1	-	2.603	1.0	45	0.615	5.0
1	-	3.885	1.5	102	0.614	11.2
1	-	5.167	2.0	181	0.613	20.0
1	-	6.448	2.5	282	0.612	31.2
2	-	4.637	2.2	178	0.525	24.2
2	-	5.196	2.6	236	0.500	33.0
2	-	5.756	3.0	302	0.479	45.0
2	-	6.455	3.5	395	0.458	61.2
2	-	7.155	4.0	501	0.441	80.

$$US = 3.553 + 1.786 \cdot UP - 3.66(2.71 \cdot RHO0) + 0.81(2.71 \cdot RHO0)^2 \cdot UP \quad (\text{FOR FIT 1})$$

$\Delta U, US = 0.15 \text{ KM/SEC. FOR THE LIMITS INDICATED BY THE TABLE.}$

$$US = 3.882 + 1.399 \cdot UP - 2.42(2.71 \cdot RHO0) \quad (\text{FOR FIT 2})$$

$\Delta U, US = 0.09 \text{ KM/SEC. FOR THE LIMITS INDICATED BY THE TABLE.}$

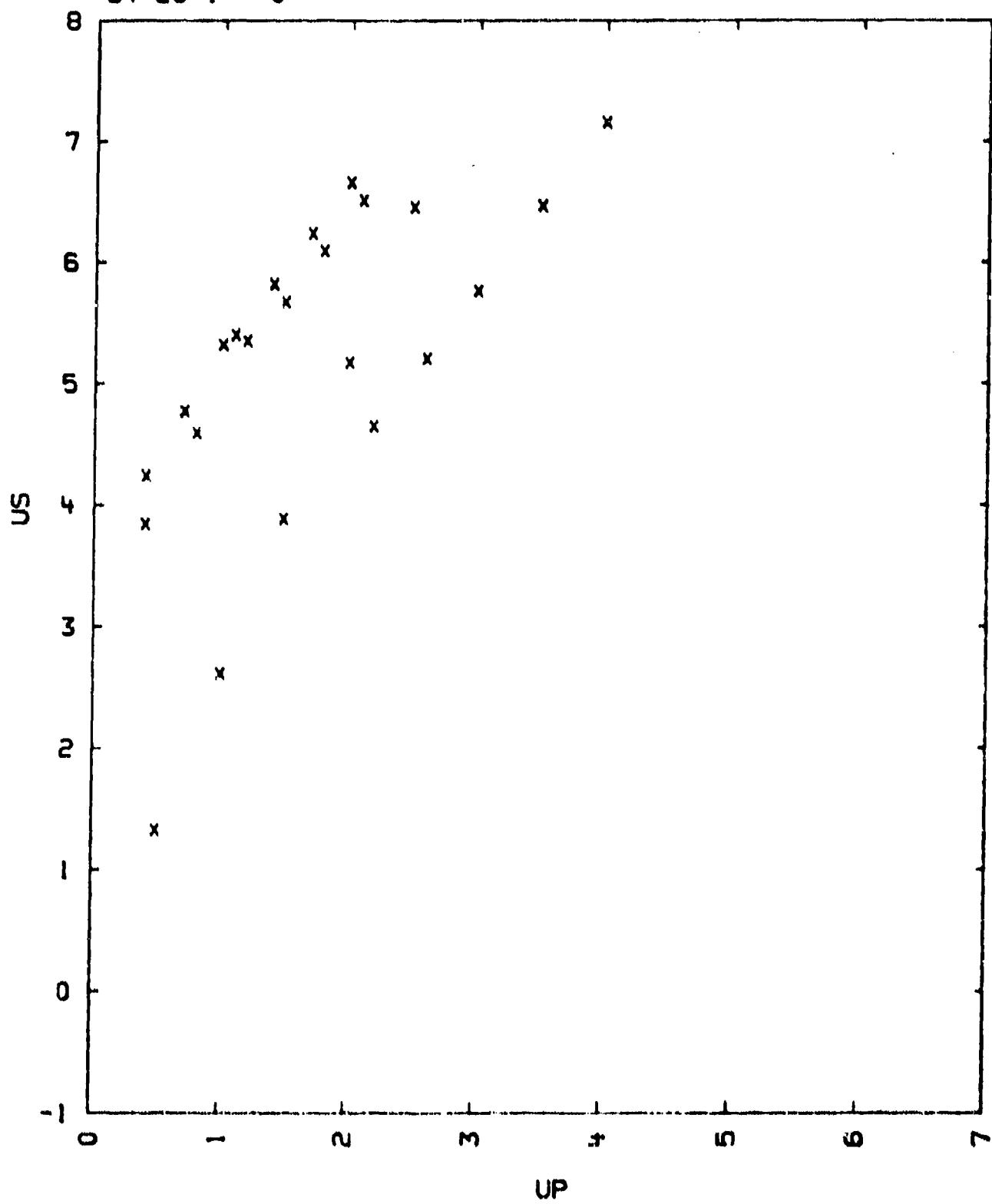
COMMENTS

1) SOURCE: COMPILER

DATA FROM PAGES 94-23-1---1,6 AND 7 WERE USED FOR THIS SUMMARY.

- 2) PAGE 94-23-1--5 INDICATES A LARGE NUMBER OF TRANSITIONS AT LOW PRESSURES. TABLE III OF THAT ENTRY GIVES THE BEST CALCITE RESULTS BELOW THE ABOVE TABULATED RANGE.
- 3) THE REMAINDER OF THE DATA SUFFERS FROM GREATER UNCERTAINTIES AND (OR) A LOWER PURITY.
- 4) VOI HAS BEEN CALCULATED FROM THE HEXAGONAL LATTICE CONSTANTS
 $A = 4.89008$ AND $C = 17.05851$ AT 18 DEG. K. WYCKOFF, CRYSTAL STRUCTURES, VOL 2 (INTERSCIENCE PUBL., N.Y. 1964) 2ND. ED.

TABLE I
CALCIUMCARBONATE SUMMARY (CALCITE SUMMARY)
94-23-1---0



94-23-1---1

MARBLE

CA(C-03)

$$V_0 = 0.370 \text{ CC}/\text{O}$$

$$V_{01} = 0.368 \text{ CC}/\text{O}$$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN MM/MICROSEC. AND PRESSURE IN KILOBARS.

TABLE

US	UP	P	V/V ₀
4.26	0.43	50	0.989
4.51	0.56	88	0.976
4.70	0.64	82	0.961
4.92	0.77	102.5	0.9475
5.18	0.90	129	0.926
5.26	0.92	131	0.923
5.47	1.125	168	0.794
5.51	1.17	174	0.7875
5.66	1.26	193	0.781
5.76	1.33	208	0.764
6.04	1.56	232	0.741
6.27	1.72	291	0.725
6.47	1.85	325	0.715
7.35	2.56	508	0.654

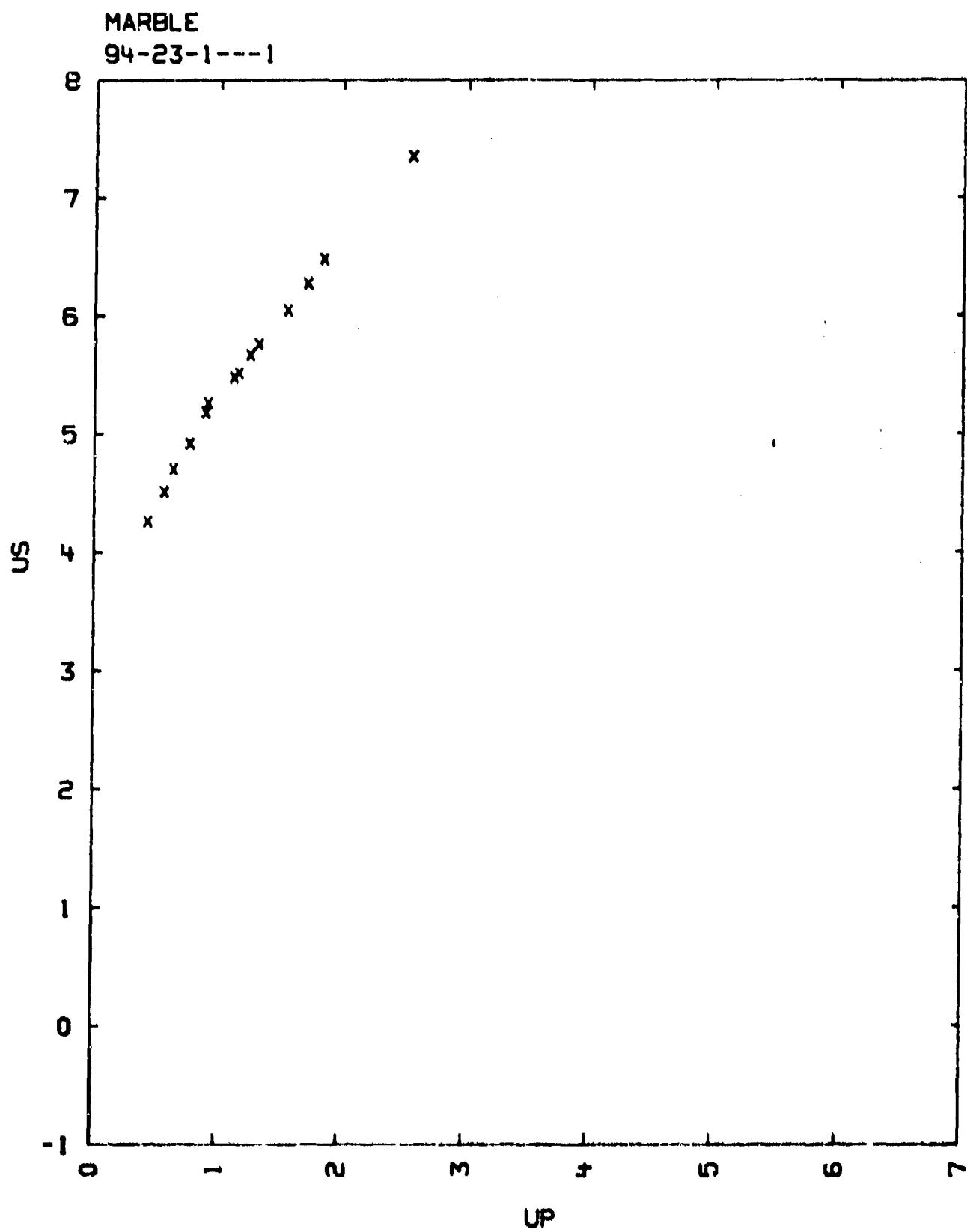
US *

COMMENTS:

- 1) SOURCE: DREMIN, A.N. AND ADADUKOV, G.A.
SOVIET PHYS.-DOKLADY, VOL. 4, P. 970 (1959)
SOVIET PHYS.-DOKLADY, VOL. 129, P. 261 (1959) (RUSS.)
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION TECHNIQUE B
- 3) IN THE ABOVE TABLE UNCERTAINTY IN VELOCITY IS 0.01 MM/MICROSEC.

006/14/77

TABLE I



94-23-1---2
MARBLE YULE

CALCITE(GRANULAR) CA(C-O3) 100 PERCENT
PARTICLE SIZE .2 TO .4 MM.
A FEW GRAINS AS LARGE AS 1.5 MM

T0 = 27 (+OR-) 3 DEGREES CENTIGRADE
V0 = .3721 CC/G
V01 = .3609 CC/G

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN MM/MICROSEC. AND PRESSURE IN KILOBARS.

TABLE

US1	UP1	P1	V1/V0	US2	UP2	P2	V2/V0
4.63	.396	49	.911				
4.21	.697	83	.841	3.537	.762	91	.814
5.73	.103	16	.967				
4.94	.796	104	.833	4.478	1.024	134	.787
				5.52	1.17	176	.785
				5.83	1.12	177	.803
				5.91	1.59	253	.728

US1 =

COMMENTS:

- 1) SOURCE: GREGSON, V.O., PETERSON, C.F. AND JAMIESON, J.C.
REPORT NO. AFCHL 63-662
STANFORD RESEARCH INSTITUTE, MENLO PARK, CALIFORNIA.
- 2) EXPERIMENTAL TECHNIQUE C
DATA REDUCTION TECHNIQUE B
- 3) ALL EXCEPT THE LAST TABLE ENTRY ARE COMPARATIVELY UNCERTAIN.
SOME OF THE ELASTIC WAVES INDICATED A SLOW RELAXATION EFFECT TO THE PLASTIC STATE.

106/14/77

TABLE I

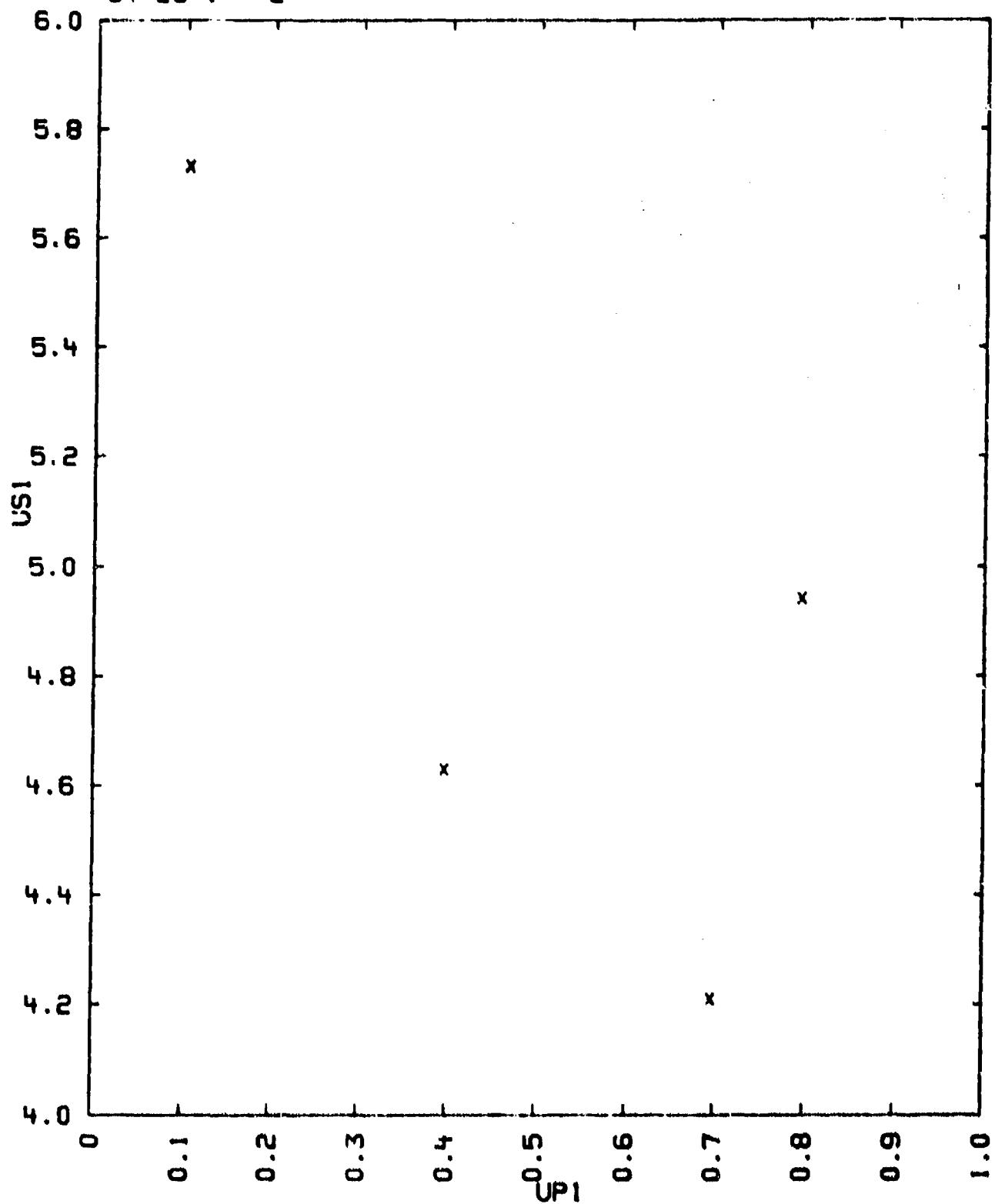
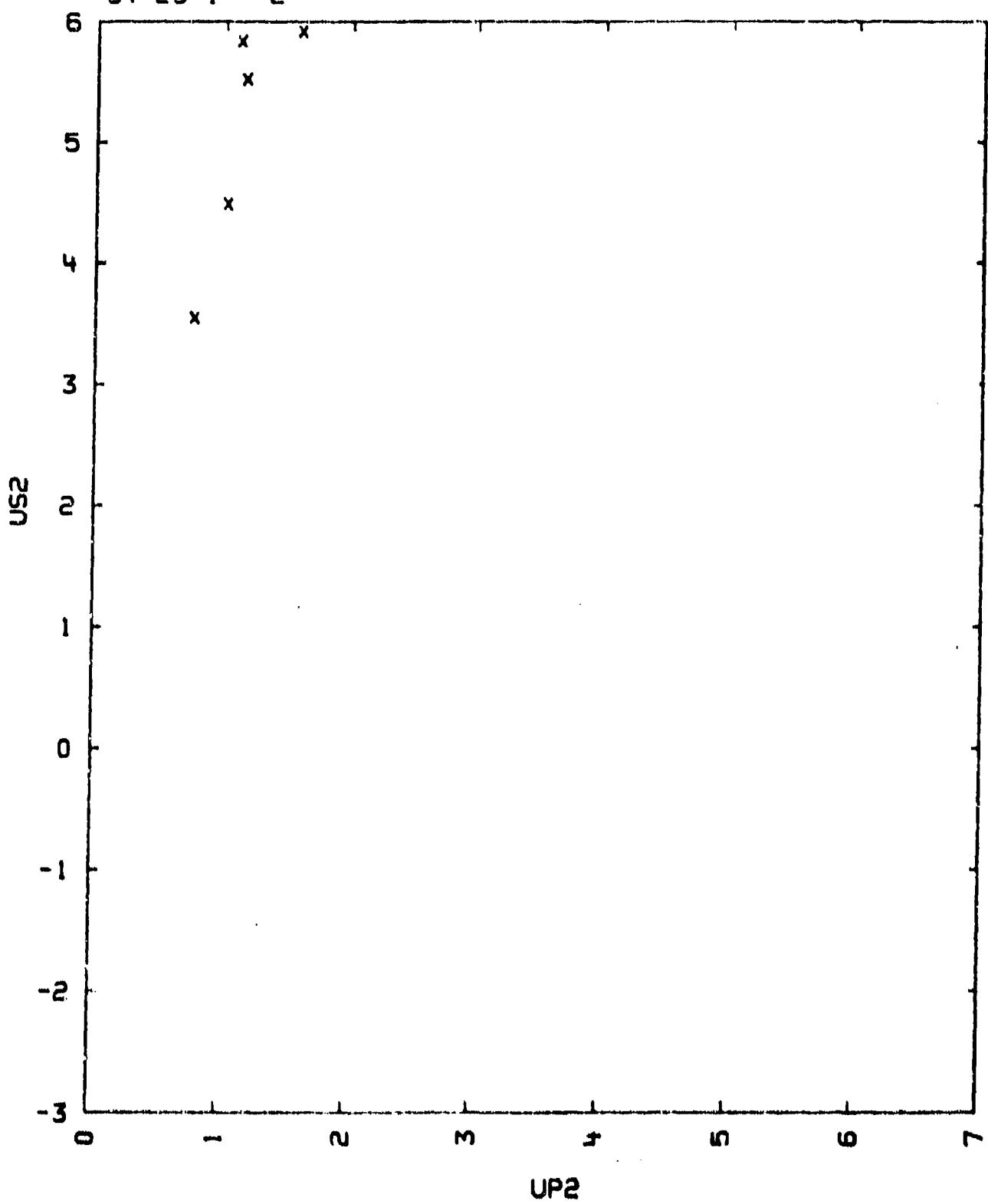
MARBLE YULE
94-23-1---2

TABLE I

MARBLE YULE
94-23-1---2



94-23-1---3
LIMESTONE SOLENHOFEN

CALCITE	Ca(C-O3)	96 PERCENT
CLAY		2 TO 3 PERCENT
QUARTZ	Si-O2	1 TO 2 PERCENT
POROSITY		0.2 TO 0.3 PERCENT
GRAIN SIZE		.005 TO .015 MM

$T_0 = 27$ (+OR-) 3 DEGREES CENTIGRADE
 $\rho_0 = 0.387$ CC/G

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN MM/MICROSEC. AND PRESSURE IN KILOBARS.

TABLE

US1	UP1	P1	V1/V0	US2	UP2	P2	V2/V0
5.330	.073	10	.987				
5.808	.108	13	.977				
3.585	.163	18	.961	3.094	0.441	42	.876
3.419	.223	24	.943				
3.342	.387	38	.844				
4.572	.820	97	.822	(1.238)	(3.666)	(134)	(.700)

US -

COMMENTS:

- 1) SOURCE: GREGSON, V.O., PETERSON, C.F. AND JAMIESON, J.C.
 REPORT NO. AFCRL 63-662
 STANFORD RESEARCH INSTITUTE, MENLO PARK, CALIFORNIA.
- 2) EXPERIMENTAL TECHNIQUE C
 DATA REDUCTION TECHNIQUE B
 THE ELASTIC WAVE (SUBSCRIPT 1) IS UNSTABLE AND SHOWS A STRONG STRAIN RATE DEPENDENCE.
- 3) THE VALUES IN PARENTHESES ARE UNCERTAIN RESULTS.

TABLE I

LIMESTONE SOLENHOFEN

94-23-1---3

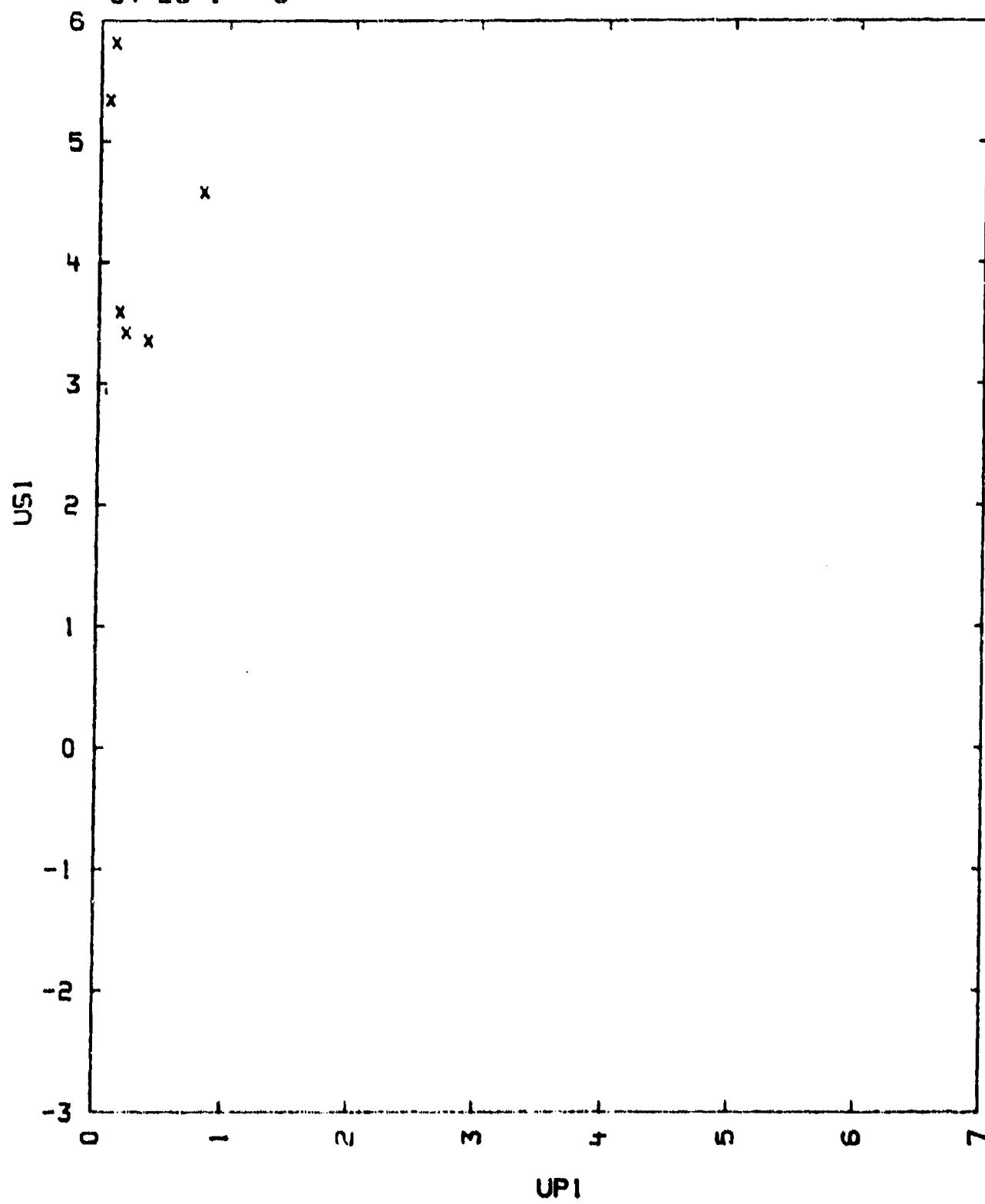
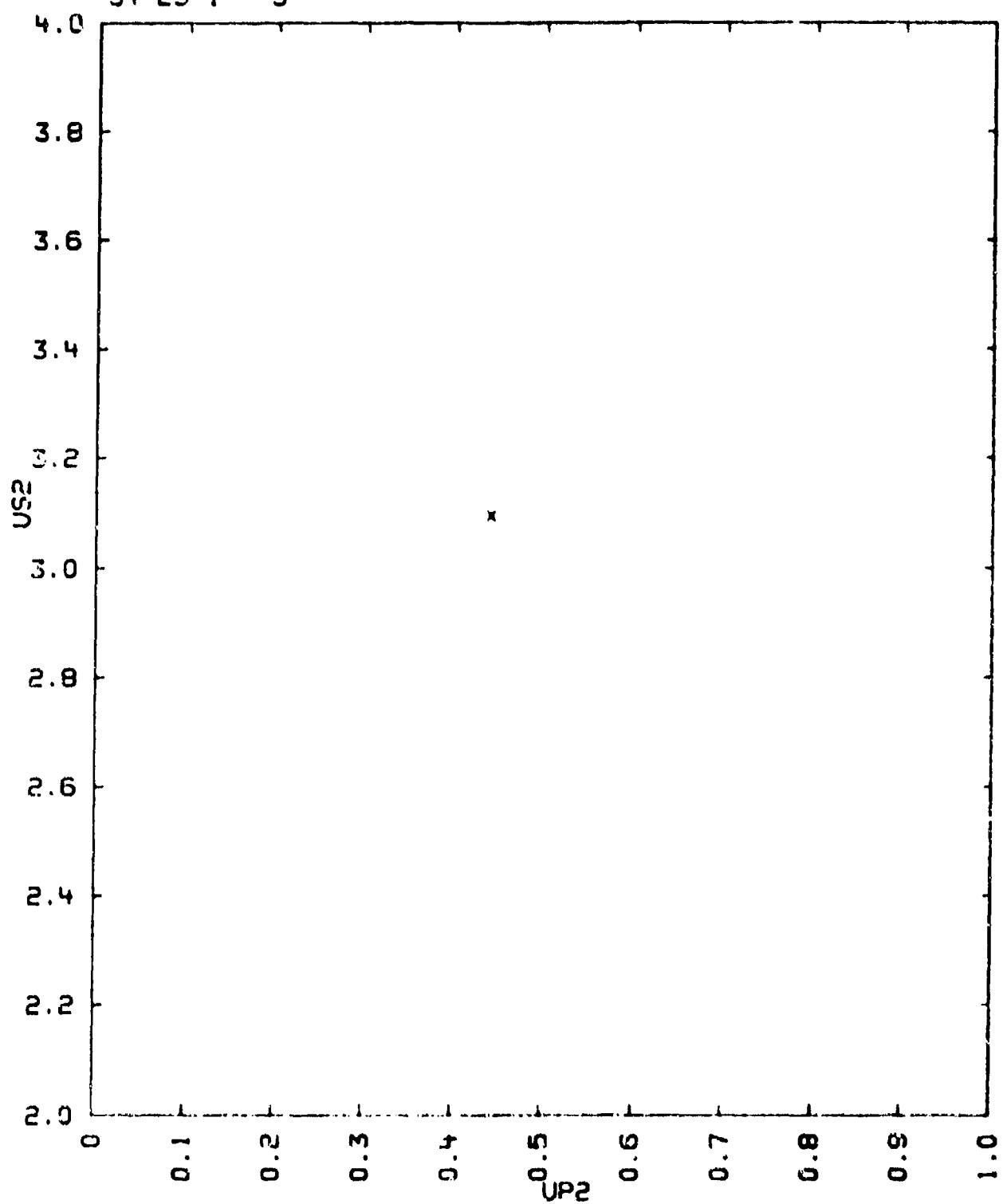


TABLE I

LIMESTONE SOLENHOFEN

94-23-1---3



94-23-1--4
MARBLE VERMONT

CALCITE	CAIC-03)	95 PERCENT.
QUARTZ	S1-02	5 PERCENT,
GRAIN SIZE		.05 TO .2 MM

$T_0 = 27$ 1+0R-1 3 DEGREES CENTIGRADE
 $V_0 = 0.372$ CC/O
 $V_{01} = 0.369$ CC/O

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN MM/MICROSEC. AND PRESSURE IN KILOBARS.

TABLE

U1	U1	P1	V1/V0	U2	U2	P2	V2/V0
5.262	.086	12	.984				
4.300	.165	21	.965	3.791	.378	43	.909
4.718	.123	15	.973				
3.98	.190	23	.957				
3.73	.352	39	.914	3.284	.443	47	.884

US -

COMMENTS:

- 1) SOURCE: GREGSON, V.O., PETERSON, L.F., AND JAMIESON, J.C.
 REPORT NO. AFCHL 63-662
 STANFORD RESEARCH INSTITUTE, MENLO PARK, CALIFORNIA.
- 2) EXPERIMENTAL TECHNIQUE C
 DATA REDUCTION TECHNIQUE B
- 3) THE QUARTZ IMPURITY OCCURRED IN ONE MM. BANDS THROUGHOUT THE SAMPLE.
- 4) THE PRESSURE ENTRY OF 23 KILOBARS IS IN A TRANSITION REGION BETWEEN TWO STATES AND CORRESPONDS TO AN UNSTEADY SHOCKWAVE.

TABLE I

MARBLE VERMONT
94-23-1---4

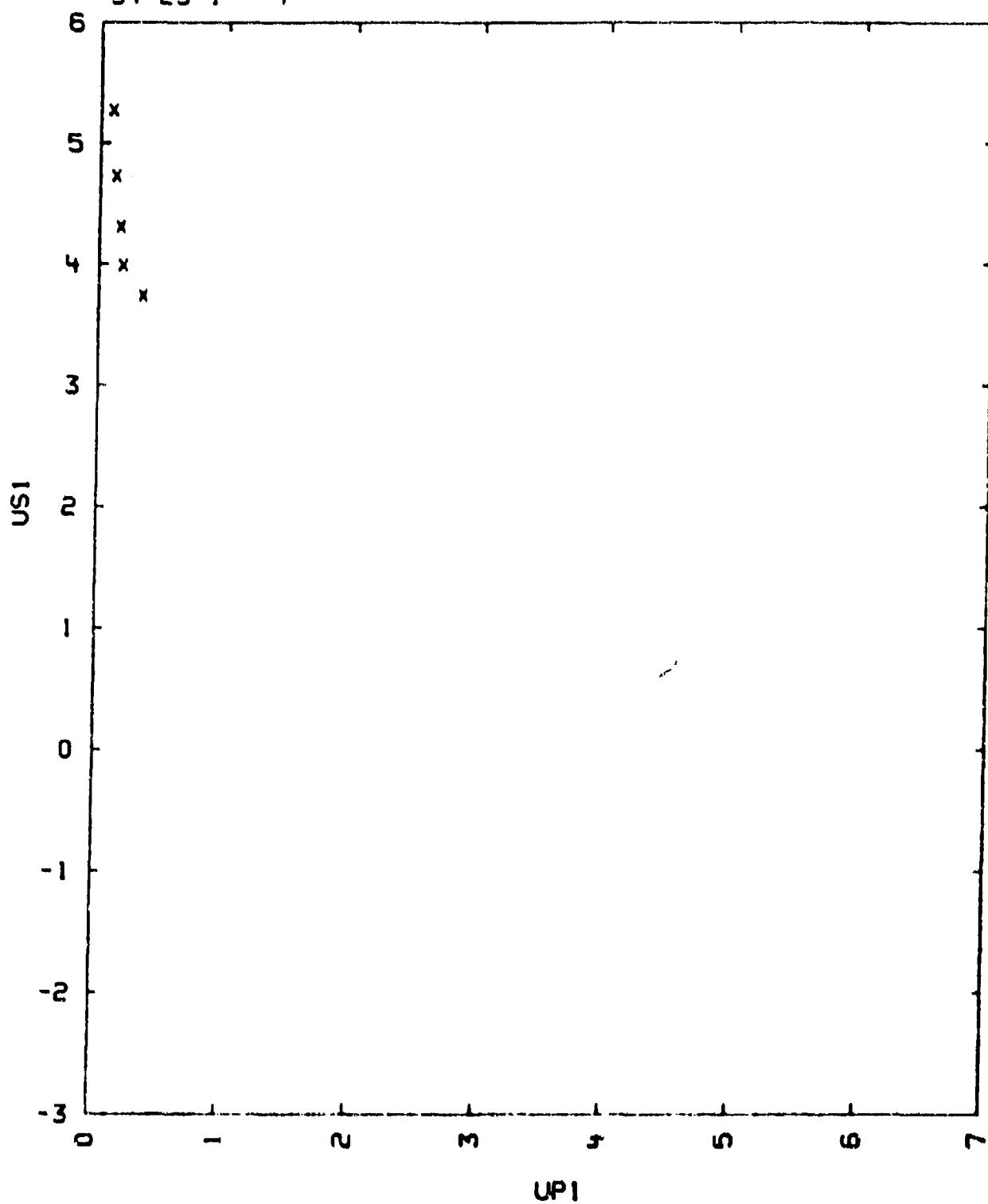
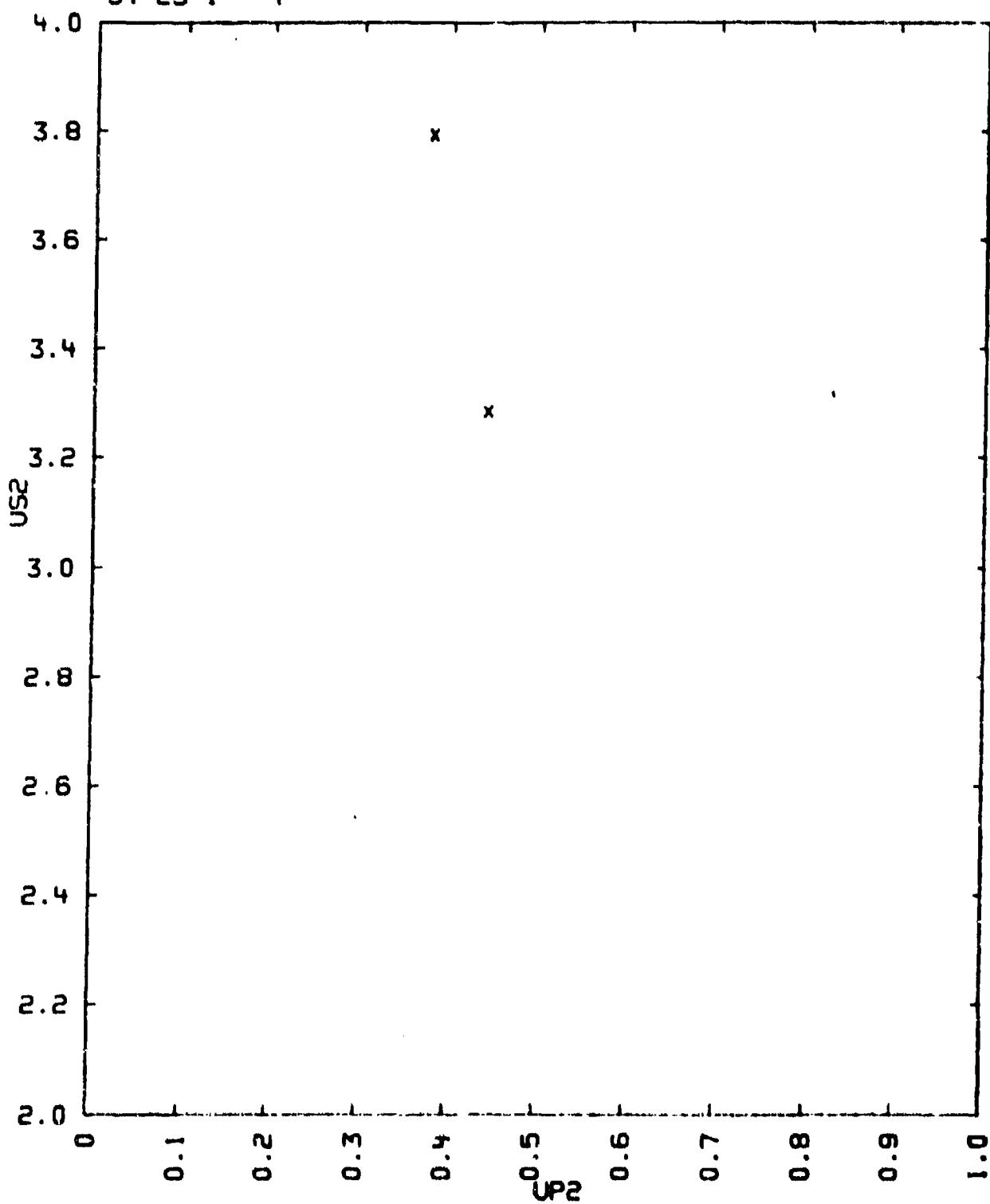


TABLE I

MARBLE VERMONT
94-23-1---4



94-23-1---5
 CALCITE (ICELAND SPAR SINGLE CRYSTAL)

CA-C-03 100 PERCENT

$$V_0 = 0.3689 \text{ CC/O} \quad CL(X\text{-CUT}) = 7.29 \text{ KM/SEC}$$

$$V_{01} = 0.3689 \text{ CC/O} \quad CL(Y\text{-CUT}) = 7.35 \text{ KM/SEC}$$

TABLE I LISTS THE SHOCK AND PARTICLE VELOCITIES OF VARIOUS SHOCK-FRONTS OBSERVED IN EACH EXPERIMENT. THE CRYSTAL CUT AND SHOCK FRONTS ARE PERPENDICULAR TO THE AXIS SHOWN IN COLUMN 2. CLE INDICATES THE NATURAL CLEAVAGE PLANE. ALL VELOCITIES ARE LABORATORY COORDINATES. UNITS ARE KM/SEC. SAMPLE THICKNESS D IS IN MM

TABLE I

SAMPLE											HOLDER
NO	CUT	D	US1	UP1	US2	UP2	US3	UP3	US4	UP4	UFS
1	CLE	10.066	7.13	0.081	5.04	0.134	3.86	0.193			1.1741
2	CLE	-	-	7.134	0.1144	3.952	0.2694				1.1520
3	CLE	9.245	7.068	0.0971	5.02	0.3331	4.639	0.6246			2.1754
4	X	6.224	6.852	0.1050	4.227	0.2173	3.605	0.3073			1.2824
5	X	6.274	6.886	0.1089	4.441	0.2280	3.572	0.3433			1.3777
6	X	6.096	7.041	0.1065	4.38	0.209	3.76	0.328	3.16	0.361	1.3823
7	X	6.121	6.789	0.1248	4.698	0.6817					2.499
8	X	5.215	7.40	0.132	5.24	0.346	4.42	0.664			
9	X	6.096	6.955	0.1202	4.740	0.6813	4.001	0.7702			1.478
10	X	6.322	6.493	1.3948							3.5187
A	X	-	7.363	0.13	6.283	1.54					*
B	X	-	7.277	-	6.163	1.46					
C	X	-	-	-	6.675	1.86					
11	Y	5.944	6.636	0.1179	4.33	0.785	3.33	0.284	2.86	0.351	1.438
12	Y	5.994	6.955	0.1352	4.290	0.2219	3.685	0.3180			1.2408
13	Y	6.198	7.082	0.1412	4.582	0.6874					2.4555
14	Y	5.967	7.044	0.1102	4.788	0.6137	4.336	0.7486			1.5377
15	Y	6.015	7.122	0.1448	4.765	0.5536	4.390	0.7481			1.4618
16	Y	6.175	6.206	1.4773							3.261
D	Y	-	7.45	0.12	6.06	1.435					
E	Y	-	-	-	6.630	1.77					
17	Z	8.001	5.451	0.1293	4.146	0.2357	3.682	0.3480	3.184	0.4051	1.4079
18	Z	8.001	5.407	0.1231	4.222	0.2210	3.591	0.3499			1.4422
19	Z	7.838	5.752	0.1100	5.13	0.596					2.3819
20	Z	11.024	5.384	0.206	4.652	0.7312					1.482
21	Z	17.366	5.750	0.1026	4.807	0.8368					1.4952
22	Z	6.091	5.583	0.1393	4.822	0.7692	4.051	0.8651			1.4087
23	Z	7.838	-	-	5.13	0.900					2.3989
24	Z	11.024	-	-	4.98	0.853	4.72	1.04			1.3998
25	Z	5.931	5.921	1.5155							
F	Z	-	8.09	1.47							
G	Z	-	6.702	1.87							

CALCITE (ICELAND SPAR SINGLE CRYSTAL)

NO CUT	D	US1	UP1	US2	UP2	US3	UP3	US4	UP4	UFS
--------	---	-----	-----	-----	-----	-----	-----	-----	-----	-----

US1 *

TABLE II LISTS PRESSURE IN KILOBARS AND VOLUME IN CC/G OF THE SAMPLES BEHIND THE ABOVE SHOCK FRONTS 1 THROUGH 4. THE LAST TWO COLUMNS GIVE THE PRESSURE AND MATERIALS OF THE SAMPLE HOLDERS. THESE ARE 12.5 MM PLATES OF FE = MILD STEEL, CH = LUCITE, AL = ALUMINUM, BR = BRASS

TABLE II

- - - - - SAMPLE - - - - -										- HOLDER -	
NO	P1	V1	P2	V2	P3	V3	P4	V4	MTRL	P	
1	16.	0.365	23	0.362	29	0.356			FE + CH	29	
2	22.1	0.3630	38.5	0.3483					FE + CH	24.5	
3	18.6	0.3638	50	0.346	86.8	0.3229			CH	55	
A	25.9	0.3624	265.	0.279							
B	25.6	0.3523	247.	0.282							
C	-	-	338.	0.266							
4	19.5	0.3632	32.3	0.3533	40.9	0.3439			FE + CH	27	
5	20.3	0.3630	34.6	0.3531	45.5	0.3409			FE + CH	29	
6	20.3	0.3633	32	0.354	44	0.343	47	0.339	BR + CH	30	
7	23.0	0.3621	93.3	0.3180					CH	67	
8	26.	0.362	57	0.347	94	0.320			AL		
9	22.7	0.3625	94.2	0.3185	103.4	0.2997			AL	130	
10	245.5	0.2898							AL	349	
11	21.2	0.3625	29	0.357	38	0.345	41	0.338	BR + CH	32	
12	25.5	0.3619	35.4	0.3542	44.8	0.3444			FE + CH	27	
13	27.1	0.3615	94.2	0.3170					CH	69	
14	21.0	0.3631	85.9	0.3240	101.4	0.3123			AL	136	
15	20.0	0.3614	80.2	0.3294	102.9	0.3127			AL	129	
16	247.9	0.2813							AL	342	
O	24.2	0.3630	239.	0.283							
E	-	-	320.	0.271							
17	19.1	0.3601	31.0	0.3506	42.0	0.3391	46.7	0.3323	FE + CH	31	
18	18.0	0.3603	29.2	0.3519	41.9	0.3384			FE + CH	32	
19	18.3	0.3612	93	0.328					CH	63	
20	30	0.3548	95.9	0.3120					AL	130	
21	18.0	0.3623	111.3	0.3050					AL	132	
22	21.0	0.3598	105.6	0.3097	113.6	0.3025			AL	129	
23			126.	0.3049					CH	63	
24			115.	0.305	139	0.290			AL	122.5	
25	246.0	0.2749							AL		
F	243.	0.280									
O	340.	0.266									

UO6/14/77

THE ABOVE DATA SUGGEST THE FOLLOWING PHASE TRANSITION POINTS ON THE HUGONIOT. THE BRACKETED VALUES INDICATE A LESS CLEAR CUT OBSERVATION.

TABLE III

	HUGONIOT ELASTIC LIMIT		1ST TRANSITION		2ND TRANSITION		3RD TRANSITION	
CUT	F1	V1	P2	V2	P3	V3	P4	V4
CLE	18.0	0.363				(50.5)(0.348)		
2	18.5	0.360	30.1	0.351	41.9	0.339	98.9	0.307
X	21.2	0.363	33.1	0.354	(50.4)(0.345)	94.2	0.318	
Y	23.7	0.362	32.2	0.354	(37.8)(0.345)	83.1	0.327	

COMMENTS:

- 1) SOURCE: GREGSON V. O., PETERSEN C. F., AND JAMIESON J. C.
 REPORT NO: SRI-POU-3630-STR-3 (1962)
 POULTER LABORATORIES
 MENLO PARK, CALIFORNIA
 ALSO: AHRENS T.J. AND GREGSON V.G. J. GEOPHYS. RES. NO64 P.4839 1959
 AHRENS T.J., ROSENBERG J.T. AND RUDERMAN M.H. (ENTRY A TO G)
 DYNAMIC PROPERTIES OF ROCKS
 PROJECT FOU-4B16 REPORT DATA 1968 (SEPT. 30 1968)
 STANFORD RES. INST., MENLO PARK, CALIF., U.S.A.
- 2) EXPERIMENTAL TECHNIQUE G1
 DATA REDUCTION METHOD B1 IN ENTRIES A,B,C,E AND G1 AND D1 FOR THE REST
 3) VO1 WAS OBTAINED FROM X RAY RESULTS OF SYNTHETIC CALCITE AT 18 DEGREE
 CENTIGRADE: A = 4.9898 AND C = 17.060 ANGSTROM WITH 6 MOLECULES
 IN THE HEXAGONAL UNIT CELL.
 ANDREWS STRUCTURE REPORTS VOL. XIII, PAGE 295. (1950)
- 4) THE FIRST SHOCK IN ENTRY 21 WAS ASSUMED TO BE THAT OF ENTRY 10 AND
 THE FIRST SHOCK IN ENTRY 22 WAS ASSUMED TO BE THAT OF ENTRY 15
 ALSO ASSUMED WERE UP1 OF ENTRIES A THROUGH C AND E; US1 OF C,E,F AND
 G; UNCERTAINTIES IN THESE LATTER ASSUMPTIONS AFFECT P,V VALUES NEOLY-
 GELY.
- 5) UPS VALUES OF A B C E AND G 12.94 2.90 3.46 AND 3.74 KM/SEC RESP. I
 INDICATE RAPID PHASE REVERSAL TO THE ORIGINAL LOW PRESSURE PHASE,
 SINCE 0.5UPS IS CLOSE TO UP MAX.
- 6) A VALUE OF 14 KBAR FOR THE FIRST PHASE CHANGE IS INDICATED BY ULTRA-
 SONIC MEASUREMENTS ON YAMATOGUCHI MARBLE (SHOJI KONDO ET.AL. J.PHYS.
 EARTH V.20 P.245 (1972))
- 7) CL VALUES FROM PESELNICK AND ROBBIE, J. APPL. PHYS. VOL. 34, 2494
 (1963).

TABLE I
CALCITE (ICELAND SPAR SINGLE CRYSTAL)
94-23-1---5

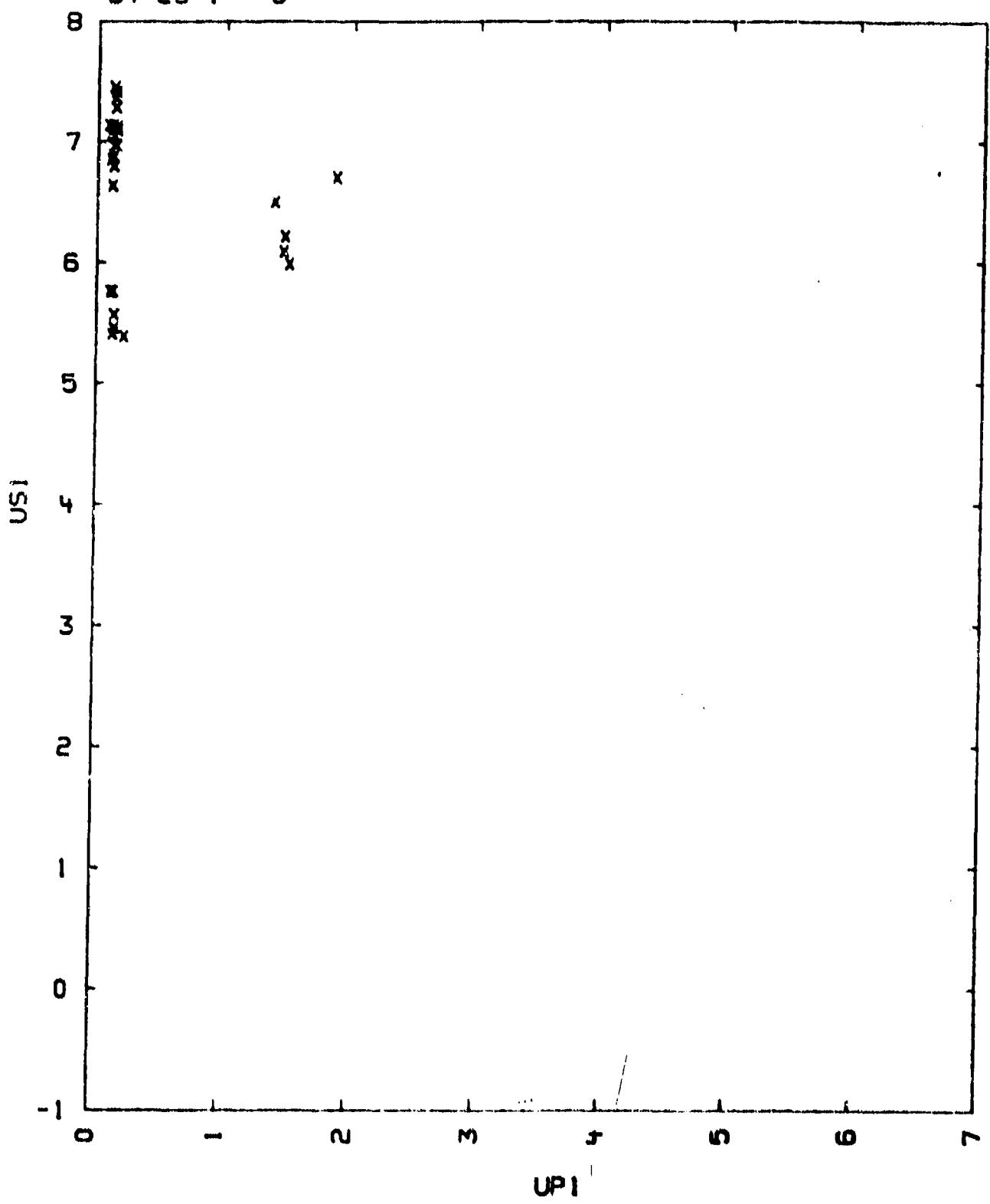


TABLE I
CALCITE (ICELAND SPAR SINGLE CRYSTAL)
94-23-1---5

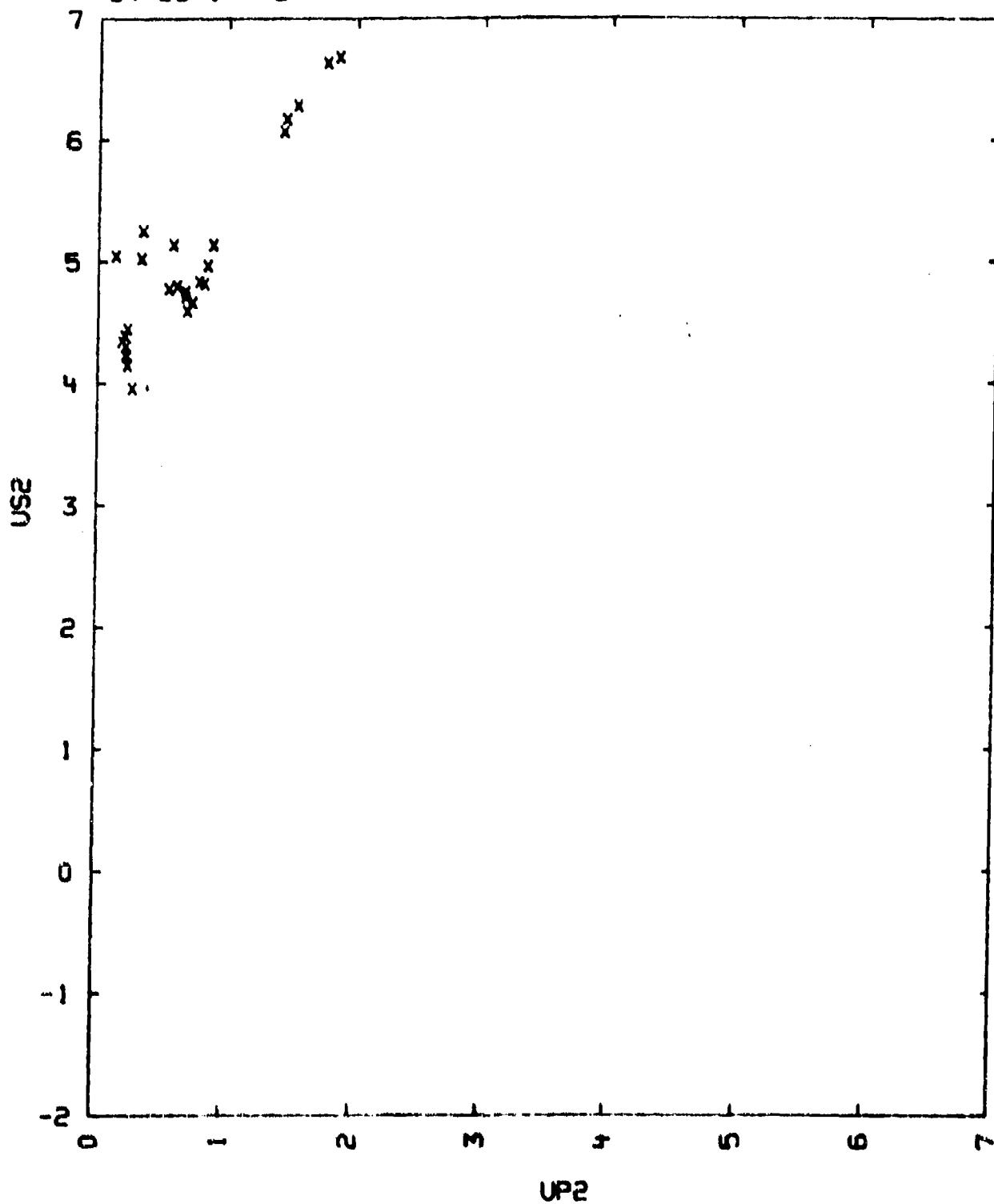


TABLE I
CALCITE (ICELAND SPAR SINGLE CRYSTAL)
94-23-1---5

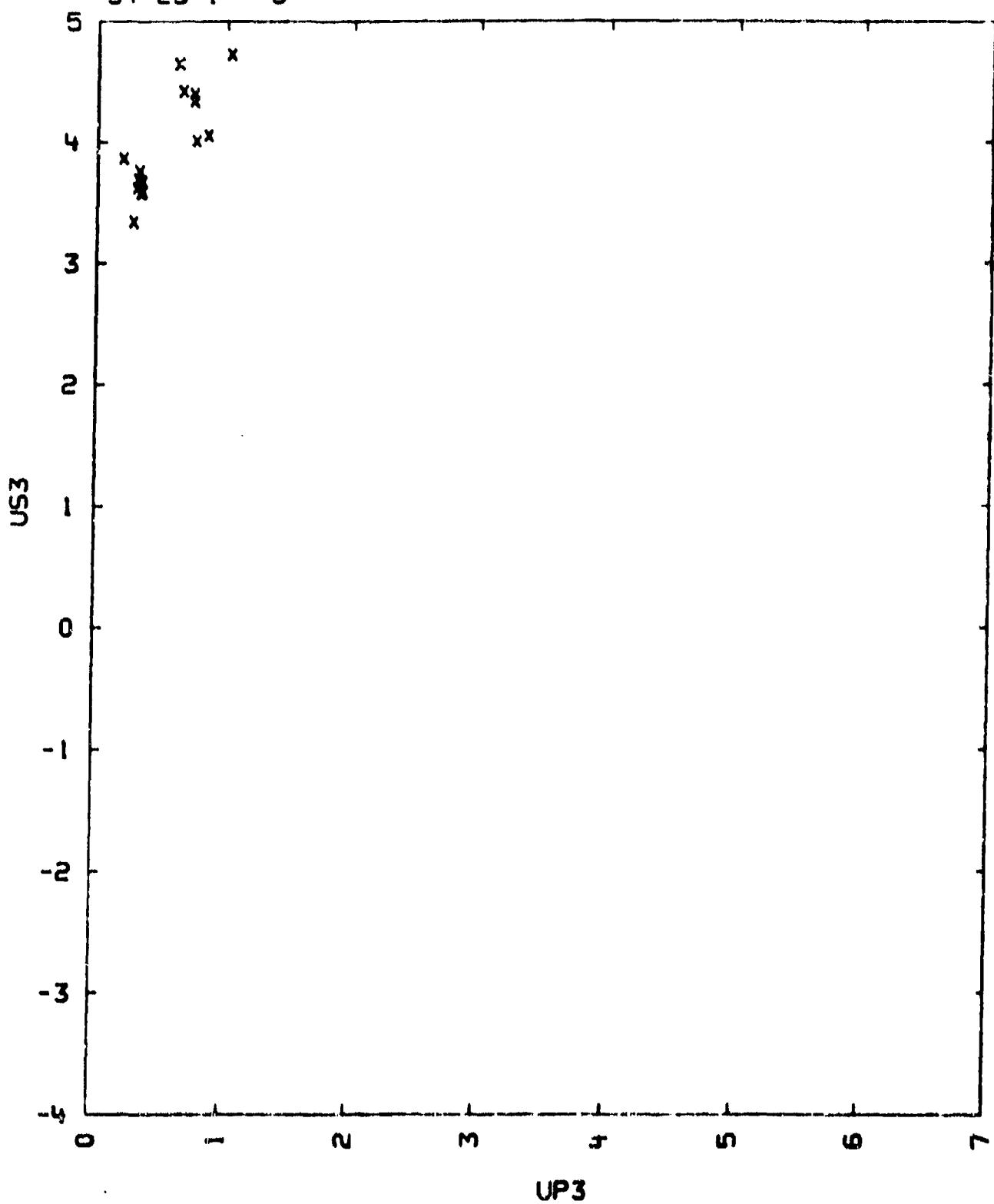
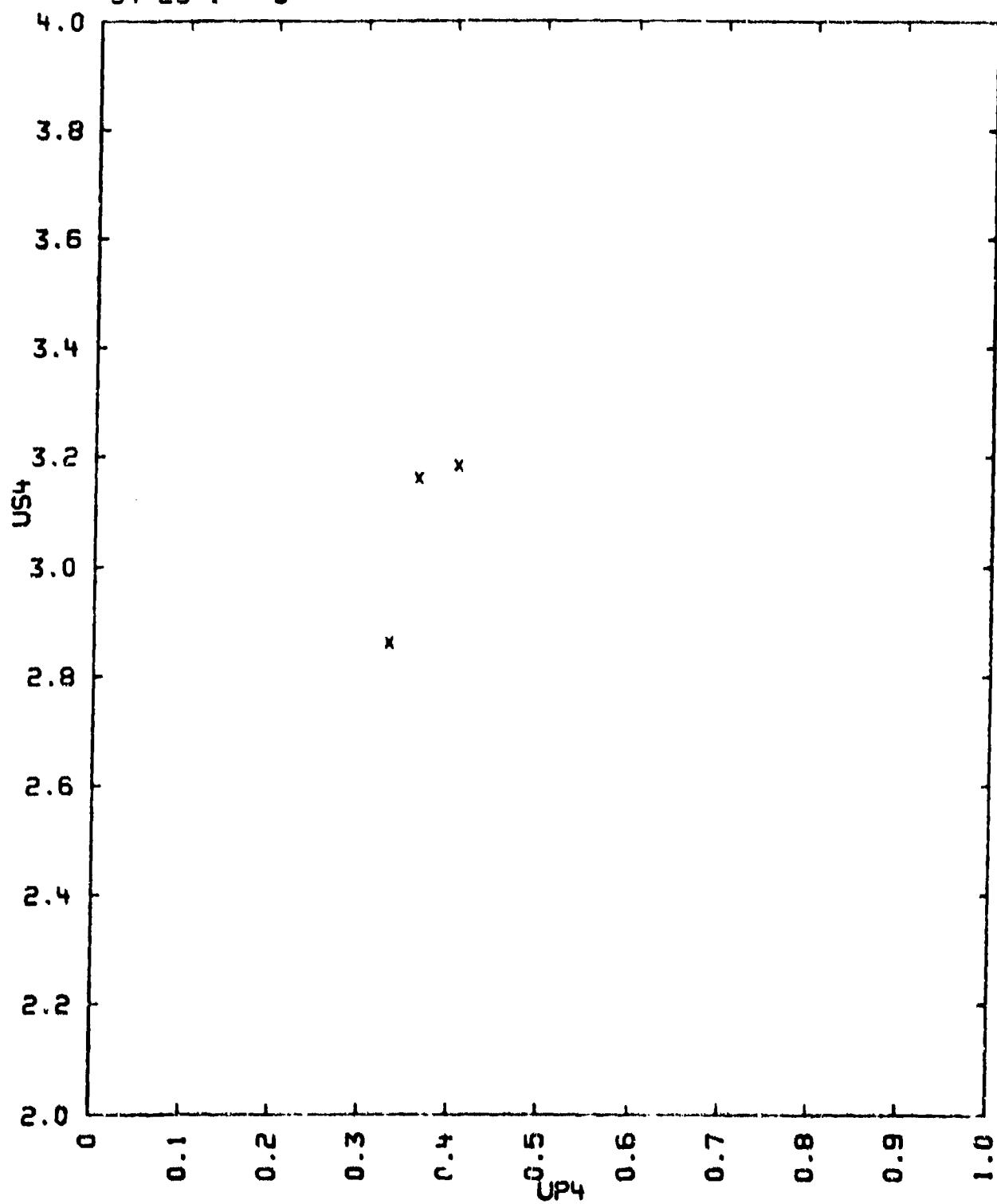


TABLE 1
CALCITE (ICELAND SPAR SINGLE CRYSTAL)
94-23-1---5



84-23-1---6
LIMESTONE SOLENHOFEN

CALCITE CA(C-O3) 100 PERCENT
AVERAGE GRAIN SIZE 0.01 MM
MAXIMUM GRAIN SIZE 0.02 MM

$$V_0 = 0.3869 \text{ CC/CC} \quad CL = 5.30 \text{ KM/SEC} \\ CS = 2.89 \text{ KM/SEC}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICROSEC,
AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UFS	UP	P	V/V0
2.590	4.33	1.30	0.69	78	0.841
2.597	5.33	2.25	1.17	162	0.781
2.597	5.27	2.22	1.18	161	0.776
2.598	5.69	2.82	1.48	218	0.740
2.594	5.67	2.81	1.50	220	0.735
2.560	6.41	3.87	2.11	347	0.670
2.566	5.72	3.12	1.63	240	0.715
2.573	9.04	7.37	3.87	900	0.572

US *

COMMENTS:

1) SOURCE: COMPILER

L.R.L. EQUATION OF STATE FILE (1965)

LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA

2) EXPERIMENTAL TECHNIQUE B

DATA REDUCTION TECHNIQUE B

STANDARD MATERIAL 2024 ALUMINUM

3) CHEMICAL ANALYSIS: C-03 56.7 PERCENT

CA 37.82 PERCENT

Mg LESS THAN 0.5 PERCENT

Fe 0.02 PERCENT

Si 0.62 PERCENT

Al 0.15 PERCENT (SPECTROGRAPH)

THE CHEMICAL ANALYSIS INDICATES THAT CALCIUM CARBONATE ACCOUNTS FOR APPROXIMATELY 95-97 PERCENT OF THE SAMPLE IF Si EXISTS AS Si-O4.

4) ANOTHER SOLENHOFEN SAMPLE WITH A RHO0 = 2.656 G/CC. YIELDED HIGHER SOUND VELOCITIES, D. S. HUGHES AND C. HAURETTE, REVUE DE L'INSTITUT FRANCAIS DU PETROLE ET ANNALES DES COMBUSTIBLES LIQUIDES, VOL. XII, P. 730. (1957)

P = 1. 100 250 500 1000 1500 2000 3000 4000 5000 BARS

CL = 5.97 6.00 6.01 6.02 6.05 6.06 6.08 6.11 6.12 6.13

CS = 2.88 2.95 2.98 2.99 3.01 3.01 3.02 3.02 3.05 3.04

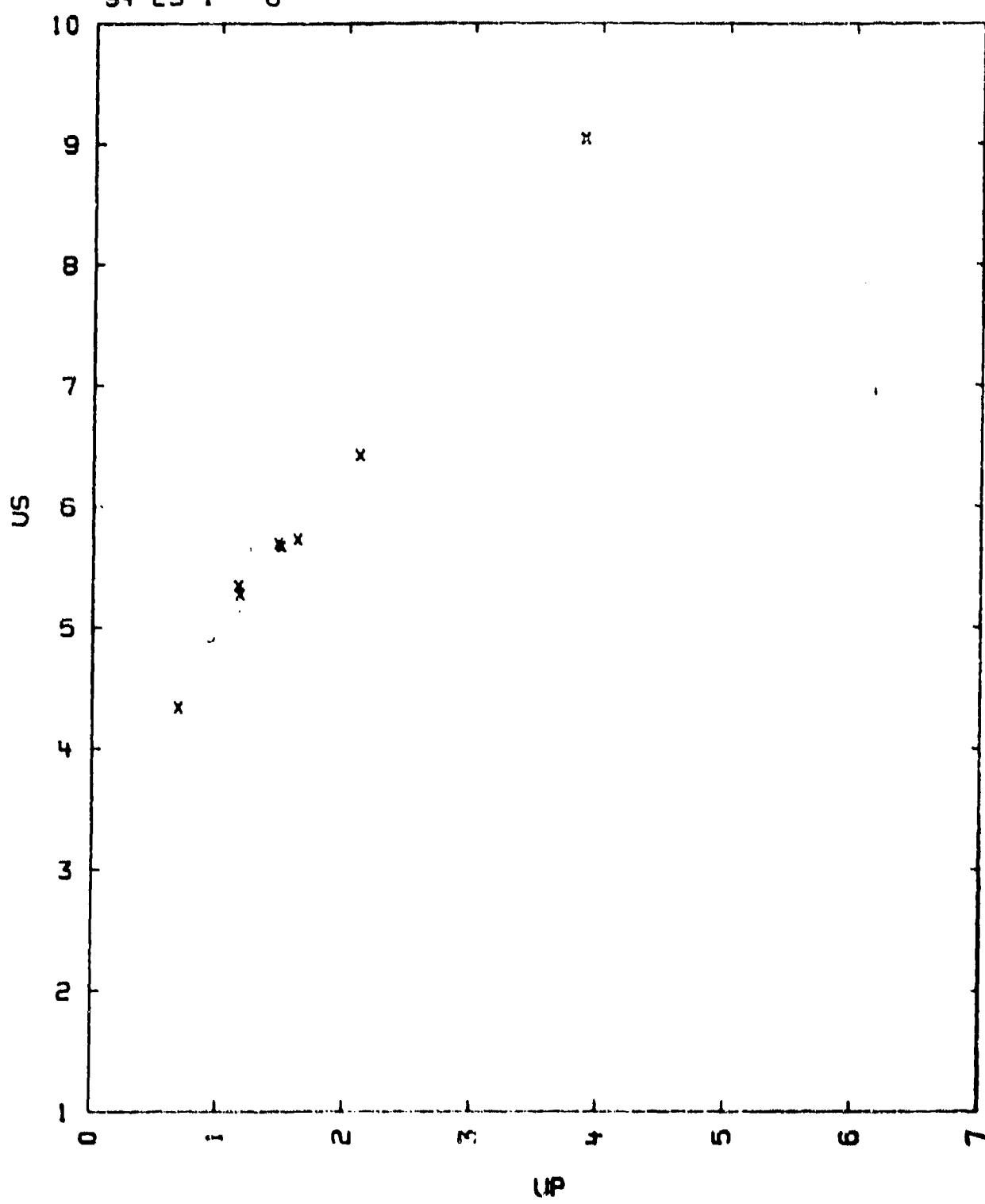
ALL VELOCITIES IN KM/SEC.

UOG/14/77

TABLE I

LIMESTONE SOLENHOFEN

94-23-1---6



94-23-1---7
LIMESTONE (CALCIUM CARBONATE)

CA-C-O3	98.2	PERCENT BY WEIGHT		
H ₂ O	0.03	-	-	-
MG	0.20	-	-	-
SI-O2	0.62	-	-	-
MN	0.02	-	-	-
FE	0.07	-	-	-
P	0.22	-	-	(AS P-04)
SR	TRACE			
CL	-			
CU	-			
TI	-			
NA	-			
K	-			
VOIDS	35	PERCENT BY VOLUME		

$$\rho_0 = 2.574 \text{ g/cc.}$$

$$\rho_{01} = 2.3689 \text{ g/cc.}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITY IN KM/SEC.,
AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UP	P	V/V0
1.75	1.59	0.58	16	0.635
-	1.53	0.56	15	0.634
-	1.90	0.81	27	0.574
-	1.97	0.79	27	0.593
-	2.97	1.04	54	0.613
-	2.76	1.14	55	0.587
-	4.00	1.52	106	0.620
-	4.23	1.51	112	0.643
-	4.12	1.67	120	0.595
-	4.38	1.67	128	0.619
-	4.35	1.74	132	0.600
-	4.70	2.28	187	0.515
-	4.06	2.34	199	0.516
-	5.84	3.14	321	0.462
-	6.22	3.26	355	0.476
-	6.67	3.54	413	0.469
-	6.67	3.60	444	0.430

$$US = 0.587 + 1.240 UP + 0.718 UP^2 \text{ KM/SEC. } \sigma US = 0.20 \text{ KM/SEC.}$$

FOR UP FROM 0.58 TO 1.52 KM/SEC.

$$US = 2.151 + 1.214 UP \text{ KM/SEC. } \sigma US = 0.17 \text{ KM/SEC.}$$

FOR UP FROM 1.6 TO 3.8 KM/SEC.

COMMENTS:

- 1) SOURCE: HART AND SKIDMORE I. C.

PRIVATE COMMUNICATIONS (1965)

BERKSHIRE, ENGLAND.

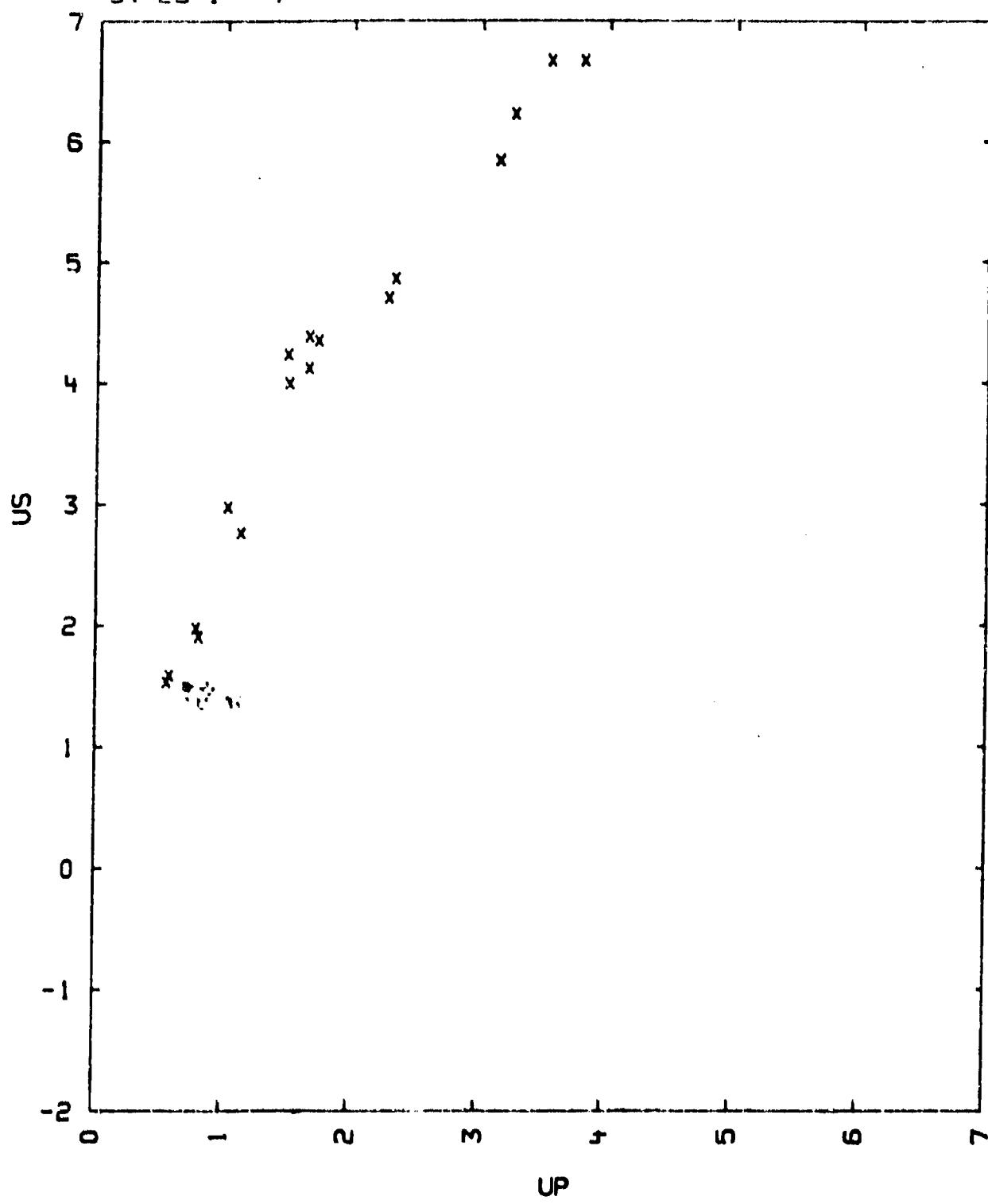
ATOMIC WEAPONS RESEARCH ESTABLISHMENT, ALDERMASTON.

- 2) EXPERIMENTAL TECHNIQUE A.
DATA REDUCTION TECHNIQUE B.
ALUMINUM, IRON, AND STEEL WERE USED AS STANDARDS.
- 3) THE POROSITY WAS DETERMINED BY ASSUMING THE SAMPLES TO BE PURE CALCIUM CARBONATE AND TAKING A CRYSTAL DENSITY OF 2.71 G/CC.
- 4) VOI WAS CALCULATED FOR PURE CALCIUM CARBONATE USING THE LATTICE CONSTANTS, $A = 4.9898$ AND $C = 17.060$ ANGSTROMS AT 18 DEG. CENTIGRADE FOR A HEXAGONAL CELL.
A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION, POLYCRYSTAL BOOK SERVICE, BROOKLYN, N.Y., 1963) 2ND ED.
- 5) THE SAMPLES WERE OBTAINED FROM THE SALISBURY PLAIN.
- 6) ANOTHER FIT OF THE LOW PRESSURE DATA USING OTHER THEORETICAL CONSIDERATIONS IS: $UP = (0.384 US)/(\lambda - 0.0003 US^{2.1})$ KM/SEC.
NO PHYSICAL SIGNIFICANCE IS ATTACHED TO THE DISCONTINUITY AT $UP = 1.52$ KM/SEC.

TABLE I

LIMESTONE (CALCIUM CARBONATE)

94-23-1---7



94-23-1--8
LIMESTONE

CALCITE	CA-C-03	96. -98.	WT. PERCENT
MAGNESIUM CARBONATE	MG-C-03	2.6- 0.4	-
WATER	H2-O	REST	-
MANGANESE CARBONATE	MN-C-03	-	-
IRON CARBONATE	FE-C-03	-	-
ORGANICS		-	-

VO = 0.370 CC/G.
VOL = 0.

THE TABLE LISTS DENSITY IN G/CC., VELOCITIES IN KM/SEC. AND PRESSURE IN KBAR.

TABLE

RHO0	US	UP	P	V/V0
2.70	12.59	5.82	1977.	0.538
-	10.22	4.41	1214.	0.570
-	10.16	4.23	1159.	0.583
-	9.38	3.93	995.	0.583
-	8.07	3.29	717.	0.591
-	6.72	1.99	361.	0.704
-	5.23	1.04	147.	0.801

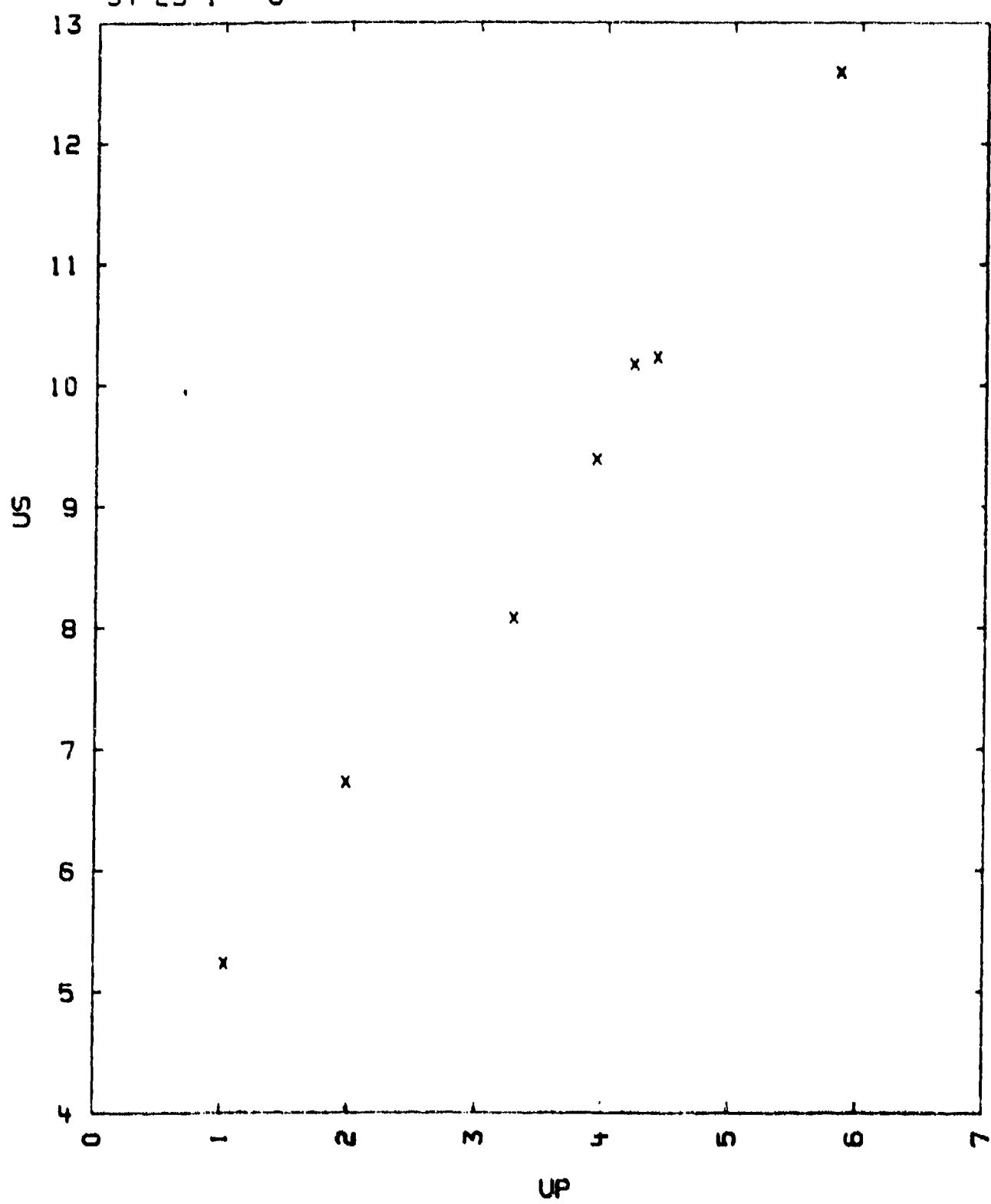
US = 3.51 + 1.53*UP KM/SEC.
S10 US = 0.26 KM/SEC.

COMMENTS:

- 1) SOURCE: ISRELL W. M., SHIPMAN F. H. AND JONES A. H.
PRIVATE COMMUNICATION
CONTRACT DA-49-146-XZ-429
GENERAL MOTORS TECHNICAL CENTER, WARREN, MICH., U.S.A.
- 2) EXPERIMENTAL TECHNIQUE: A. THE PROJECTILE (FANSTEEL OR HIGH PURITY COPPER) VELOCITIES WERE DETERMINED BY TWO TIMED X-RAY FLASHES.
- DATA REDUCTION METHOD: A
- 3) THE COMPOSITION OF THESE SAMPLES PROBABLY VARIES LESS THAN INDICATED ABOVE, SINCE THE SAMPLES WERE OBTAINED FROM UNIFORM PORTIONS OF A CORE FROM A PARTICULAR DEPTH, WHILE THE ANALYSIS REPRESENTS THE VARIATION ACROSS THE LIMESTONE STRATUM FROM WHICH THE SAMPLES WERE OBTAINED.
SEE: F. M. BYERS JR., T. BOTINELLY AND H. BARNES
TECHNICAL LETTER NTS-24 (1962)
U. S. GEOLOGICAL SURVEY, FEDERAL CENTER, DENVER 25, COLORADO, U.S.A.

TABLE I

LIMESTONE
94-23-1---8



94-93-23-1---1

DOLOMITE

DOLOMITE	CA-MO-1C-0312	96.4	WT. PERCENT
LIMESTONE	CA-C-03	1.	-
QUARTZ	SI-02	1.8	-
CLAY	(AL,FE,O,SI,H)	1.7	-
GOETITE	FE2-03-(H2-01)	.2	-

$$V_0 = 0.3539 \text{ CC/G}$$

$$V_{01} = 0.350 \text{ CC/G}$$

$$C_D = 5.81 \text{ KM/SEC.}$$

THE TABLE LISTS DENSITY IN G/CC., VELOCITIES IN KM/SEC. AND PRESSURE IN KBAR.

TABLE

- - - - - SAMPLE - - - - - STANDARD

RHO0	US	UFS	UP	P	V/V0	P
2.831	7.03	2.35	1.17	233.	0.834	231.
2.820	7.45	3.58	1.79	378.	0.760	381.
2.829	8.07	4.86	2.38	543.	0.705	553.
2.824	8.75	6.09	3.14	776.	0.641	804.
2.822	6.92	2.33	1.12	219.	0.838	218.
2.825	6.68	1.69	0.813	153.	0.878	151.
2.824	6.44	0.987	0.495	90.	0.923	85.

$$US = 5.97 + 0.876 \cdot UP \text{ KM/SEC.}$$

$$S10.US = 0.05 \text{ KM/SEC.}$$

COMMENTS:

- 1) SOURCE: HORN B. L. AND COMPILER
L.R.L. EQUATION OF STATE FILE
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIF. 94550, U.S.A
- 2) EXPERIMENTAL TECHNIQUE: B
DATA REDUCTION TECHNIQUE: B, STANDARD MATERIAL AL.
- 3) V01 IS THE SUM OF THE VOLUMES OF THE COMPONENTS, DIVIDED BY THE TOTAL WEIGHT. THE V01 VALUES OF SI-02 AND CA-C-03 WERE COMBINED WITH THAT OF PURE DOLOMITE: R. H. O. WYCKOFF, CRYSTAL STRUCTURES (INTERSCIENCE PUBLISHERS 1964) VOL. 2, 2ND ED. V01(CA-MO-C2-061)= 0.3489 CC/G FOR MONTMORILLINITE CLAY AND GOETITE SPECIFIC VOLUMES USED WERE 0.40 AND 0.229 CC/G RESP.
- 4) THESE SAMPLES WERE OBTAINED FROM DEPTHS OF 1308 TO 1341 FOOT IN A HOLE DESIGNATED U10B AT THE APPROXIMATE NEVADA CENTRAL COORDINATES N. 880,000 - E. 870,000.
- 5) AN AVERAGE ANALYSIS OVER THE DEPTH RANGE 1303 TO 1346 FEET (F. STEPHENS). THIS LABORATORY YIELDED THE FOLLOWING WT. PERCENTAGES:

H2-O	SI-02	FE-O	FE2-03	CA-O	MO-O	AL2-03	C-02	INSOL
0.09	1.22	0.04	0.13	30.63	21.07	0.48	46.48	1.57

 BETWEEN 1346 AND 1373 FEET SOMEWHAT PURER CARBONATE WAS OBTAINED

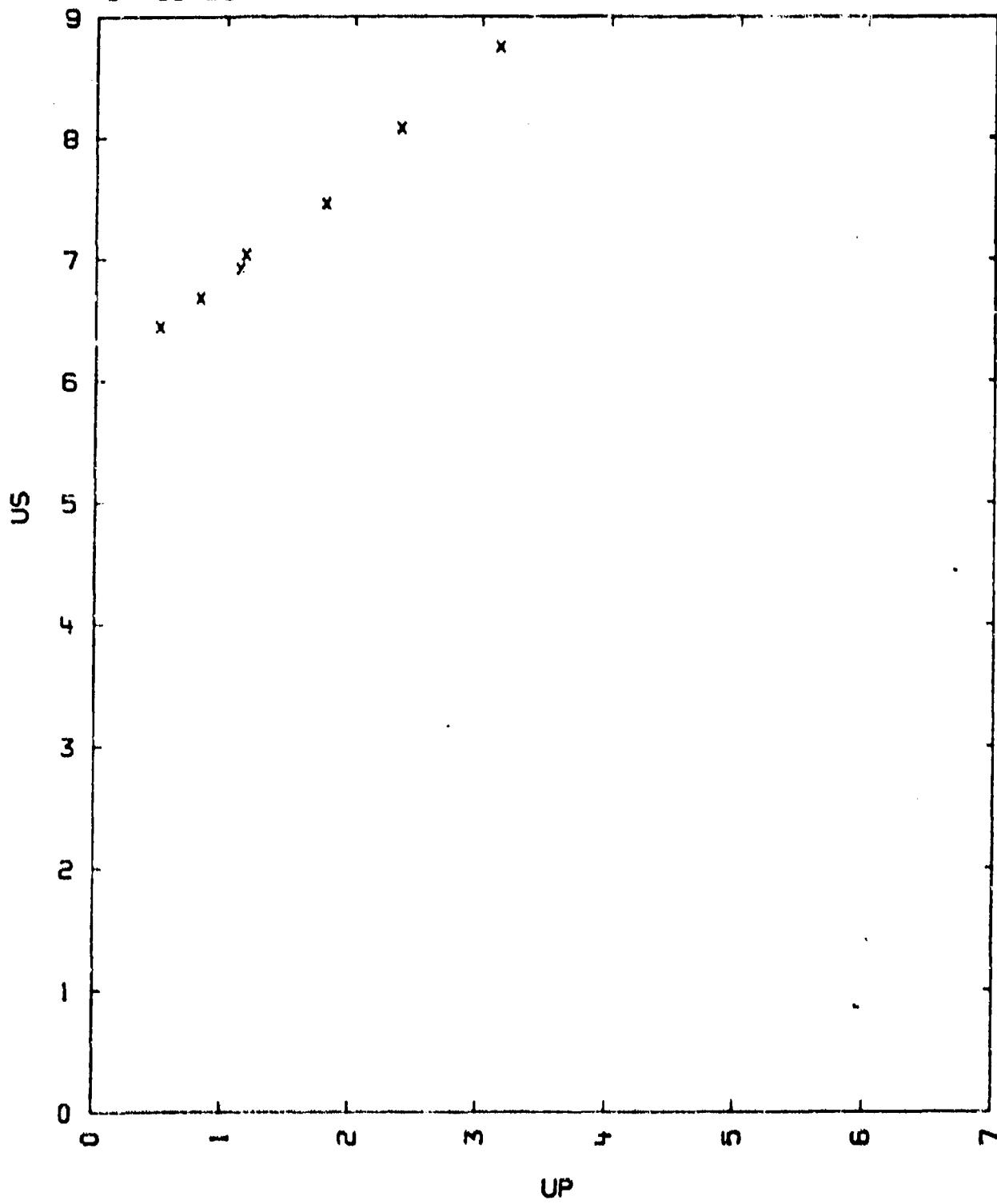
0.08	0.31	0.04	0.12	31.02	21.24	0.25	46.82	0.70
------	------	------	------	-------	-------	------	-------	------

- THE INSOL (INSOLUBLE IN BN H-Cl) FRACTION CONTAINED MOSTLY
SI WITH SOME AL, MG, FE AND Ti AS WELL AS A NUMBER OF TRACE ELEMENTS
- 6) PETROGRAPHIC ANALYSIS (J. S. KAHN OF THIS LABORATORY) SHOWED
ESSENTIALLY PURE DOLOMITE WITH SOME CLASTIC PARTICLES AND AN OCCASIO-
NAL QUARTZ VEIN. ALSO PRESENT SOME Fe₂O₃ AND CLAY. THE LATTER SHOWED
UP ESPECIALLY IN THE INSOL FRACTION AS MONTMORILLINITE TOGETHER
WITH QUARTZ AND GOETITE.
- 7) THE ABOVE COMPOSITION IS CONSISTANT WITH THIS ANALYSIS AND HAS
CONFIRMED BY AN X-RAY ANALYSIS MADE ON REPRESENTATIVE SAMPLES BY
I BORG, PRIVATE COMMUNICATION 1959

TABLE I

DOLOMITE

94-93-23-1---1



04-93-23-1---2
DOLOMITE

CA-MG-C2-08 94-97 WT. PERCENT
REST PROBABLY SIMILAR TO ENTRY 1

$V_0 = 0.355 \text{ CC}/\text{G}$.
 $V_{01} =$

THE TABLE LISTS DENSITY IN G/CC., VELOCITIES IN KM/SEC. AND PRESSURE IN KBAR.

TABLE

RHO0	US	UP	P	V/V0
2.62	11.54	5.32	1731.	0.540
-	10.02	4.14	1171.	0.587
-	9.77	3.73	1020.	0.610
-	8.44	2.65	631.	0.686

$$US = 5.39 + 1.15 \cdot UP \text{ KM/SEC}$$

$$\text{SIG.US} = 0.11 \text{ KM/SEC.}$$

COMMENTS:

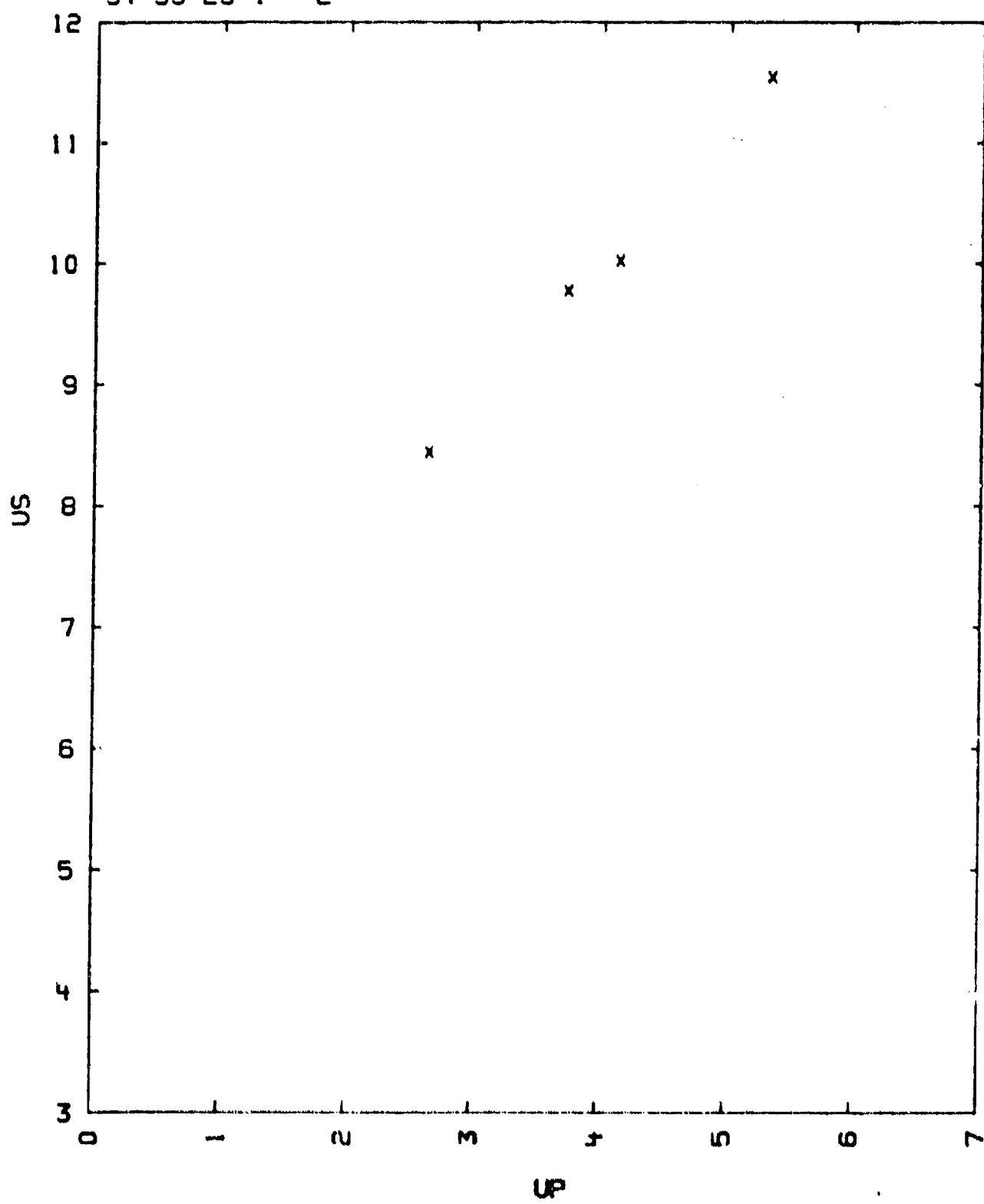
- 1) SOURCE: ISBELL H. M., SHIPMAN F. H. AND JONES A. H.
PROGRESS REPORT NO. 5, AUG. (1966)
ON CONTRACT DA-49-146-X2-429
GENERAL MOTORS TECHNICAL CENTER, WARREN, MICH., U.S.A.
- 2) EXPERIMENTAL TECHNIQUE: A. THE VELOCITY OF FANSTEEL OR HIGH PURITY COPPER PROJECTILES WERE DETERMINED BY TWO X-RAY FLASH PHOTOGRAPHS.
- DATA REDUCTION TECHNIQUE: A
- 3) THE COMPOSITION OF THIS SAMPLE WAS ESTIMATED TO BE SIMILAR TO THAT OF A MICROSCOPICALLY SIMILAR SAMPLE FROM A NEIGHBORING AREA (BANDED MOUNTAIN NEVADA TEST SITE). THIS SAMPLE WAS ALSO FROM THE SAME STRATUM THAT THE SAMPLES OF ENTRY ---1 WERE TAKEN FROM, BUT ABOUT 5 MILES AWAY AT THE APPROXIMATE NEVADA CENTRAL COORDINATES: N. 873,000 - E. 697,000, FROM DRILL HOLE D-1.12 AT 44.3-50.3 FEET DEPTH.
H. BARNES (DENVER COLO.) AND D. RAWSON (THIS LAB.), PRIVATE COMM.
H. BARNES, TECHNICAL LETTER NTS-185 (1967)
U.S. GEOLOGICAL SURVEY, FEDERAL CENTER, DENVER, COLO. 80225
- 4) X-RAY ANALYSIS OF A REPRESENTATIVE SAMPLE SHOWED THE FOLLOWING:

CALCITE	LESS THAN 5 WT PERCENT
SILICA	- - - - -
CLAY AND OTHER MINERALS	- - - - -

I BORG, PRIVATE COMMUNICATION 1969. LAWRENCE RAD. LAB., LIVERMORE

TABLE I

DOLOMITE
94-93-23-1---2



94-93-24-1 ---

DIOPSIDE

CA-MG-S12-06 (SEE NOTE 3) GRAIN SIZE ABOUT 0.5 MM.

$V_0 = 0.3046 - 0.3093 \text{ G/CC}$ $C_L = 5.83 - 8.00 \text{ KM/SEC.}$
 $V_{01} = 0.2994 - 0.3047$ -

THE TABLE LISTS DENSITY IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KBAR. STM IS THE STANDARD BASE PLATE MATERIAL, AL=ALUMINUM AND BR=BRASS D=SAMPLE THICKNESS IN MM.

TABLE

SAMPLE											STANDARD	
RHO0	US1	UP1	P1	V1/V0	VS2	UP2	UFS	P2	V2/V0	D	STM	UFS
3.283	7.31	.289	69.4	.960	6.30	0.68	1.33	149.7	.898	11	AL	1.51
3.233	7.66	.289	71.6	.962	6.86	0.96	1.88	219.7	.864	7	AL	2.11
3.279	7.92				7.69	1.26	2.51	317.7	.836	11	AL	2.82
3.272					7.92	1.43	2.77	370.6	.819	11	AL	3.18
3.233	8.52	.289	79.6	.966	8.03	1.09	3.70	494.4	.766	6	BR	3.03
3.233	10.00	.289	93.4	.971	9.22	2.09	4.21	629.9	.775	7	BR	3.45
3.233	8.90	.289	83.2	.968	8.33	2.47	4.93	664.2	.705	7	BR	3.90
3.166	6.57	.201	41.8	.969						1P	AL	1.89

US2 *

COMMENTS:

- 1) SOURCE: ANHENG T.J., ROSENBERG J.T., RUDERMAN M.H.
STANFORD RESEARCH INSTITUTE REPORT NO DASA 1868 (1966)
STANFORD RESEARCH INSTITUTE, MENLO PARK, CALIFORNIA 94030
U.S.A.
- 2) EXPERIMENTAL TECHNIQUE C1 (INCLINED MIRRORS)
DATA REDUCTION METHOD B (ELASTIC WAVES)
- 3) THE ABOVE COMPOSITION IS NOMINAL. THE VALUES OF V01 WERE CALCULATED
FROM A 96 PERCENT PURE DIOPSIDE (CRYSTAL DATA DETERMINATIVE TABLES)
J.D.H.DONNAY AND H.M.OMODIK ED. (US DEP. OF COMMERCE, NBS, 3RD ED.
1973) P. M-97 : BETA= 105.27, A=9.6776, B=8.9308, C=5.2515 ANGSTROM,
AND FROM A PRESUMED PURE SAMPLE WITH BETA=74.17 DEGREES, A=9.750
B=8.930 AND C=5.249 ANGSTROM.
- 4) UP1 WAS MEASURED ONLY IN THE FIRST AND LAST ENTRY, THE OTHER VALUES
WERE ASSUMED.
- 5) THE LAST ENTRY WAS TAKEN ON A (001) SINGLE CRYSTAL WHICH CONTAINED
VISIBLE CRACKS.

TABLE 1

DIOPSIDE

94-93-24-1---1

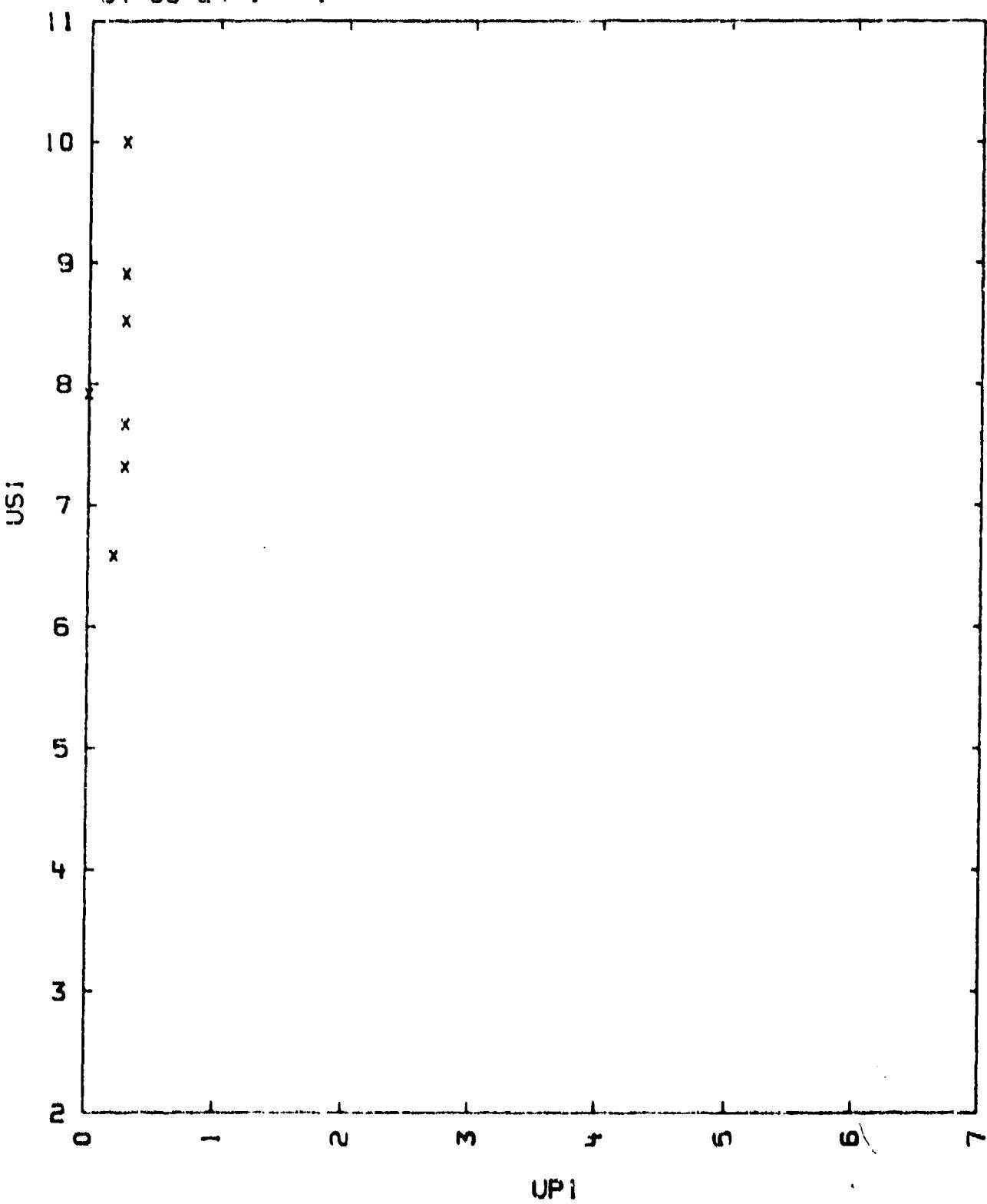
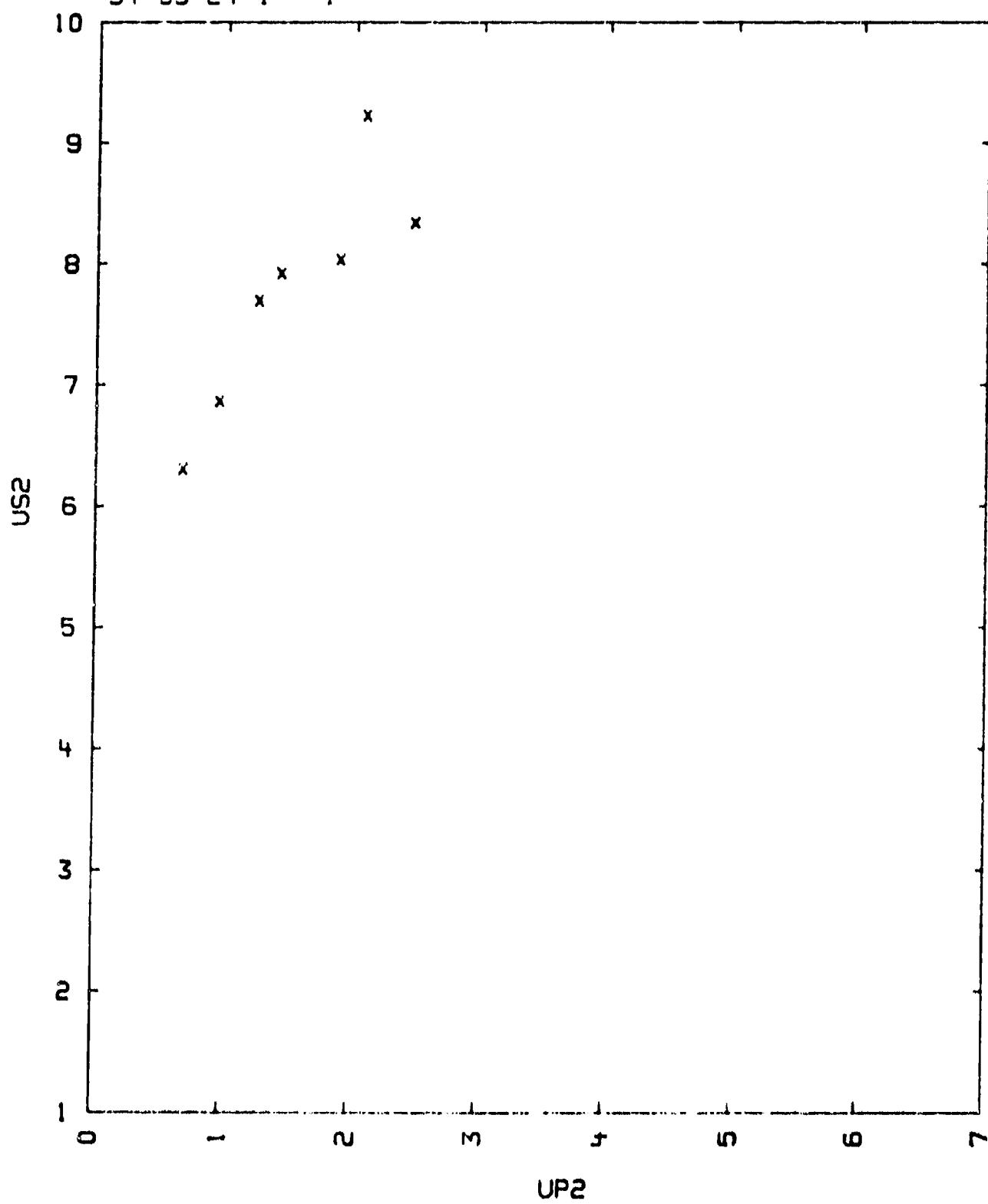


TABLE I

DIOPSIDE

94-93-24-1---1



96-57-1---1
BARIUM TITANATE

BA-11-03

$V_0 = 0.184 \text{ CC/G.}$
 $V_{01} = 0.172 \text{ CC/G.}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRE^{RE} IN KILOBARS AND DENSITY IN G/CC.

TABLE

RHOD	SAMPLE					--STANDARD-- UFS
	US	UP	P	V/V0		
5.43	5.605	1.250	380	0.777	3.040	
-	5.683	1.257	388	0.779	3.080	
-	5.342	1.200	374	0.759	3.060	
-	5.574	1.250	378	0.776	3.040	
-	5.302	1.106	318.5	0.791	2.665	
-	5.342	1.114	323	0.791	2.690	
-	5.382	1.157	338	0.785	2.800	
-	5.476	1.160	345	0.788	2.820	
-	5.453	1.172	347	0.785	2.860	
-	5.476	1.195	355	0.782	2.900	
-	5.246	1.215	344	0.768	2.875	
-	5.291	1.165	334	0.780	2.780	
-	4.935	1.025	275	0.792	2.452	
-	4.892	1.035	275	0.788	2.425	
-	4.199	1.047	284	0.790	2.475	
-	4.199	1.055	287	0.789	2.490	
-	4.955	1.037	273	0.790	2.420	
-	4.849	1.042	275	0.785	2.430	
-	5.268	1.010	281	0.808	2.425	
-	5.117	1.005	279	0.803	2.405	
-	5.285	1.042	300	0.803	2.530	
-	5.347	1.040	302	0.805	2.535	
-	5.035	1.110	303	0.779	2.615	
-	5.039	1.117	306	0.778	2.635	
-	4.595	0.860	219	0.817	2.015	
-	4.621	0.860	216	0.814	2.005	
-	4.672	0.865	220	0.815	2.027	
-	4.721	0.867	223	0.816	2.040	
-	4.708	0.775	199	0.839	1.845	
-	4.633	0.787	199	0.830	1.695	
-	4.212	0.810	185	0.807	1.815	
-	4.212	0.817	186.5	0.806	1.830	
-	3.876	0.605	128	0.844	1.340	
-	3.843	0.610	127	0.841	1.345	
-	4.078	0.605	134	0.852	1.375	
-	4.098	0.590	132	0.856	1.350	
-	3.977	0.630	137.5	0.841	1.415	
-	4.012	0.620	136	0.845	1.400	
-	3.623	0.655	128.5	0.819	1.392	
-	3.623	0.615	127	0.821	1.377	

006/14/77

BARIUM TITANATE

RHO0	US	UP	P	V/V0	UFS
-	3.706	0.533	107	0.856	1.167
-	3.706	0.537	108	0.855	1.173
-	3.725	0.560	112	0.849	1.220
-	3.663	0.570	113	0.844	1.232

$$US = 2.32 + 2.60 UP \text{ KM/SEC.} \quad S10.US = 0.19 \text{ KM/SEC.}$$

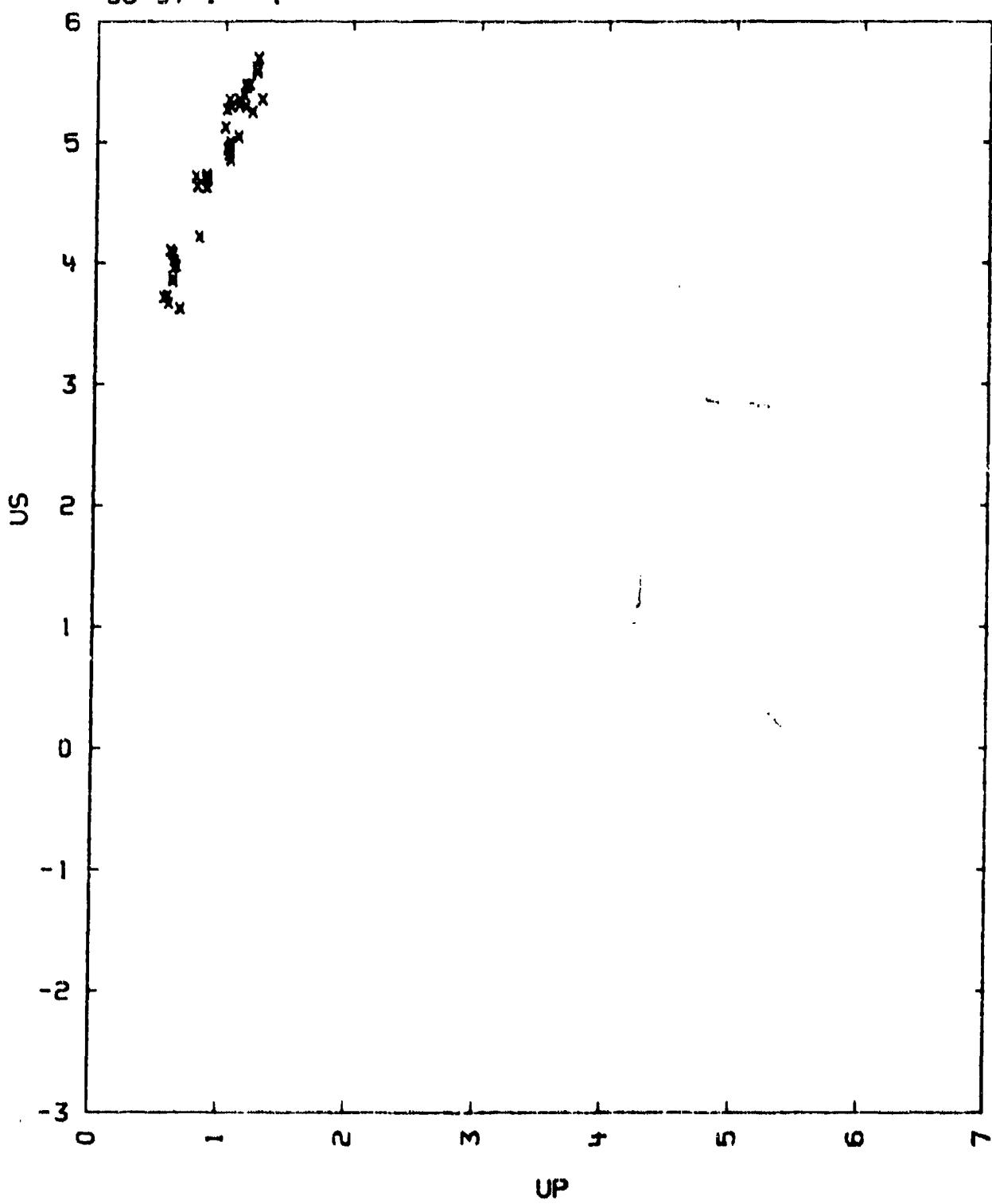
COMMENTS:

- 1) SOURCE: BERGER J. AND FAUQIONON C.
PRIVATE COMMUNICATION (1964), B.P. NO. 7, SEVRAN, FRANCE
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION TECHNIQUE B
STANDARD MATERIAL ALUMINUM ALMg ALLOY
- 3) V01 WAS OBTAINED FROM CRYSTAL DATA DETERMINATIVE TABLES (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION, POLYCRYSTAL BOOK SERVICE, BROOKLYN, N.Y., 1963) 2ND ED.
- 4) SAMPLE DIMENSIONS WERE: 2.0 CM DIAMETER
0.5 CM THICKNESS

U06/14/77

TABLE I

BARIUM TITANATE
96-57-1---1



96-57-1---2

BARIUMTITANATE-CALCIUMTITANATE CERAMIC

SILICA	SI-02	0.30	WEIGHT PERCENT
ALUMINUM OXIDE	AL2-03	0.29	-
STRONTIUM OXIDE	SR-0	0.22	-
SODIUM OXIDE	NA2-0	0.17	-
PHOSPHORUSPENTOXIDE	P2-05	0.11	-
CALCIUMTITANATE	CA-TI-03	5.	-
BARIUMTITANATE	BA-TI-03	REMAINDER	-

$$V_0 = 0.180 - 0.181 \text{ CC}/\text{O} \quad C_L = 5.48$$

$$V_{01} = 0.1705 \text{ CC}/\text{O}$$

TABLE I LISTS ELASTIC WAVE MEASUREMENTS FOR SEVERAL EXPERIMENTS. TABLES II AND III LIST A THREE-WAVE SYSTEM OBSERVED IN ONE EXPERIMENT (SEE COMMENTS). TABLES IV AND V LIST DOUBLE WAVES OBSERVED IN A SERIES OF MORE CONVENTIONAL EXPERIMENTS. TABLE VI LISTS ELASTIC WAVE POINTS FOR A SAMPLE AT 130 DEG. C. IN THE CUBIC PHASE. EXPNO = SOURCE EXPERIMENT NUMBER. DENSITIES ARE IN G/CC, VELOCITY IN KM/SEC, PRESSURE IN KBARS. D IS SAMPLE THICKNESS IN MM. LUC = LUCITE, 4340 = STEEL ALLOY.

TABLE I
PRESSURE GRADIENT EXPERIMENTS

RHO0	T0	US	UP	P	V/V0	EXPNO
5.54	20	6.29	0.0855	29.8	0.9864	7396
-	17	5.58	0.0324	10.0	0.9942	7540
-	-	5.49	0.0301	9.17	0.9945	-
-	-	5.37	0.0261	7.78	0.9951	-
-	-	5.31	0.0255	7.51	0.9952	-
-	-	5.31	0.0243	7.16	0.9954	-
-	-	5.31	0.0237	6.98	0.9955	-
-	20	6.28	0.0885	30.9	0.9859	7592
-	-	6.27	0.0855	29.7	0.9864	-
-	-	6.27	0.0870	30.3	0.9861	-
-	-	6.23	0.0806	27.9	0.9871	-
-	-	6.15	0.0707	24.1	0.9885	-
-	-	6.09	0.0657	21.5	0.9895	-
-	-	6.07	0.0628	21.2	0.9897	-
-	-	6.05	0.0623	20.9	0.9897	-
-	-	6.04	0.0608	20.4	0.9899	-
-	-	6.03	0.0578	19.3	0.9904	-
-	-	6.00	0.0564	18.8	0.9906	-
-	-	5.99	0.0543	18.0	0.9909	-
-	21	6.19	0.0739	25.3	0.9881	7612
-	-	6.18	0.0754	25.2	0.9881	-
-	-	6.11	0.0639	21.6	0.9895	-
5.54	21	6.06	0.0605	20.4	0.9900	7612
-	-	5.95	0.0488	16.1	0.9918	-
-	-	5.90	0.0478	15.6	0.9919	-
-	-	5.86	0.0474	15.4	0.9919	-
-	-	5.82	0.0420	13.5	0.9928	-
-	-	5.71	0.0410	13.0	0.9928	-
-	-	5.67	0.0379	12.0	0.9934	-

BARIUMTITANATE-CALCIUMTITANATE CERAMIC

RHO0	T0	US	UP	P	V/V0	EXPNO
-	-	5.59	0.0326	10.1	0.9942	-
-	-	5.52	0.0295	9.05	0.9946	-

US -

TABLE II
TRIPLE-WAVE PRESSURE GRADIENT EXPERIMENT (VELOCITIES)

NO	RHO0	US1	UP1	US2	UP2	US3	UP3
1	5.54	6.27	0.0887	5.3	0.129	4.57	0.395
2	-	-	0.0882	-	0.127	4.54	0.368
3	-	-	0.0894	-	0.137	4.40	0.300
4	-	-	0.0854	-	0.135	4.33	0.327
5	-	-	0.0876	-	0.126	-	-
6	-	-	0.0854	-	0.121	4.20	0.280
7	-	-	0.0870	-	0.128	-	-
8	-	-	0.0876	-	0.118	-	-

US -

TABLE III
TRIPLE-WAVE PRESSURE GRADIENT EXPERIMENTS (P - V)

NO	RHO0	P1	V1/V0	P2	V2/V0	P3	V3/V0
1	5.54	30.8	0.9859	43	0.9782	99	0.929
2	-	30.6	0.9859	44	-	102	0.926
3	-	31.1	0.9857	45	-	83	0.957
4	-	29.6	0.9864	45	-	90	0.932
5	-	30.4	0.9860	41	-	-	-
6	-	29.6	0.9864	41	-	76	0.938
7	-	30.2	0.9861	42	-	-	-
8	-	30.4	0.9860	39	-	-	-

TABLE IV
PLANE WAVE EXPERIMENTS

RHO0	US1	UP1	US2	UP2	US3/2	D	EXPND
5.54			4.78	0.60	0.53	6	7384
-	6.15	0.108	4.89	0.56	0.48	6	7400
-	6.15	0.107	5.18	0.6	0.56	12.5	7446
-	6.32	0.11	5.82	0.98	0.96	6	7447
-	6.39	0.108	4.59	0.59	0.46	6	7591
-	5.25	0.0175				6	8445

BARIUMTITANATE-CALCIUMTITANATE CERAMIC

RHO0	US1	UPI	US2	UP2	UPS/2	D	EXPNO
-	5.90	0.0492				5	8748
-	6.15	0.098					8882
-	6.08	0.065				5.4	8883
-	5.24	0.016				6	8884

US1 = $4.70 + 31.37 \cdot U_P + 15 \cdot 2 \cdot U_P \cdot 2 \text{ KM/SEC}$ (FIRST WAVE)
 $SIG US = 0.037 \text{ KM/SEC FOR UP FROM } 0.016 \text{ TO } 0.11 \text{ KM/SEC}$

US2 = $3.68 + 2.16 \cdot U_P \text{ KM/SEC}$ (LAST WAVE)
 $SIG US = 0.13 \text{ KM/SEC FOR UP FROM } 0.3 \text{ TO } 1.0 \text{ KM/SEC}$

TABLE V
PLANE WAVE EXPERIMENTS

-----SAMPLE----- ---STANDARD---

RHO0	P1	V1/V0	P2	V2/V0	P	EXPNO	MAT
5.54			169	0.875	133	7384	AL
-	37	0.982	149	0.901	125	7400	AL
-	37	0.992	167	0.896	133	7446	AL
-	40	0.982	310	0.8363	245	7447	AL
-	38	0.983	127	0.9055	67	7591	LUCITE
-	5.1	0.9967			7.9	8445	IRON
-	16	0.9917			18	8748	STEEL
-	34	0.9840			32	8882	LUCITE
-	22	0.9891			23	8883	STEEL
-	4.7	0.9969			2.5	8884	LUCITE

TABLE VI
130-DEG. PRESSURE GRADIENT EXPERIMENT

RHO0	US1	UPI	P1	V/V0
5.54	6.30	0.0910	32.2	0.9058
-	6.38	0.0780	27.6	0.9870
-	6.38	0.0715	25.3	0.9888
-	6.37	0.0740	26.2	0.9884
-	6.36	0.0815	28.8	0.9872
-	6.34	0.0715	25.2	0.9887
-	6.33	0.0505	17.7	0.9920
-	6.32	0.0585	20.5	0.9908
-	6.32	0.0595	20.9	0.9908
-	6.31	0.0570	20.0	0.9910
-	6.30	0.0510	17.8	0.9913
-	6.29	0.0495	17.3	0.9921
-	6.28	0.0443	15.5	0.9930
-	6.28	0.0416	14.5	0.9934
-	6.28	0.0440	15.3	0.9930

BARIUMTITANATE-CALCIUMTITANATE CERAMIC

RHO0	US1	UPI	P1	V/V0
------	-----	-----	----	------

-	6.28	0.0485	16.9	0.9923
-	6.28	0.0448	15.6	0.9929
-	6.28	0.0421	14.7	0.9933
-	6.28	0.0384	13.4	0.9939
-	6.28	0.0375	13.1	0.9940

US *

COMMENTS:

1) SOURCE: DORAN, D. O.

J. APPL. PHYS., VOL. 39, P. 40, (1968)

2) EXPERIMENTAL TECHNIQUE C2 (TABLES IV AND VI) AND D (THE REST)

TABLES IV AND V DATA WERE OBTAINED WITH A PLANE WAVE EXPLOSIVE SYSTEM, WHILE THE OTHER DATA WERE OBTAINED WITH A CONFIGURATION THAT IMPRESSED A PRESSURE GRADIENT ACROSS THE FACE OF THE SAMPLE.

DATA REDUCTION METHOD: D WITH 2UP= UPS IN MOST CASES.

D AND B AVERAGED TO PARTIALLY CORRECT FOR ATTENUATION IN SOME TABLES IV AND V ENTRIES.

3) VO1 WAS OBTAINED FROM THE CRYSTAL DENSITIES OF BA-TI AND CA-TI-O3 ASSUMING VOLUME ADDITIVITY: WYCKOFF, CRYSTAL STRUCTURES, VOL II (JOHN WILEY AND SONS, N. Y. 1963) 2ND ED.

FOR BA-TI-O3 20 DEG C MONOCLINIC A = 3.9947 ANGSTROM

C = 4.0330 -

- - 201 - - CUBIC A = 4.0118 -

- - 1372 - - A = 4.0783 -

FOR CA-TI-O3 26 - - A = 3.84 -

4) IN EXPERIMENTS NO 7400 AND 7446 THE REFLECTION OF THE ELASTIC WAVE IS EXPLICITLY TAKEN INTO ACCOUNT IN CALCULATING US2.

5) THE TABULATION IN TABLES II AND III IS A SIMPLIFICATION OF A MORE COMPLEX WAVE SYSTEM: WAVE 1 IS A SIMPLE STEP, BUT WAVE 2 IS A GRADIENT WITH A GRADUAL PRESSURE INCREASE OF ABOUT 10-15 KBAARS, WHILE WAVE 3 APPEARS TO BE SPLIT INTO TWO WAVES WITH NEARLY THE SAME VELOCITY.

6) THE CURIE TEMPERATURE IS 115 DEG. C.

7) DENSITY UNIFORMITY OF THE SAMPLES HAS 0.06 G/CC MAXIMUM.

8) A FIT GIVEN BY REYNOLDS AND SEA, J. APPL. PHYS., VOL. 33, P 2234 (1962), FOR PURE BA-TI-O3 WITH VO = 0.175 IS:

US1 = 4.34 + 21.2*UPI KM/SEC, FOR UPI FROM 0.0 TO 0.674+OR- 0.002

US2 = 3.51 + 1.69*UP2 - - UP2 - 0.074+OR- 0.002 TO 1.0

SIGNS = 1.0 PERCENT.

9) THE FREE SURFACE EXPERIMENT NUMBERS 7447, 7591, AND 8882 WERE MADE ON SAMPLES HALF AS THICK AS THOSE ON WHICH THE SHOCK VELOCITIES WERE MEASURED, NAMELY 3MM. THE THICKNESS INDICATED FOR EXPERIMENT 8882 IS THE MAXIMUM THICKNESS OF A 10-DEG. WEDGE.

TABLE I
BARIUMTITANATE-CALCIUMTITANATE CERAMIC
96-57-1---2

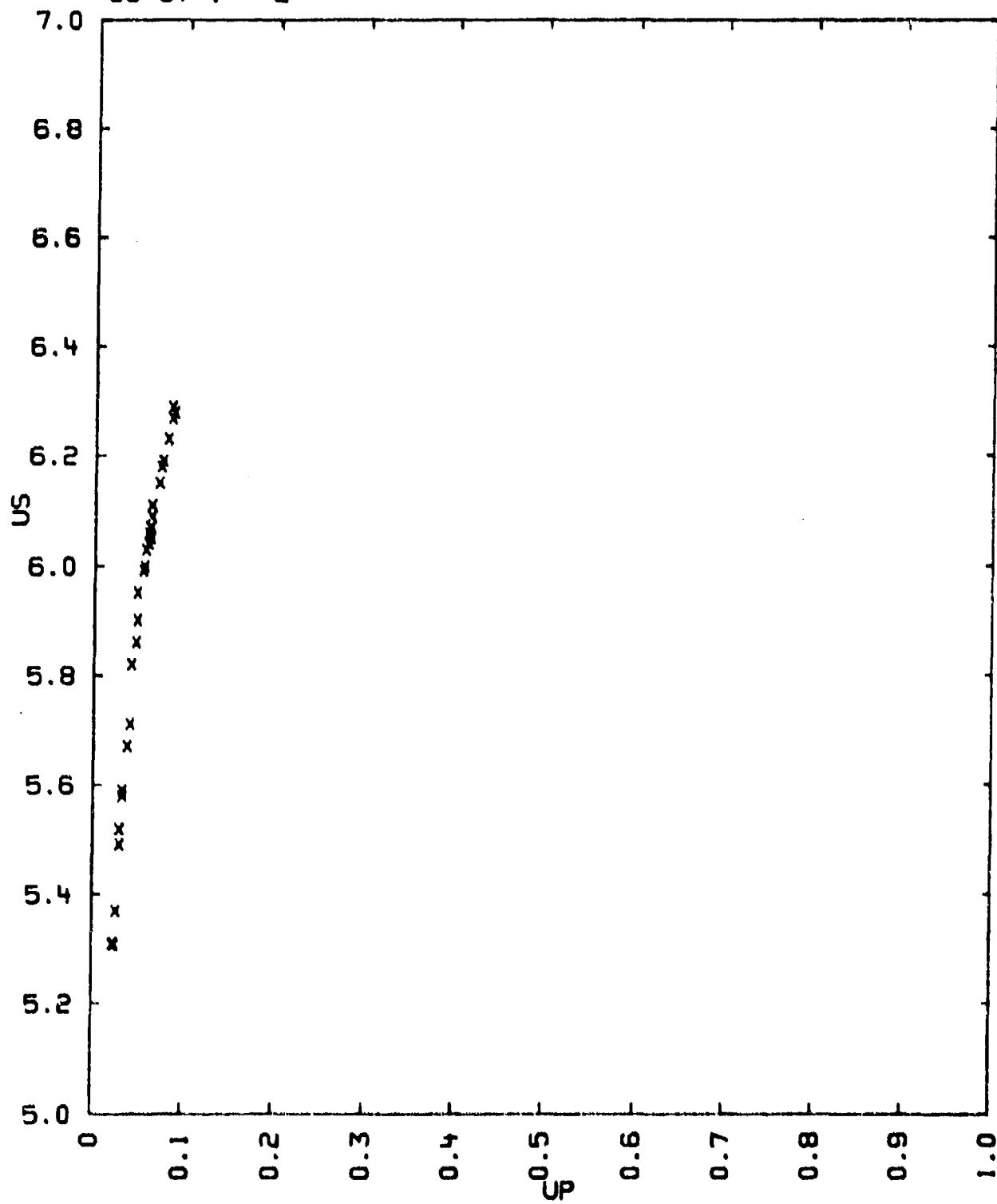


TABLE II
BARIUMTITANATE-CALCIUMTITANATE CERAMIC
96-57-1---2

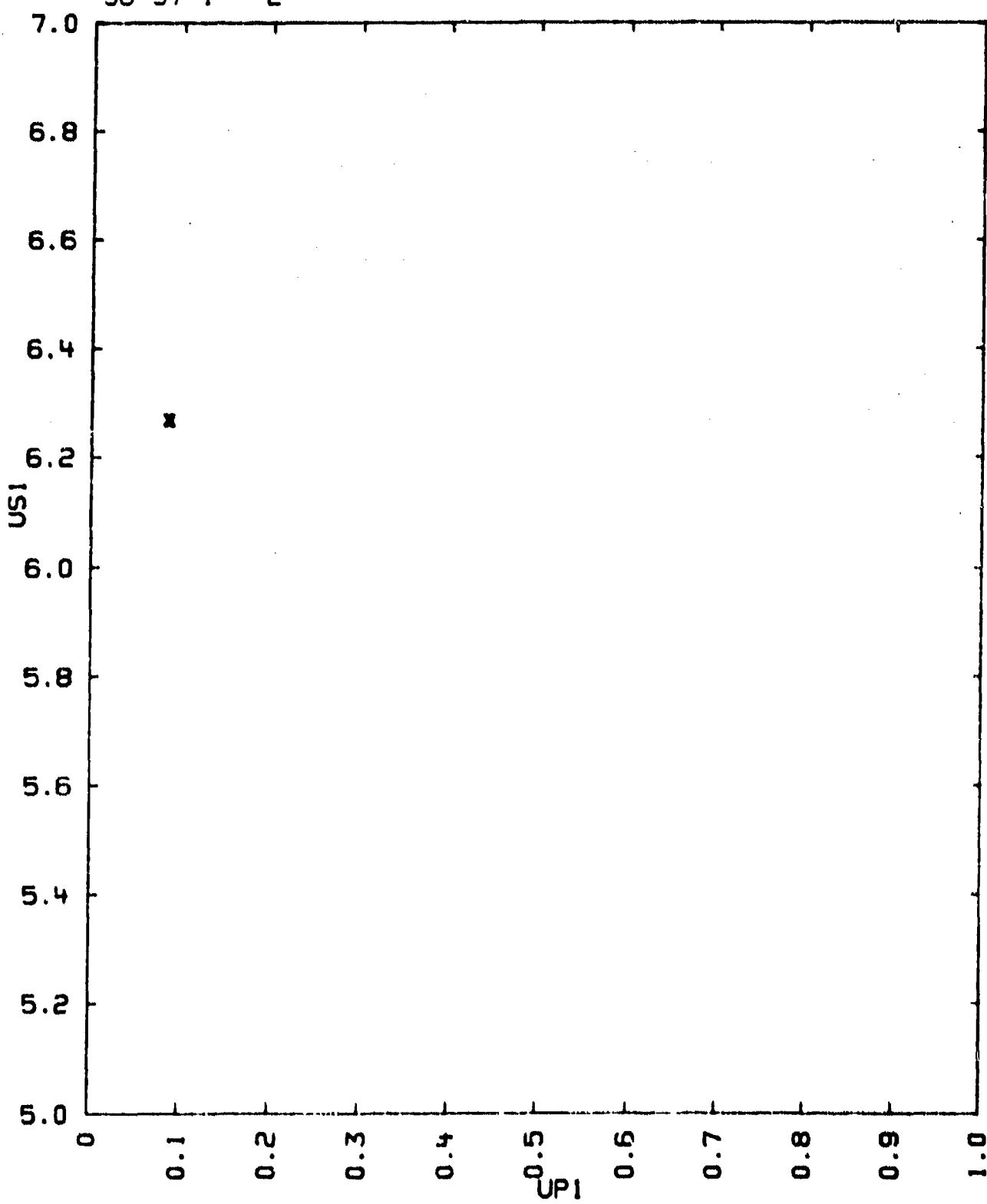


TABLE II
BARIUMTITANATE-CALCIUMTITANATE CERAMIC
96-57-1---2

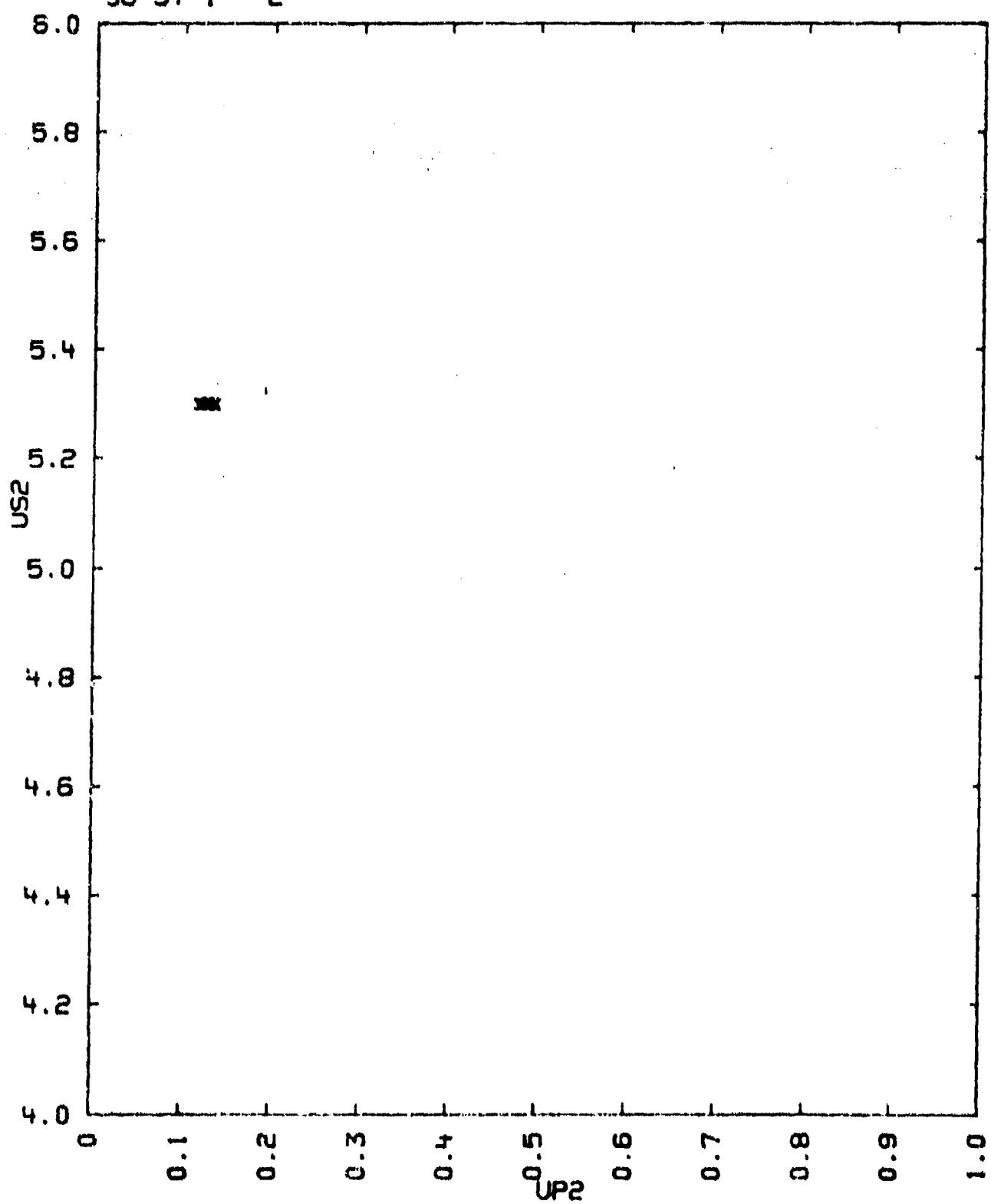


TABLE II
BARIUMTITANATE-CALCIUMTITANATE CERAMIC
96-57-1---2

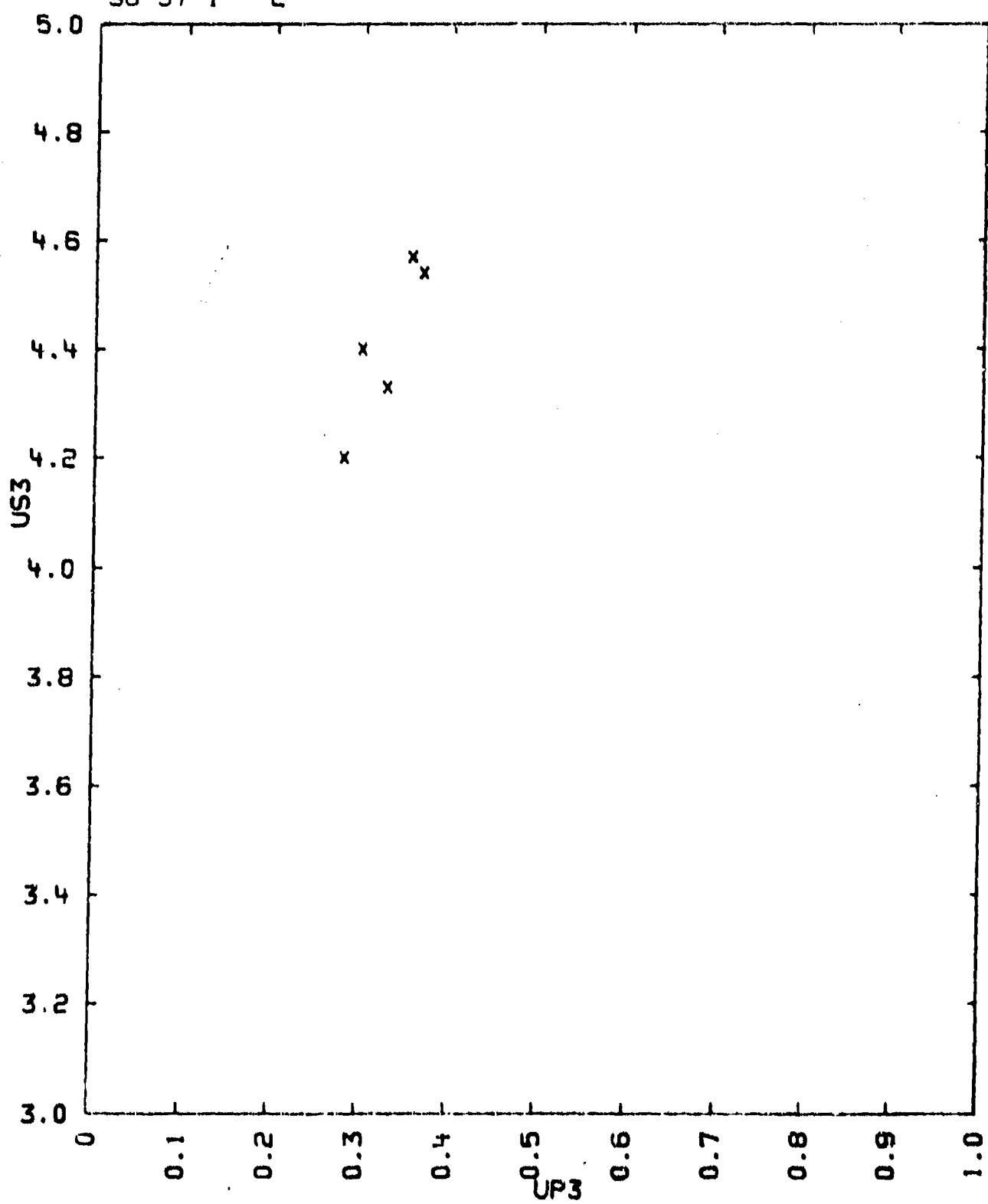


TABLE IV
BARIUMTITANATE-CALCIUMTITANATE CERAMIC
96-57-1---2

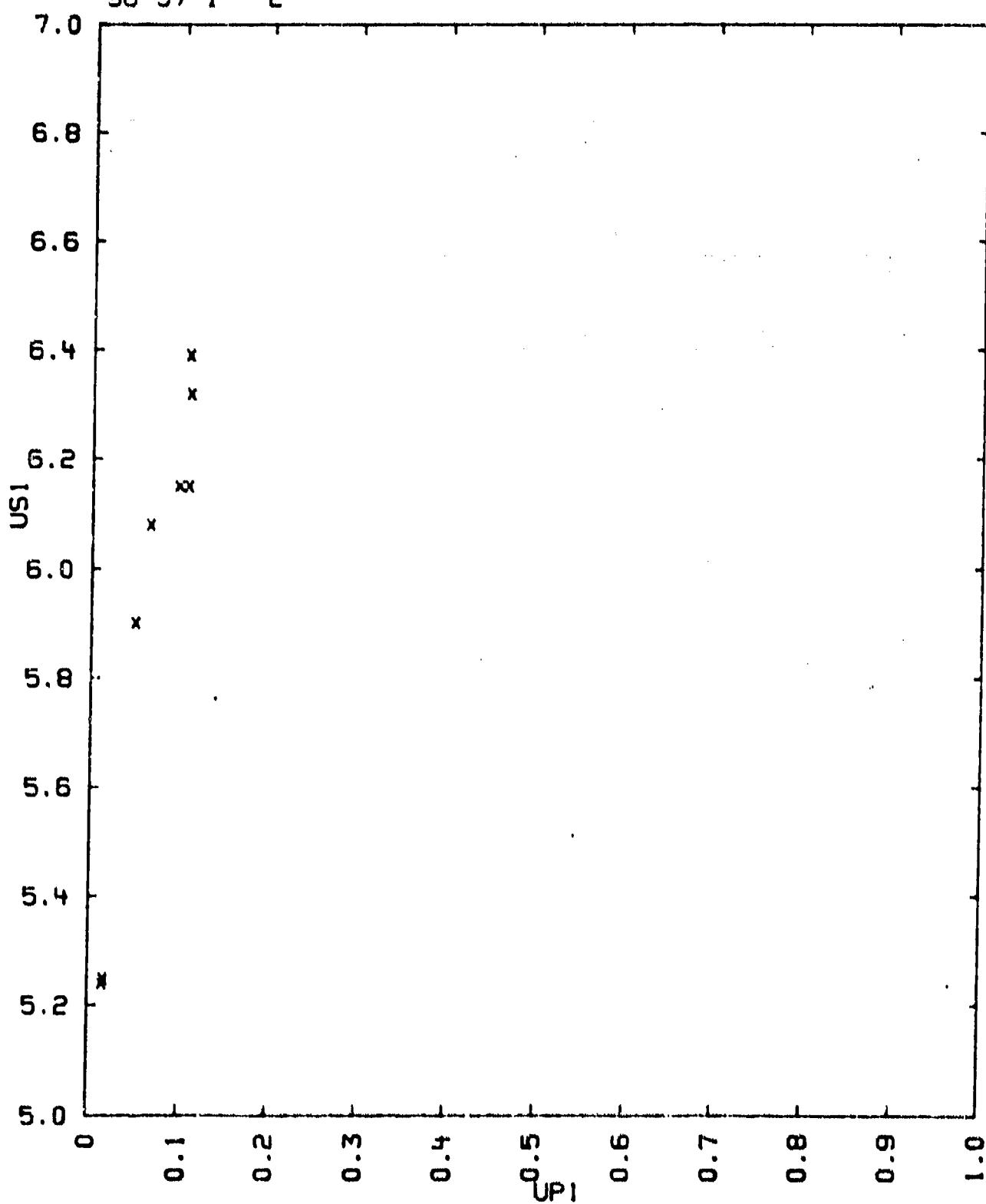


TABLE IV
BARIUMTITANATE-CALCIUMTITANATE CERAMIC
96-57-1---2

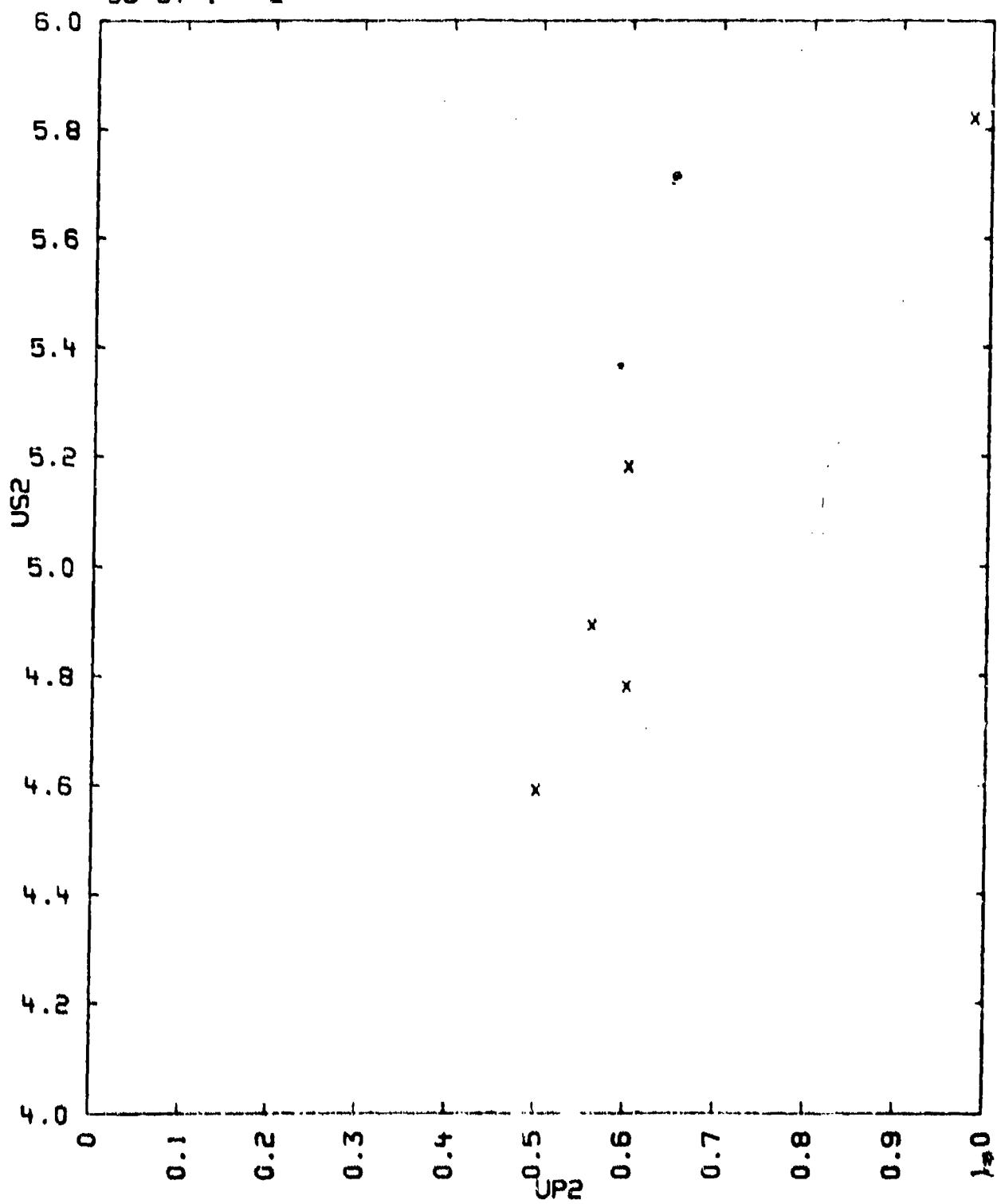
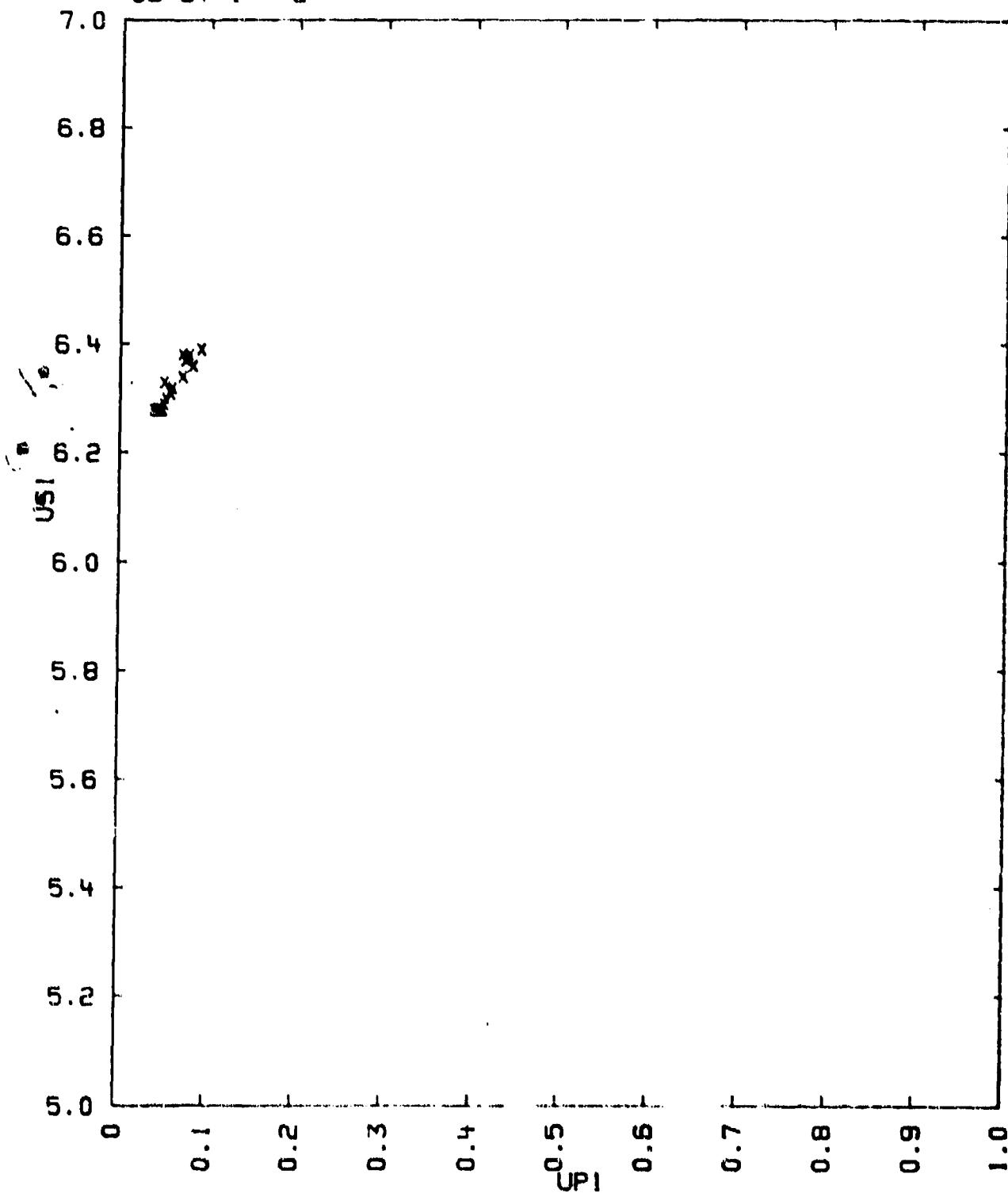


TABLE VI
BARIUMTITANATE-CALCIUMTITANATE CERAMIC
96-57-1---2



98-2--1
LITHIUM HYDRIDE

L-H :
LITHIUM 7 ISOTOPE 92.5 ATOM PERCENT
 6 7.5

$V_0 = 1.335 \text{ CC/G}$ $C_L = 10.02 \text{ KM/SEC}$ $C_0 = 6.22 \text{ KM/SEC.}$
 $V_{01} = 1.294 \text{ CC/G}$ $C_S = 6.80 \text{ KM/SEC}$

THE TABLE LISTS DENSITY IN G/CC., VELOCITIES IN KM/SEC AND PRESSURES IN KBAR. A .1, INDICATES THE ELASTIC- AND A .2, THE PLASTIC WAVE. MET = EXPERIMENTAL METHOD.

TABLE

RHO0	US1	UP1	P1	V1/V0	US2	UP2	P2	V2/V0	MET
0.749	9.51	0.007	0.47	0.9993	5.89	0.82	35.3	0.86	F
0.749	9.68	0.005	0.39	0.9993	7.62	1.68	96.3	0.78	-
0.749	9.40	0.005	0.37	0.9993	8.40	2.21	137.4	0.74	-
0.749	9.43				8.71	2.50	163.2	0.71	-
0.749	9.05	0.01	0.66	0.9989	5.89	0.87	38.4	0.85	A
0.749	8.93	0.008	0.51	0.9991	6.53	1.14	55.4	0.83	-

$$US2 = 3.553 + 3.113 \cdot UP - 0.419 \cdot UP^{+2} \text{ KM/SEC}$$

COMMENTS:

- 1) SOURCE: MAY, R. P., BIESECKER, R. G. AND KING, T. N.
SANDIA CORPORATION REPORT, SC-TM-68-113, APRIL 1968.
SANDIA CORPORATION, ALBUQUERQUE, NEW MEXICO, U.S.A.
- 2) EXPERIMENTAL TECHNIQUE: F AND A
DATA REDUCTION METHOD: B+ AND B RESPECTIVELY
- 3) THE SAMPLES WERE OBTAINED FROM UNION CARBIDE NUCLEAR DIV.
- 4) CL, CS AND CO WERE DETERMINED BY T. R. GUESS, SANDIA LABORATORY,
ALBUQUERQUE, NEW MEXICO, U.S.A.
- 5) PRELIMINARY DATA, WORK IN PROGRESS.

008/14/77

TABLE I

LITHIUM HYDRIDE
98-2---1

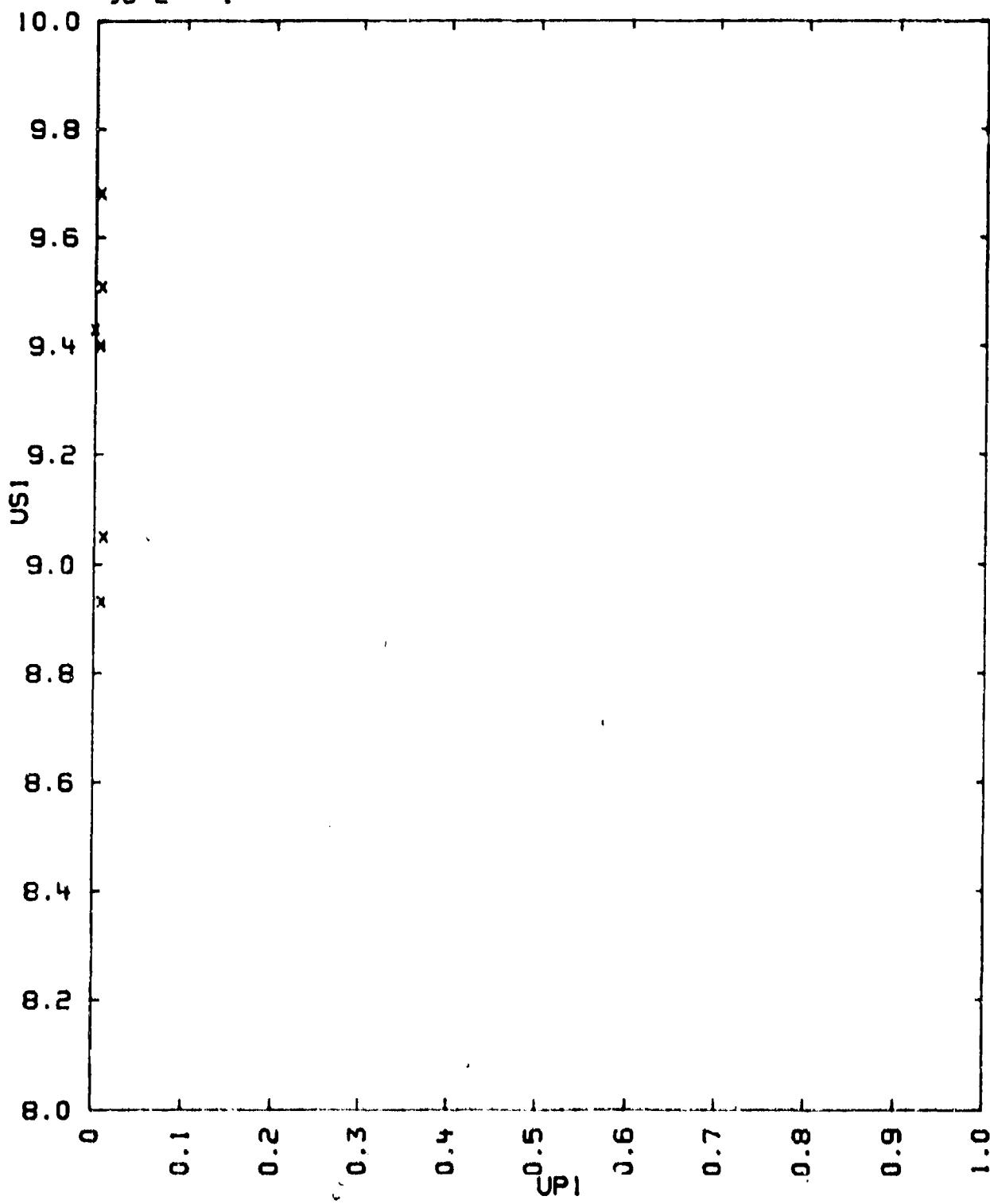
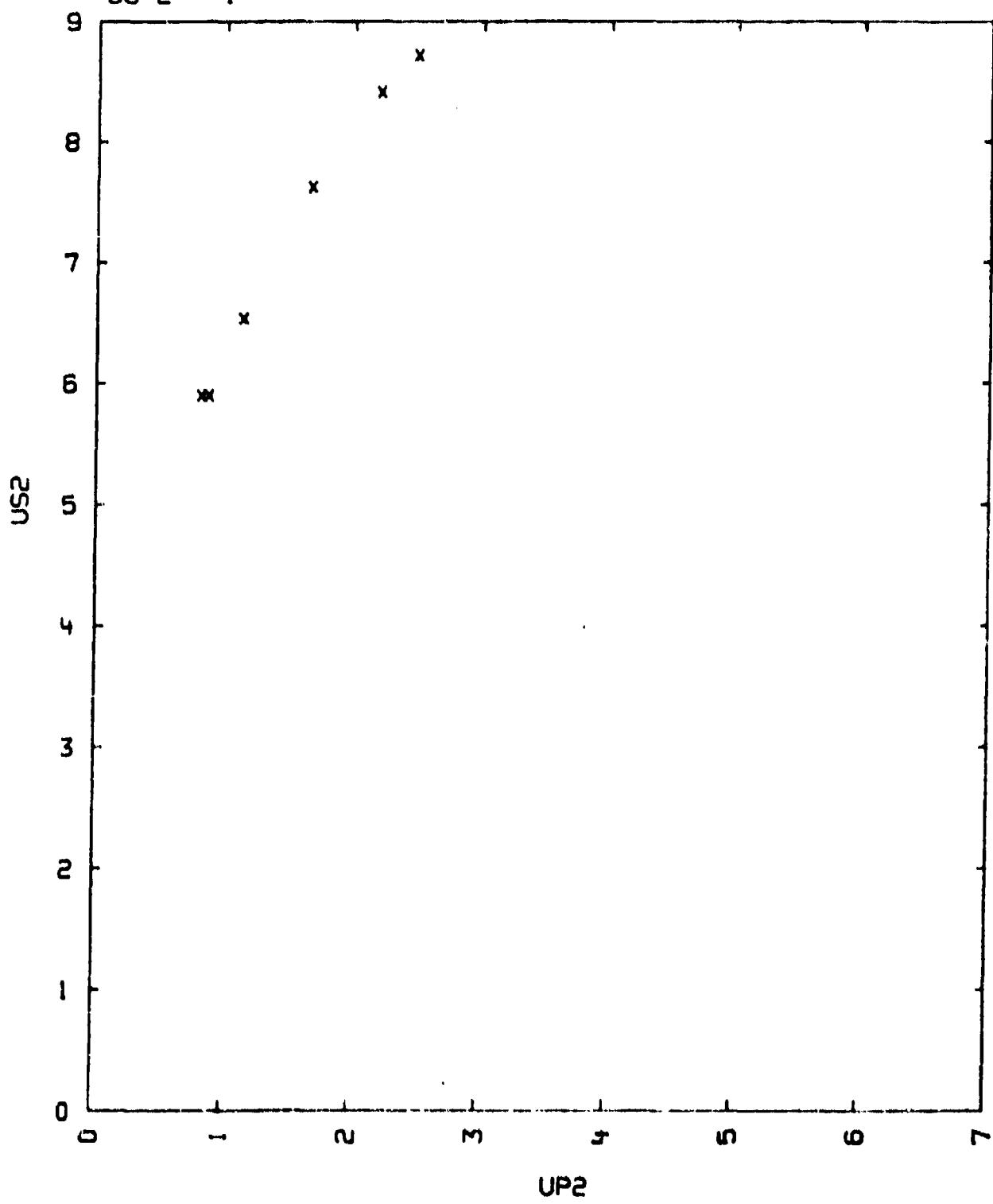


TABLE I

LITHIUM HYDRIDE
98-2---1



98-9--1
LITHIUM FLUORIDE

LI-F

$$V_0 = 0.3773 \text{ CC}/\text{O}$$

$$V_{01} = 0.3788 \text{ CC}/\text{O}$$

$$C_B = 4.97 \text{ KM}/\text{SEC}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS. SH DESIGNATES SAMPLE HOLDER.

TABLE

RHO0	US	UP	P	V/V0	SH	UP(SH)
2.65	5.74	0.52	79.0	0.9081	CU	0.37
-	7.14	1.53	289.5	0.8019	AL	1.50
-	7.52	1.73	345.0	0.7692	AL	1.71
-	8.97	2.87	683.0	0.6803	AL	2.82
-	10.43	3.79	1036.0	0.6394	FE	2.80

US = $4.98 + 1.434 UP$ KM/SEC FOR UP BETWEEN 0 AND 4 KM/SEC
 $SIG US = 0.095$

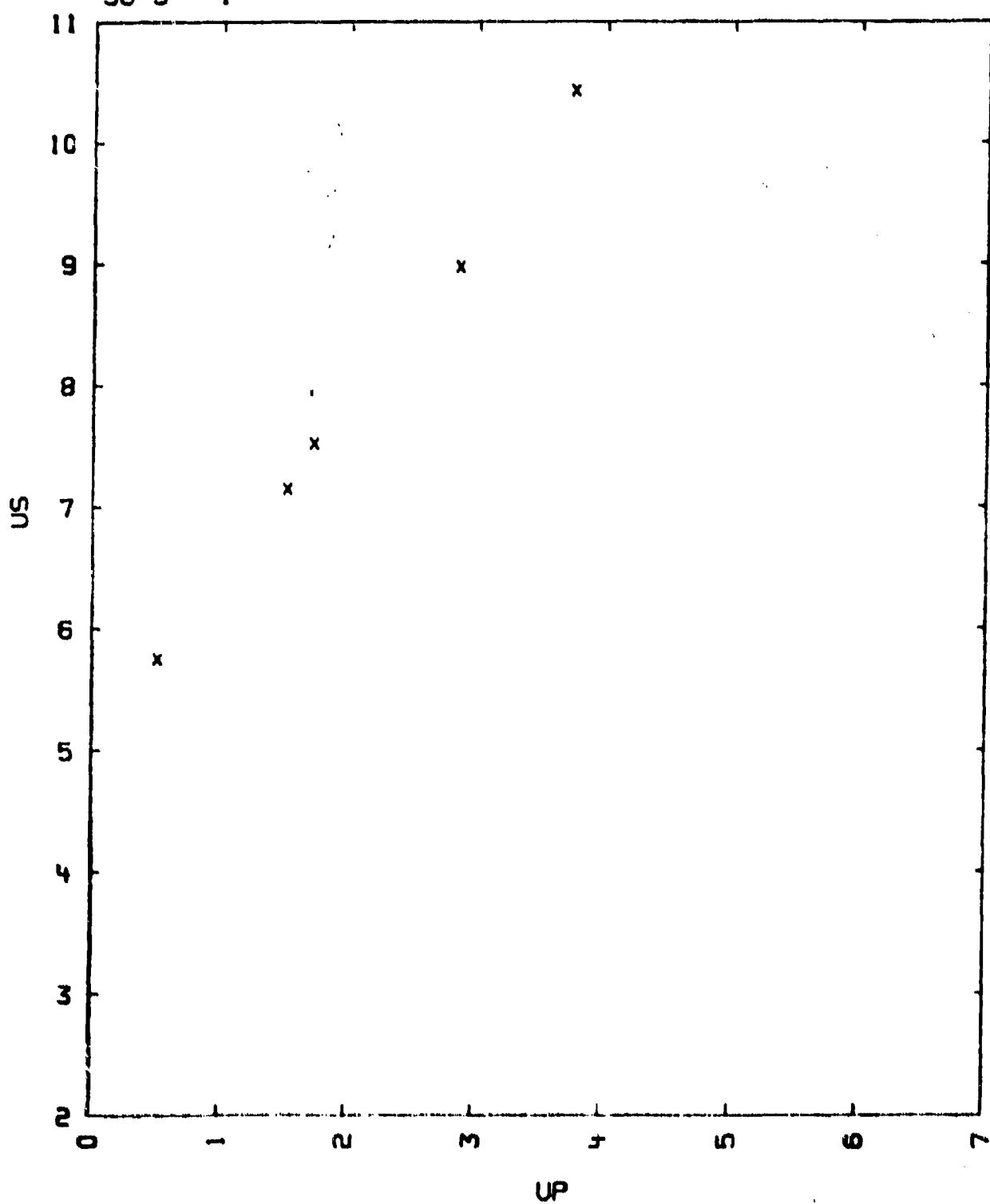
COMMENTS:

- 1) SOURCE: AL'TSHULER, L.V., PAVLOVSKII, M.M., KULESHOVA, L.V., AND SIMAKOV, O.V.
SOVIET PHYS.-SOLID STATE, VOL. 5, P. 203 (1963)
- 2) EXPERIMENTAL TECHNIQUE A
DATA REDUCTION TECHNIQUE B.
- 3) THE SAMPLES WERE POSITIONED ON PLATES OF CU AL AND FE AS INDICATED IN TAB. COLUMN 6.
THE HUGONIOTS OF FE CU AND AL WERE OBTAINED FROM
AL'TSHULER, L.V., KORMER, S.B., BAKANOVA, A.A. AND TRUNIN, R.F
JETP VOL 11, P.573 (1960)
- 4) THE AL AND CU ADIABAT WERE OBTAINED BY REFLECTING THE HUGONIOT IN THE
P VS UP PLANE. CORRECTIONS WERE MADE FOR FE.
- 5) OTHER CONSTANTS LISTED ARE: DEBYE TEMPERATURE 580 DEG. K
HEAT CAPACITY (CV) 1.482 J/G/DEG.
CATION TO ANION DISTANCE 2.009 KX
EXPANSION COEFFICIENT 0.000103 PER DEG
- 6) THE VALUE OF V01 WAS OBTAINED FROM A LATTICE CONSTANT OF 4.0262 A
A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE 1963) 2ND EDITION.

TABLE I

LITHIUM FLUORIDE

98-9---1



98-9---2
 LITHIUM FLUORIDE
 LI-F SINGLE CRYSTAL

$V_0 = 0.383 \text{ CC}/\text{O}$
 $V_{01} = 0.3789 \text{ CC}/\text{O}$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICROSEC., AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UFS	UP	P	V/V0	PRESSURE IN AL BASE PL.
2.614	6.40	1.87	0.93	155	0.855	160
2.618	6.61	2.18	1.07	185	0.838	194
2.600	7.28	3.04	1.49	282	0.796	293
2.615	7.47	3.42	1.58	328	0.775	342

$US = 5.070 + 1.450 UP \text{ MM/MICROSEC}$
 $\text{SIGMA US} = 0.044$

COMMENTS:

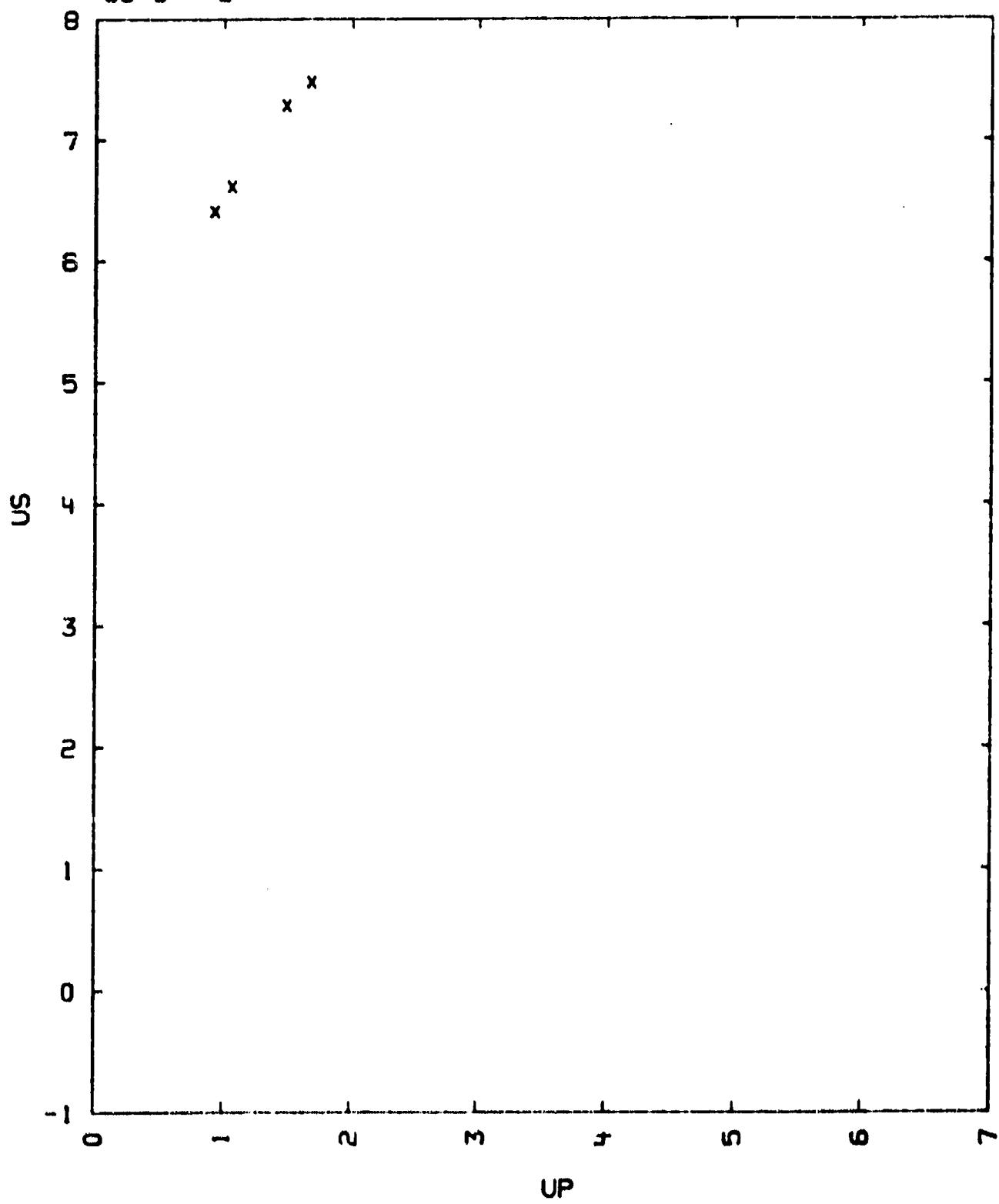
- 1) SOURCE: COMPILER
 L. R. L. EQUATION OF STATE FILE
 LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA
- 2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)
 DATA REDUCTION TECHNIQUE B.
- 3) TABULATED DATA ALSO REPORTED BY CHRISTIAN, R.H., IN
 EQUATION OF STATE OF ALKALI HALIDES AT HIGH PRESSURE (THESIS)
 UCRL-4900 MAY 16, 1957 UNIVERSITY OF CALIFORNIA.
 LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.
- 4) ALSO LISTED IN REFERENCE OF COMMENT 3 ARE:

DEBYE TEMPERATURE	646 DEG. K
HEAT CAPACITY (CV)	1.53 J/G/DEG.
EXPANSION COEFFICIENT	0.000102 PER DEG.
COMPRESSIBILITY	1.53 PER MEGABAR
MELTING POINT	845 DEG. C
- 5) THE VALUE OF V_{01} WAS OBTAINED FROM A LATTICE CONSTANT OF 4.0262 Å,
 AT 25 DEGREES CENTIGRADE.
 A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
 POLYCRYSTAL BOOK SERVICE 1963) 2ND EDITION.

TABLE I

LITHIUM FLUORIDE

98-9--2



98-9---3
LITHIUM FLUORIDE

LI-F

$$V_0 = 0.3774 \text{ CC/G}$$

$$V_{01} = 0.3789 \text{ CC/G}$$

IN THE TABLES BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN KM/SEC., AND PRESSURE IN KILOBARS. ST DESIGNATES THE STANDARD MATERIAL AND UP(ST) IS THE PARTICLE VELOCITY OF THE STANDARD.

TABLE I
SINGLE CRYSTAL

RHO0	US	UP	P	V/V0	ST	UP(ST)
2.65	8.94	2.87	680	0.680	AL	2.82
-	11.40	4.84	1460	0.575	FE	3.60
-	11.75	5.17	1610	0.559	FE	3.85
-	13.10	6.11	2120	0.535	AL	6.03
-	18.30	10.01	4850	0.452	AL	9.95

$$US = 5.05 + 1.319 UP \text{ KM/SEC. } \sigma \text{ US } = 0.10 \text{ KM/SEC.}$$

$$V_0 = 1.71 - 0.566 \text{ CC/G.}$$

TABLE II
POROUS

RHO0	US	UP	P	V/V0	ST	UP(ST)
1.71	11.70	6.19	1239	0.471	FE	4.13
1.27	4.52	2.40	138	0.474	AL	1.60
1.27	11.12	6.59	935	0.407	FE	4.13
0.883	10.57	7.03	655	3.35	FE	4.13
0.566	10.21	7.44	430	2.71	FE	4.13

$$US =$$

COMMENTS:

- 1) SOURCE: KURMER, S. B., SINITSYN, M. V., FUNKOV, A. I., URLIN, V. D. AND B. INOV, A. V.
SOVIET PHYS-JETP, VOL. 20, P. 811 (1965)
J. EXPTL. THEORET. PHYS. (U.S.S.R.) VOL. 47, P. 1202 (1964)
- 2) EXPERIMENTAL TECHNIQUE A
DATA REDUCTION TECHNIQUE B
- 3) V01 WAS CALCULATED USING THE LATTICE CONSTANT OF 4.0262 ANGSTROMS,
AT 25 DEGREES CENTIGRADE. SEE CRYSTAL DATA DETERMINATIVE
TABLES (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION, 1963) 2ND ED.
- 4) THE MEASURED EXPERIMENTAL ERROR IN THE SHOCK VELOCITY BELOW 10 KM/SEC
IS LESS THAN 1 PERCENT AND FOR THE HIGHER VALUES THE ERROR IS
APPROXIMATELY 2 PERCENT. THE VALUE OF THE SHOCK VELOCITY WAS

DETERMINED FROM 5-8 EXPERIMENTS.

C) ADDITIONAL CONSTANTS LISTED:

HEAT CAPACITY = 1.923 JOULES/G/DEG.

BAND GAP = 11.5 EV

- 6) THE ALUMINUM STANDARD HUGONIOT IS CHARACTERIZED BY THE FOLLOWING
RELATIONSHIP: $U_S = 5.254 + 1.458 \cdot U_P - 0.0276 \cdot U_P^{+2} + 0.00103 \cdot U_P^{+3}$
 $\Sigma \sigma_u u_s = 0.013 \text{ KM/SEC. FOR } U_P = 0 \text{ TO } 10.5 \text{ KM/SEC}$
 $\rho_{H0} = 2.71 \text{ G/CC.}$

TABLE I

LITHIUM FLUORIDE
98-9---3

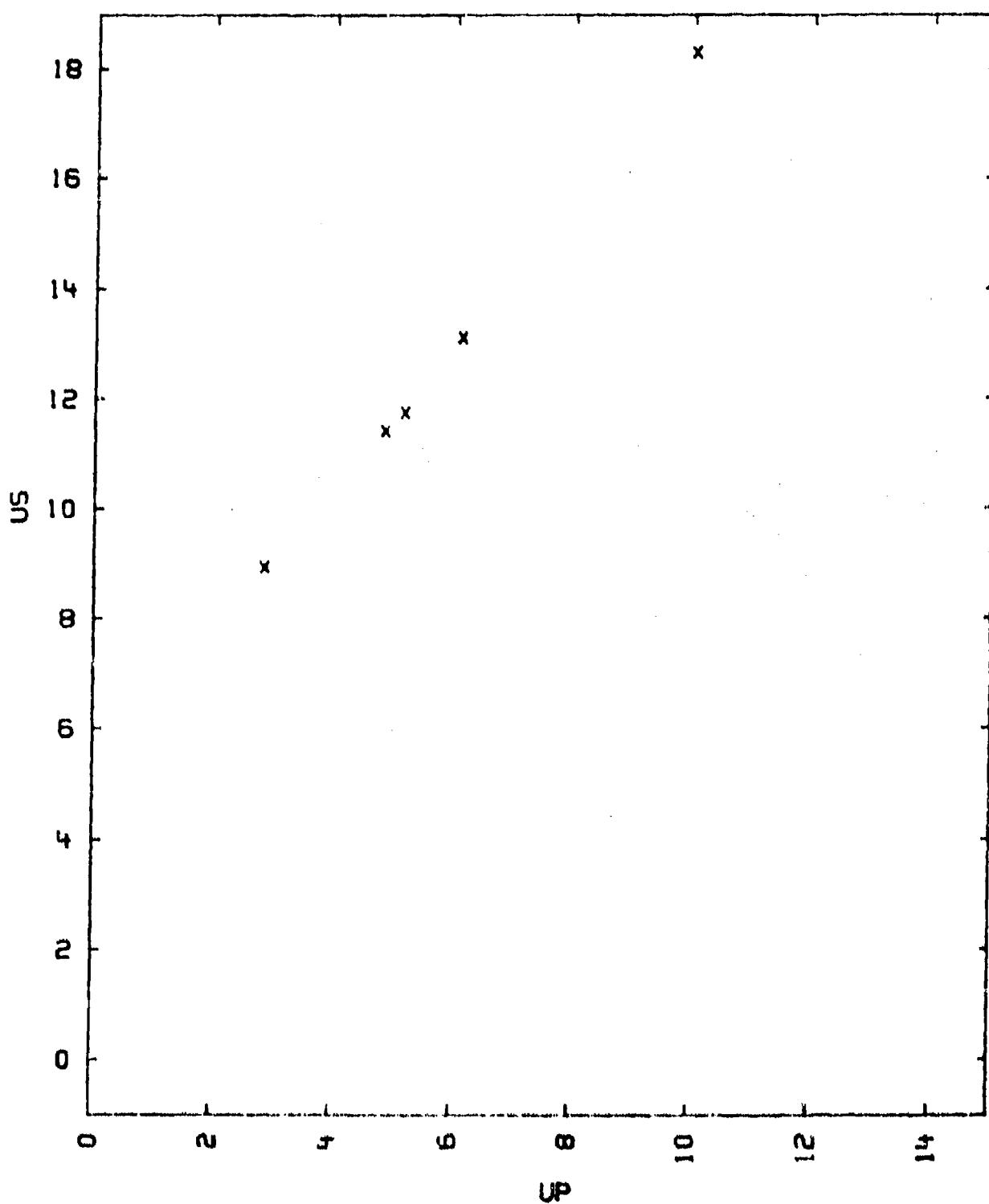
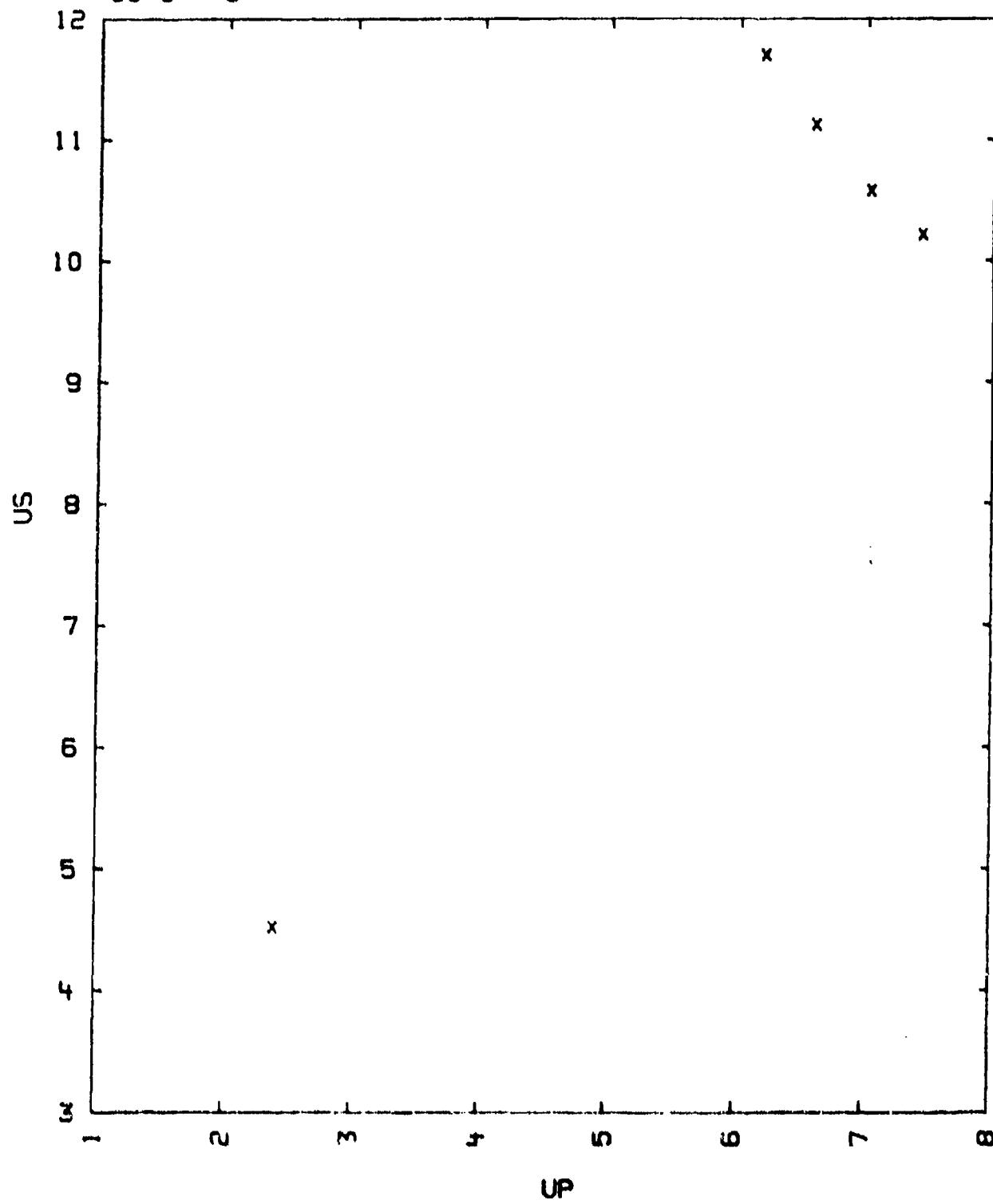


TABLE II

LITHIUM FLUORIDE

98-9---3



98-9---4
LITHIUMFLUORIDE

LI-F

$$V_0 = 0.3782 \text{ CC}/\text{G}.$$

$$V_{01} = 0.3789 \text{ CC}/\text{G}.$$

THE TABLE LISTS DENSITY IN G/CC., VELOCITIES IN KM/SEC AND PRESSURE IN KBAR. STND = STANDARD MATERIAL. AL = ALUMINUM. PLAL = FLEXIGLAS AND AL.

TABLE

RHO0	US	UP	P	V/V0	STND	DIR
2.637	7.66	1.80	363.	0.765	AL	(100)
-	7.63	1.80	362.	0.764	-	-
-	7.48	1.69	333.	0.774	-	-
-	7.44	1.64	322.	0.780	-	-
-	7.41	1.60	313.	0.784	-	-
-	7.36	1.60	310.	0.783	-	-
-	7.17	1.45	274.	0.790	-	-
-	7.09	1.45	271.	0.795	-	-
-	7.03	1.45	269.	0.794	-	-
-	6.84	1.20	216.	0.824	-	-
-	6.46	0.91	155.	0.699	-	-
-	8.10	2.31	493.	0.715	-	-
-	8.34	2.45	539.	0.706	-	-
-	8.36	2.40	529.	0.713	-	-
-	8.39	2.42	535.	0.712	-	-
-	8.44	2.55	568.	0.698	-	-
-	8.73	2.71	624.	0.690	-	-
-	9.18	2.97	719.	0.678	-	-
-	9.45	3.10	792.	0.663	-	-
-	9.69	3.32	848.	0.657	-	-
-	9.69	3.34	853.	0.655	-	-
-	9.82	3.35	867.	0.659	-	-
-	7.56	1.69	337.	0.778	PLAL	-
-	7.30	1.54	296.	0.789	-	-
-	7.14	1.49	280.	0.791	-	-
-	6.73	1.18	209.	0.824	-	-
-	7.50	1.74	344.	0.768	AL	(111)
-	6.69	1.18	208.	0.824	-	-
-	7.27	1.59	305.	0.781	PLAL	-
-	7.09	1.48	277.	0.791	-	-
-	7.09	1.44	269.	0.797	-	-

US = $5.09 + 1.405 \cdot UP$ KM/SEC. UP LESS THAN 1.9 KM/SEC.

S10 US = 0.06 KM/SEC.

US = $4.59 + 1.537 \cdot UP$ KM/SEC. UP GREATER THAN 2.2 KM/SEC.

S10 US = 0.057 KM/SEC.

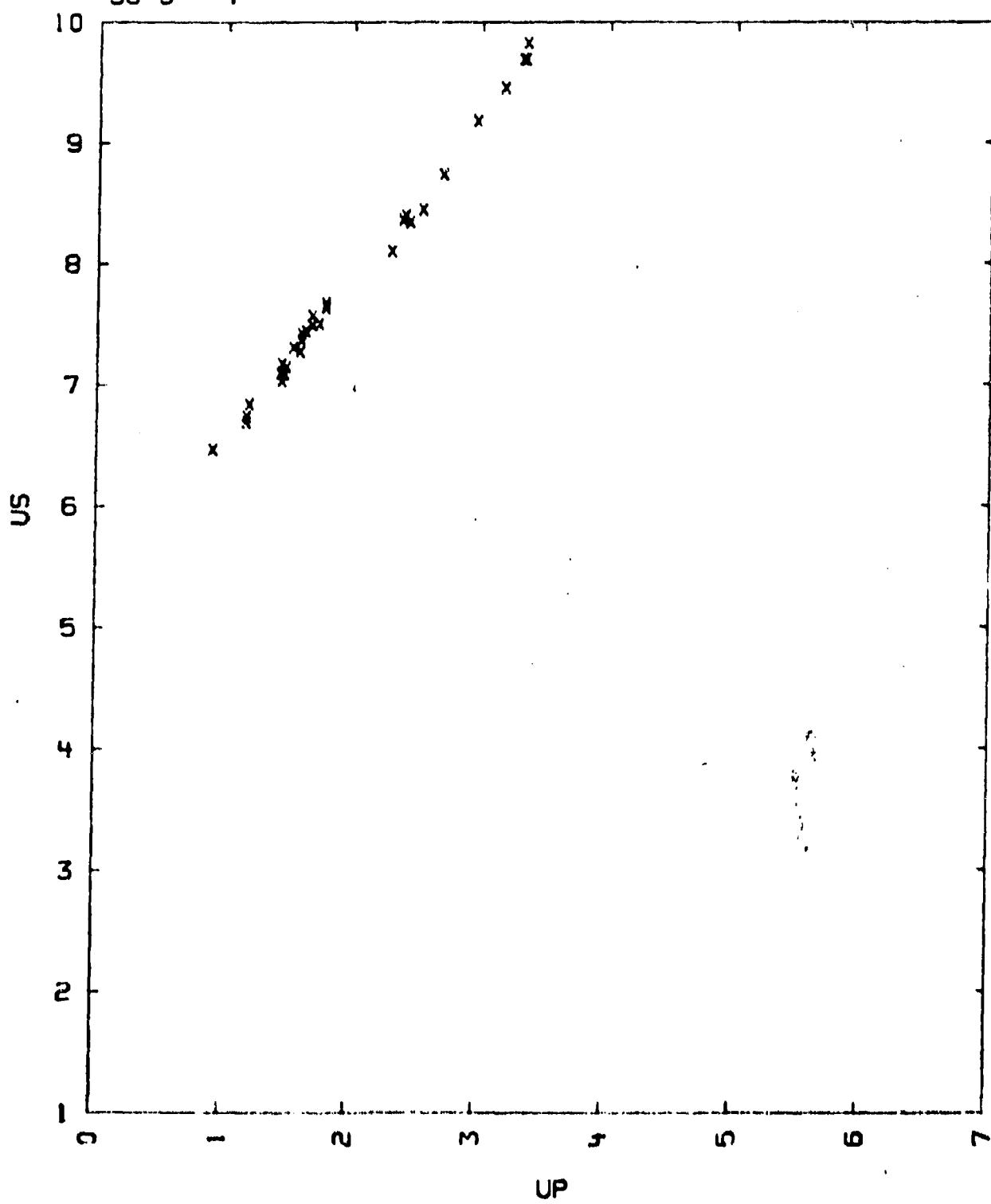
COMMENTS:

- 1) SOURCE: HAUVER, G. E. AND MELANI, A.
PRIVATE COMMUNICATION (1969)
BALLISTICS RESEARCH LABS., ABERDEEN PROVING GROUND, MARYLAND.
- 2) EXPERIMENTAL TECHNIQUE: H FOR THOSE POINTS MARKED WITH PLAL
CL - - - - AL
- DATA REDUCTION METHOD: B
- 3) PLATES OF ALUMINUM AND TITANIUM WITH KNOWN EQUATION OF STATE WERE
USED. THE ADIABATIC UNLOADING PATHS IN THE P VS UP PLANE WERE REPRE-
SENTED BY THE REFLECTION OF THE HUGONIOT, SLIGHTLY ADJUSTED TO GO
THROUGH THE POINT $0.1(UFS+2UP)^{1/2}$, FOR THOSE POINTS MARKED WITH AL.
THE AL CROSS CURVE OF THE POINTS MARKED WITH PLAL WAS LOCATED WITH
THE KNOWN P-UP CURVE OF A PLEXIGLAS DISK. FOR THE PLEXIGLAS USED:
 $US = 2.702 + 1.544 \cdot UP$ KM/SEC AND $\rho_{H0} = 1.18$ G/CC
SEE HAUVER, G.E. AND MELANI, A. BRL REPORT NO. 1259, AUGUST 1964.
- 4) THE ABOVE TWO LINE FIT IS THE SIMPLEST REPRESENTATION THAT YIELDS A
GOOD FIT
- 5) FURTHER WORK IS IN PROGRESS.
- 6) VOI HAS CALCULATED FROM A LATTICE CONSTANT OF 4.0262 ANGSTROMS (25
DEG. C.), CRYSTAL DATA DETERMINATIVE TABLES (AMERICAN CRYSTALLOGRAP-
HIC ASSOCIATION, POLYCRYSTAL BOOK SERVICE, BROOKLYN, N.Y., 1963)
2ND ED

UOG/14/77

TABLE I

LITHUMFLUORIDE
98-9---4



98-10---1
LITHIUM CHLORIDE

LI-CL PRESSED

$V_0 = 0.486 \text{ CC/G}$
 $V_{01} = 0.4823 \text{ CC/G}$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICROSEC,
AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UFS	UP	P	V/V0	PRESSURE IN AL BASE PLATE
2.050	5.48	2.37	1.09	121	0.802	162
2.070	5.80	2.06	1.42	170	0.796	225
2.051	6.32	3.79	1.78	230	0.720	303
2.061	6.57	4.24	1.94	263	0.704	345

$US = 4.049 + 1.281 UP \text{ MM/MICROSEC}$
 $\text{SIGMA US} = 0.063$

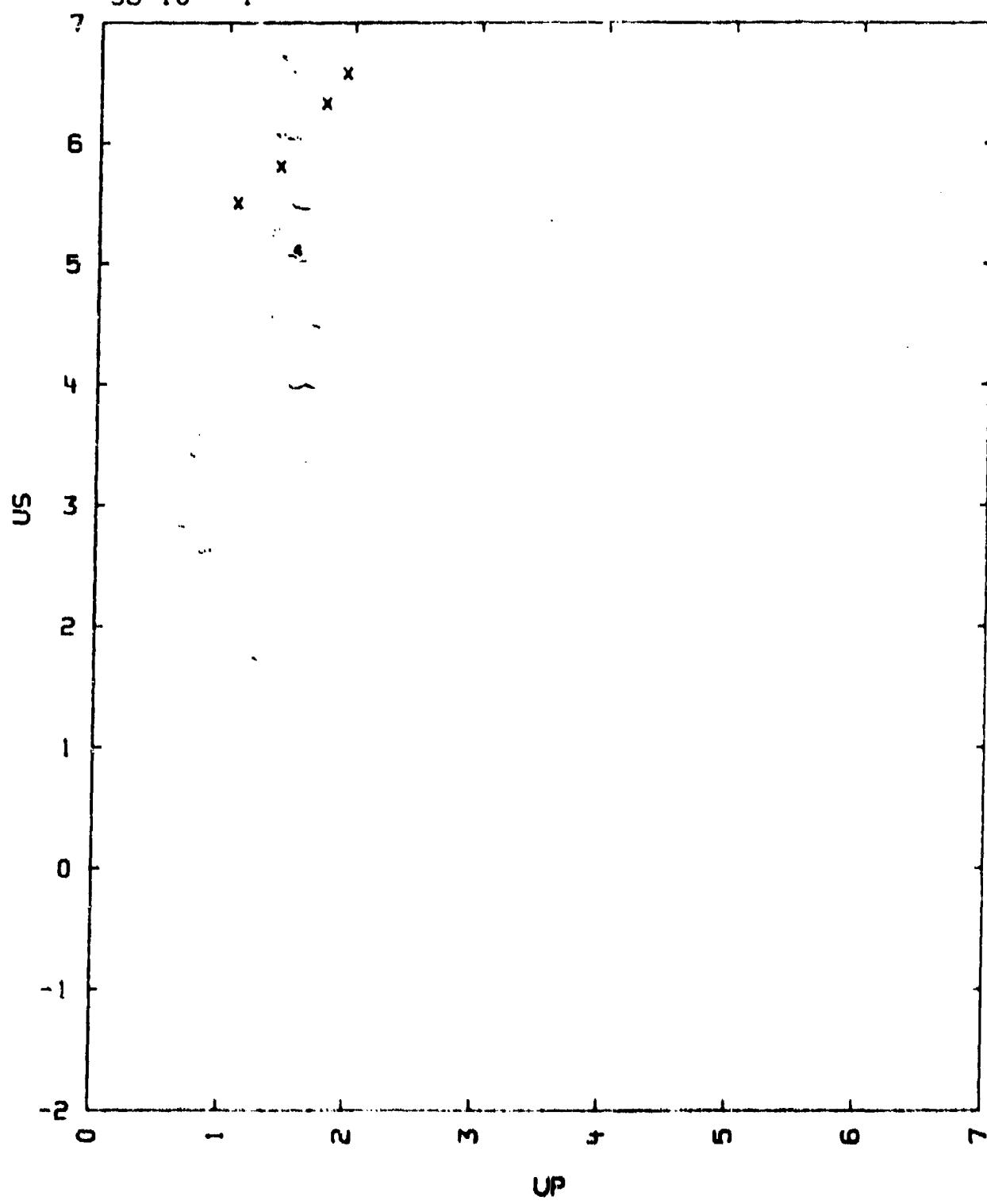
COMMENTS:

- 1) SOURCE: COMPILER
L. R. L. EQUATION OF STATE FILE
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA
- 2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)
DATA REDUCTION TECHNIQUE B.
- 3) TABULATED DATA ALSO REPORTED BY CHRISTIAN, R.H., IN
EQUATION OF STATE OF ALKALI HALIDES AT HIGH PRESSURE (THESIS)
UCRL-4900 MAY 10, 1957 UNIVERSITY OF CALIFORNIA,
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.
- 4) ALSO LISTED IN REFERENCE OF COMMENT 3 ARE:

DEBYE TEMPERATURE	330 DEG. K
HEAT CAPACITY (CV)	1.11 J/G/DEG.
EXPANSION COEFFICIENT	0.000122 PER DEG.
COMPRESSIBILITY	3.41 PER MEGABAR
MELTING POINT	610 DEG. C
- 5) THE VALUE OF V_{01} WAS OBTAINED FROM A LATTICE CONSTANT OF 5.13988 A
A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE 1963) 2ND EDITION.

TABLE I

LITHIUM CHLORIDE
98-10---1



98-11---1
LITHIUM BROMIDE

LI-BR PRESSED

$V_0 = 0.207 \text{ CC}/\text{O}$
 $V_{01} = 0.2086 \text{ CC}/\text{O}$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICROSEC,
AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UFS	UP	P	V/V0	PRESSURE IN AL BASE PLATE
3.26	4.12	2.48	1.02	138	0.792	162
3.304	4.51	2.89	1.30	194	0.712	225
3.307	4.96	-	1.63	267	0.671	303
3.30	4.97	-	1.82	298	0.634	345
3.324	4.82	3.36	1.62	260	0.564	299
3.379	3.58	1.81	0.92	111	0.745	139
3.429	4.22	2.42	1.26	186	0.702	215
3.428	5.19	3.62	1.83	328	0.647	363
3.429	3.67	1.39	0.68	98	0.815	103
3.445	4.48	2.86	1.25	192	0.722	218
3.452	5.07	3.52	1.75	306	0.655	341

$US = 2.618 + 1.379 UP \text{ MM/MICROSEC}$
 $\text{SIGMA US} = 0.150$

COMMENTS:

1) SOURCE: COMPILER

L. R. L. EQUATION OF STATE FILE

LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA

2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)
DATA REDUCTION TECHNIQUE B.

3) PART OF THE TABULATED DATA ALSO REPORTED BY CHRISTIAN, R. H., IN
EQUATION OF STATE OF ALKALI HALIDES AT HIGH PRESSURE (THESIS)
UCRL-4900, MAY 16, 1957, UNIVERSITY OF CALIFORNIA,
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.

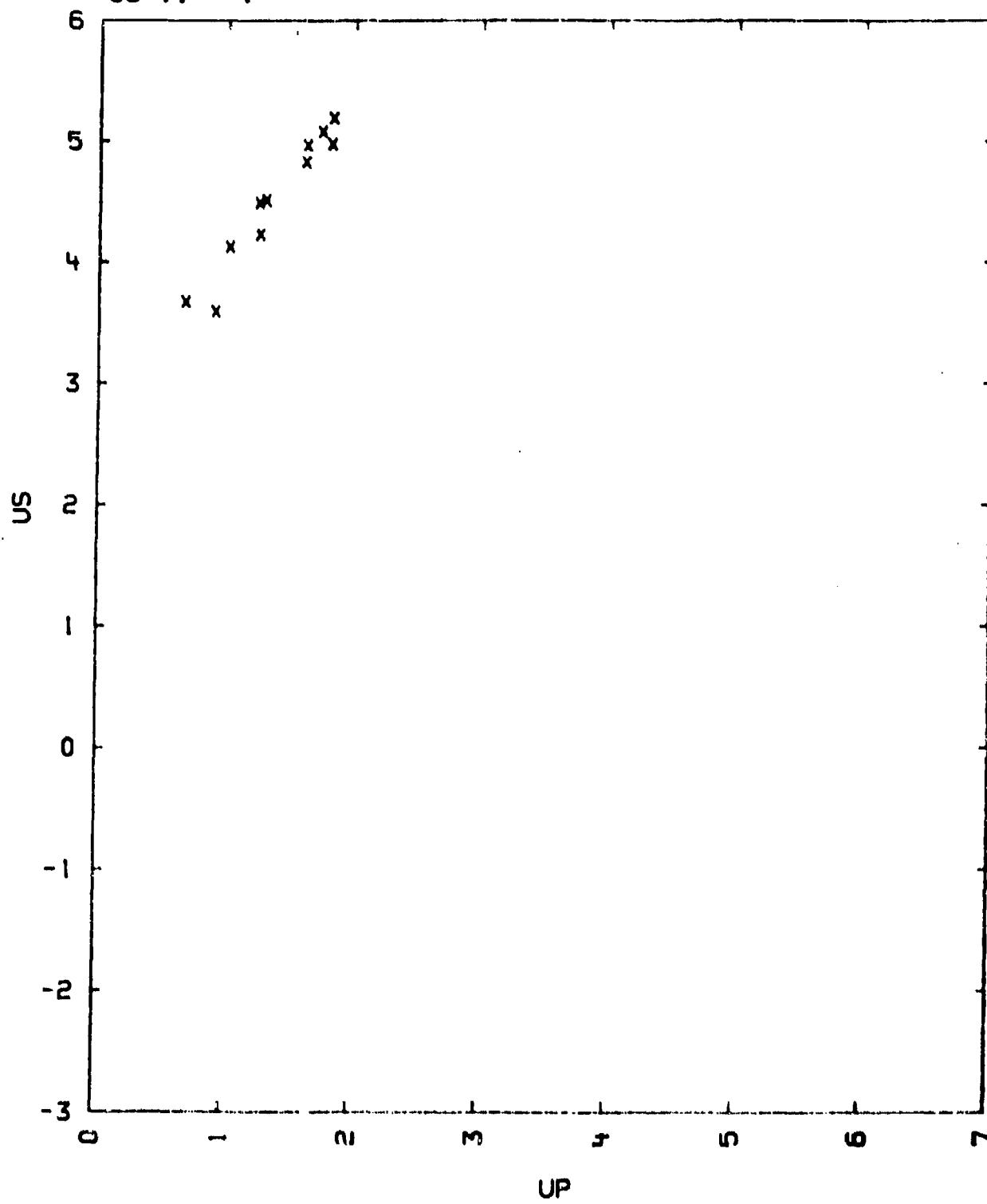
4) ALSO LISTED IN REFERENCE OF COMMENT 3 ARE:

DEBYE TEMPERATURE	210 DEG. K
HEAT CAPACITY (CV)	0.95 J/G/DEG.
EXPANSION COEFFICIENT	0.000140 PER DEG.
COMPRESSIBILITY	4.31 PER MEGABAR
MELTING POINT	550 DEG. C

5) THE VALUE OF V_{01} WAS OBTAINED FROM A LATTICE CONSTANT OF 5.301 Å
A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE, 1963) 2ND EDITION.

TABLE I

LITHIUM BROMIDE
98-11---1



98-12---1
LITHIUM IODIDE

Li-I SINGLE CRYSTAL

$$\rho_0 = 0.249 \text{ CC/G}$$

$$\rho_{01} = 0.2444 \text{ CC/G}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN MM/MICROSEC.
AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	V0	UP	P	VIVO	PRESSURE IN AL. BASE PLATE
4.016	4.01	-	1.27	205	0.683	227
4.008	4.24	-	1.58	268	0.628	296
4.016	4.47	-	1.78	320	0.602	352

$$US = 2.869 + 0.888 UP \text{ MM/MICROSEC}$$

SIGMA US = 0.040

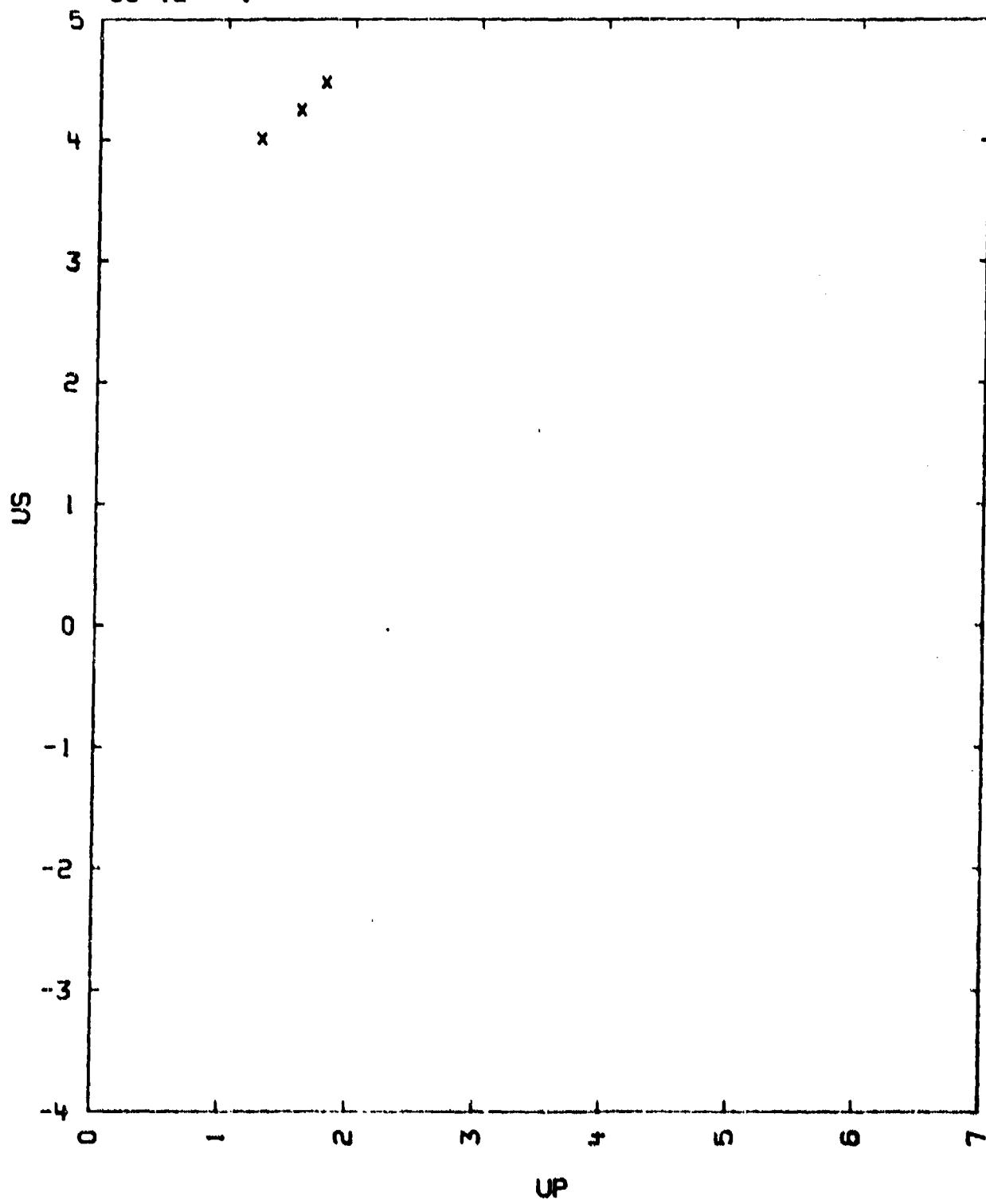
COMMENTS:

- 1) SOURCE: CHRISTIAN, R. H.
REPORT NO. UCRL-4900 (1957)
EQUATION OF STATE OF ALKALI HALIDES AT HIGH PRESSURE (THESIS)
LAURENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA
- 2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)
DATA REDUCTION TECHNIQUE B.
- 3) ALSO LISTED IN REFERENCE OF COMMENT 1 ARE:
 DEBYE TEMPERATURE 100 DEG. K
 HEAT CAPACITY (CV) 0.37 J/G/DEG.
 EXPANSION COEFFICIENT .0.000167 PER DEG.
 COMPRESSIBILITY 6.01 PER MEGABAR
 MELTING POINT 465 DEG. C
- 5) THE VALUE OF V01 WAS OBTAINED FROM A LATTICE CONSTANT OF 6.012 A
A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE 1963) 2ND EDITION.

U06/14/77

TABLE I

LITHIUM IODIDE
98-12---1



98-12---2
LITHIUM IODIDE

LI-I PRESSED

$$V_0 = 0.302 - 0.263 \text{ CC/G}$$

$$V_{01} = 0.2444 \text{ CC/G}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICROSEC., AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UFS	UP	P	V/V0	PRESSURE IN AL BASE PLATE
3.313	4.81	-	1.88	288	0.593	340
3.486	3.72	2.09	0.89	116	0.761	159
3.809	4.23	3.79	1.61	258	0.619	295
3.761	3.78	2.55	1.27	181	0.664	215
3.797	3.28	1.41	0.69	85	0.791	103
3.747	3.90	2.93	1.27	186	0.674	216

US =

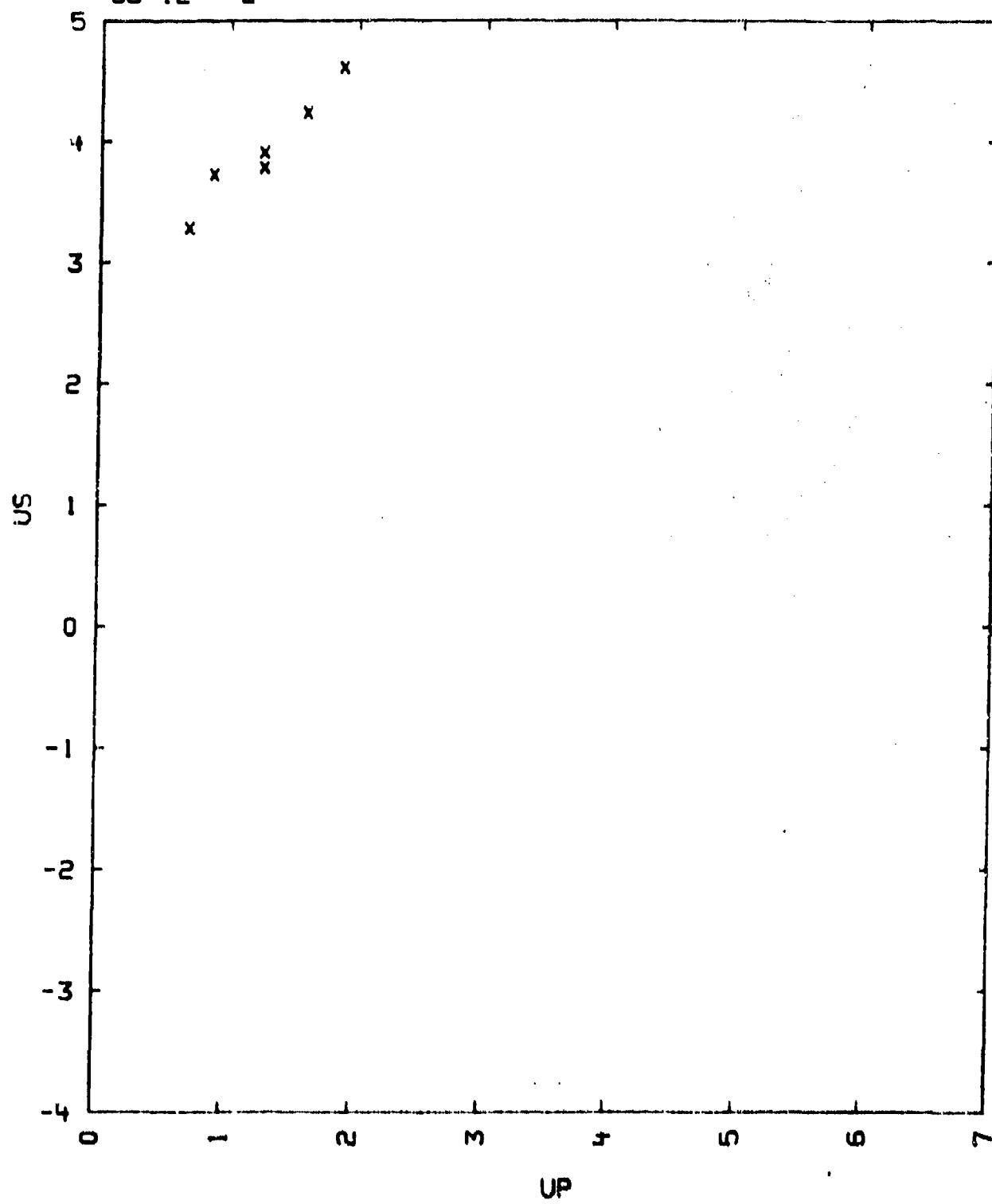
COMMENTS:

- 1) SOURCE: COMPILER
L. R. L. EQUATION OF STATE FILE
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA
- 2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)
DATA REDUCTION TECHNIQUE B.
- 3) THE VALUE OF V01 WAS OBTAINED FROM A LATTICE CONSTANT OF 0.012 A
A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE 1963) 2ND EDITION.

TABLE I

LITHIUM IODIDE

98-12---2



99-9---1
SODIUM FLUORIDE
NA-F PRESSED

$$V_0 = 0.362 \text{ CC}/\text{O}$$

$$V_{01} = 0.3554 \text{ CC}/\text{O}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN MM/MICROSEC., AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UFS	UP	P	V/V0	PRESSURE IN AL BASE PLATE
2.727	4.80	0.97	0.90	83	0.881	74
2.768	5.45	1.90	0.98	144	0.825	161
2.773	5.68	2.52	1.24	196	0.781	220
2.774	6.12	3.47	1.78	302	0.709	343
2.773	6.27	3.17	1.54	268	0.754	293
2.779	5.20	1.48	0.76	110	0.853	124

$$US = 4.172 + 1.223 UP \text{ MM/MICROSEC}$$

SIGMA US = 0.195

COMMENTS:

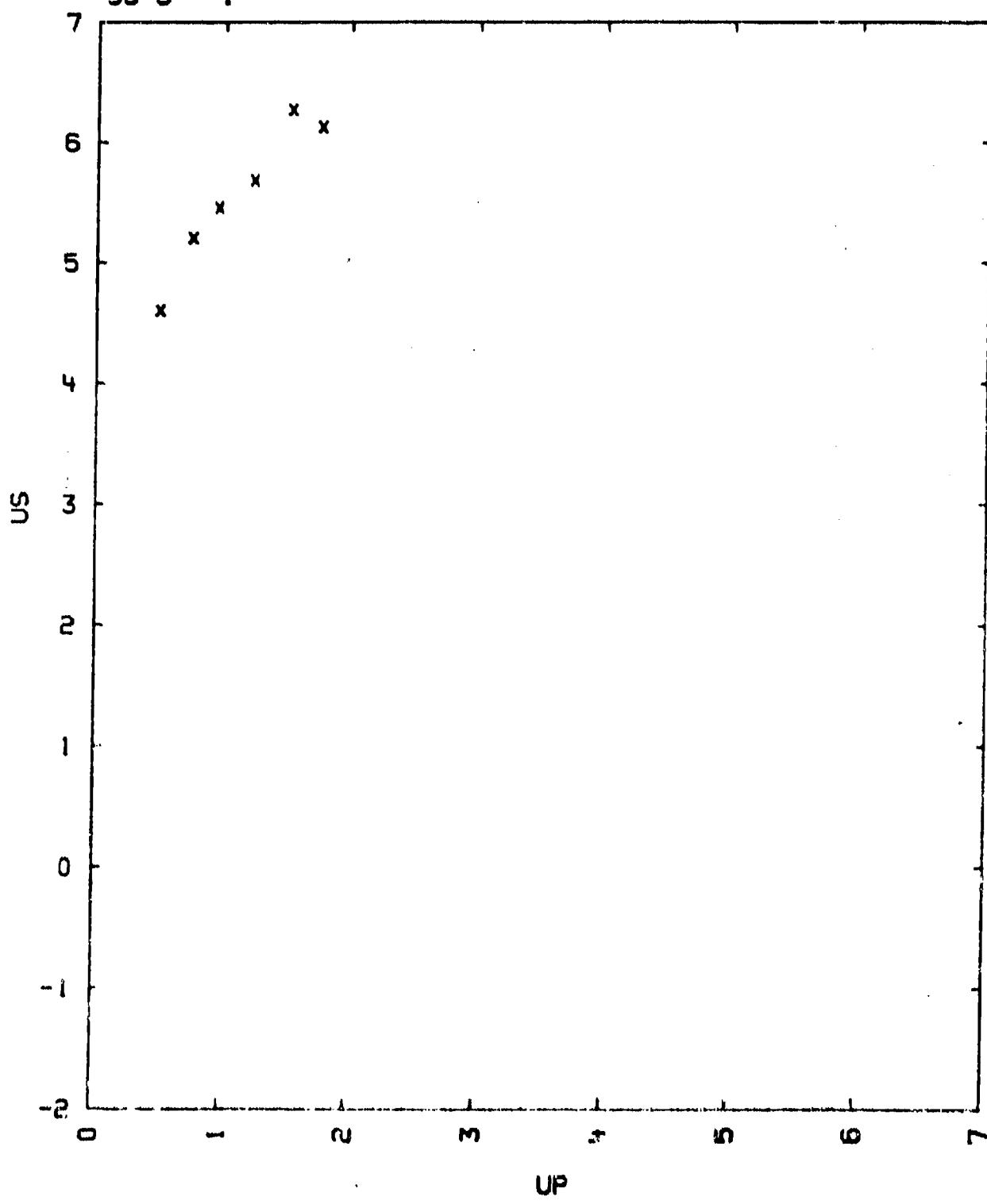
- 1) SOURCE: COMPILER
L. R. L. EQUATION OF STATE FILE
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA
- 2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)
DATA REDUCTION TECHNIQUE B.
- 3) THE FOLLOWING DATA WAS OBTAINED FROM CHRISTIAN, R. H.
EQUATION OF STATE OF ALKALI HALIDES AT HIGH PRESSURE (THESIS)
UCRL-4900 MAY 16, 1957, UNIVERSITY OF CALIFORNIA
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA:

DEBYE TEMPERATURE	439 DEG. K
HEAT CAPACITY (CV)	1.06 J/G/DEG.
EXPANSION COEFFICIENT	0.000098 PER DEG.
COMPRESSIBILITY	2.11 PER MEGABAR
MELTING POINT	995 DEG. C
- 4) THE VALUE OF V01 WAS OBTAINED FROM A LATTICE CONSTANT OF 4.628 A
A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE, BROOKLYN, N.Y., 1963) 2ND ED.

TABLE I

SODIUM FLUORIDE

99-9---1



99-10---0
SODIUMCHLORIDE SUMMARY

NA-CL.

$$V_0 = 0.463 - 1.01 \text{ CC}/0$$

$$V_{01} = 0.4622 \text{ CC}/0$$

$$C_0 = 3.380 \text{ KM/SEC}$$

THE TABLE LISTS HUGONIOT POINTS CALCULATED FROM THE FITS GIVEN BELOW.
 UNITS ARE: G/CC, KM/SEC, KBAR, AND KBAR.CC/G FOR THE ENERGY DIFFERENCE.
 TP = TRANSITION POINT.

TABLE

FIT	RHO0	US	UP	P	V/V0	E-E0	COMMENTS
1	2.165	4.147	.5	44.8	0.879	1.25	SOLID
	-	4.869	1.0	105.	0.798	5.0	-
	-	5.630	1.5	183.	0.734	11.2	-
	-	5.868	1.66	211.	0.717	13.8	TP 111 AXIS
	-	6.298	1.95	266.	0.690	19.0	TP 100 AXIS
2	-	6.271	2.2	299.	0.649	24.2	SOLID
	-	6.776	2.6	381.	0.616	33.8	-
	-	7.282	3.0	473.	0.588	45.0	-
3	-	7.890	3.2	547.	0.594	51.2	LQUID
	-	8.407	3.6	655.	0.572	64.8	-
	-	8.924	4.0	773.	0.552	80.0	-
	-	10.216	5.0	1106.	0.511	125.	-
	-	12.154	6.5	1710.	0.465	211.	-
4	-	11.794	6.8	1335.	0.423	231	-
	-	13.450	8.2	2308.	0.390	336	-
	-	15.107	9.6	3140.	0.364	461	-
	-	16.763	11.0	3992.	0.344	605	-
5	1.43	4.721	2.0	135.	0.576	20.0	
	-	6.123	3.0	263.	0.510	45.0	
	-	7.526	4.0	430.	0.468	80.	
	-	10.331	6.0	886.	0.419	180.	
	.091	3.721	2.0	73.8	.462	20.0	
	-	5.157	3.0	153.	.418	45.0	
	-	8.030	5.0	398.	.377	125.	
	-	10.803	7.0	756.	.359	245.	

US = 3.406 + 1.483*UP, SIG.US = 0.06 KM/SEC (FOR FIT 1)
 FOR UP BETWEEN .4 AND 2 (COMMENT 2 AND 3)
 US = 3.49 + 1.264*UP, SIG.US = 0.11 KM/SEC (FOR FIT 2)
 FOR UP BETWEEN 2.2 AND 3.0
 US = 3.756 + 1.292*UP, SIG.US = 0.11 KM/SEC (FOR FIT 3)
 FOR UP BETWEEN 3.2 AND 6.5
 US = 3.75 + 1.183*UP, SIG.US = 0.07 KM/SEC (FOR FIT 4)

FOR UP BETWEEN 6.8 AND 11.

$$US = 3.426 + 1.346 \cdot UP - 1.82(2.165-RH00) + 0.077(2.165-RH00)UP$$

$$- 0.32(2.165-RH00)^2$$

SIG.US = 0.11 KM/SEC (FOR FIT 5)

FOR UP BETWEEN THE LIMITS OF THE TABLE

COMMENTS :

1) SOURCE: COMPILER

DATA SOURCES WERE USED AS FOLLOWS:

PAGES 99-10---2,3 AND 4	FIT 1 AND 2
- 99-10---1,3,4 AND 5	FIT 3
- 99-10---5	FIT 4
- 99-10---1 AND 5	FIT 5

2) SIGNIFICANCE OF THE FITS:

FIT 1: SOLID PHASE, ORIGINAL NA-CL STRUCTURE

- 2: CS-CL STRUCTURE : THE ONLY EVIDENCE FOR PLACING THE PHASE CHANGE THIS HIGH, IS THE RATE OF INCREASE OF THE TRANSFORMATION PRESSURE IN K-CL WHEN NA-CL IS ADDED.

S. WIEDERHORN AND H. O DRICKAMER J. APPL. PHYS., V. 31, P. 1665
(1960).

FIT 3: LIQUID PHASE AND MIXED LIQUID-SOLID PHASES:

KORMER, S. B. ET AL., Z. EKSP. TEOR. FIZIKI, V. 48, P. 1033 (1965)

FIT 4: VERY HIGH PRESSURE DATA OF 99-10---5, CHANGE IN SLOPE COULD BE DUE TO ELECTRONIC EXCITATION.

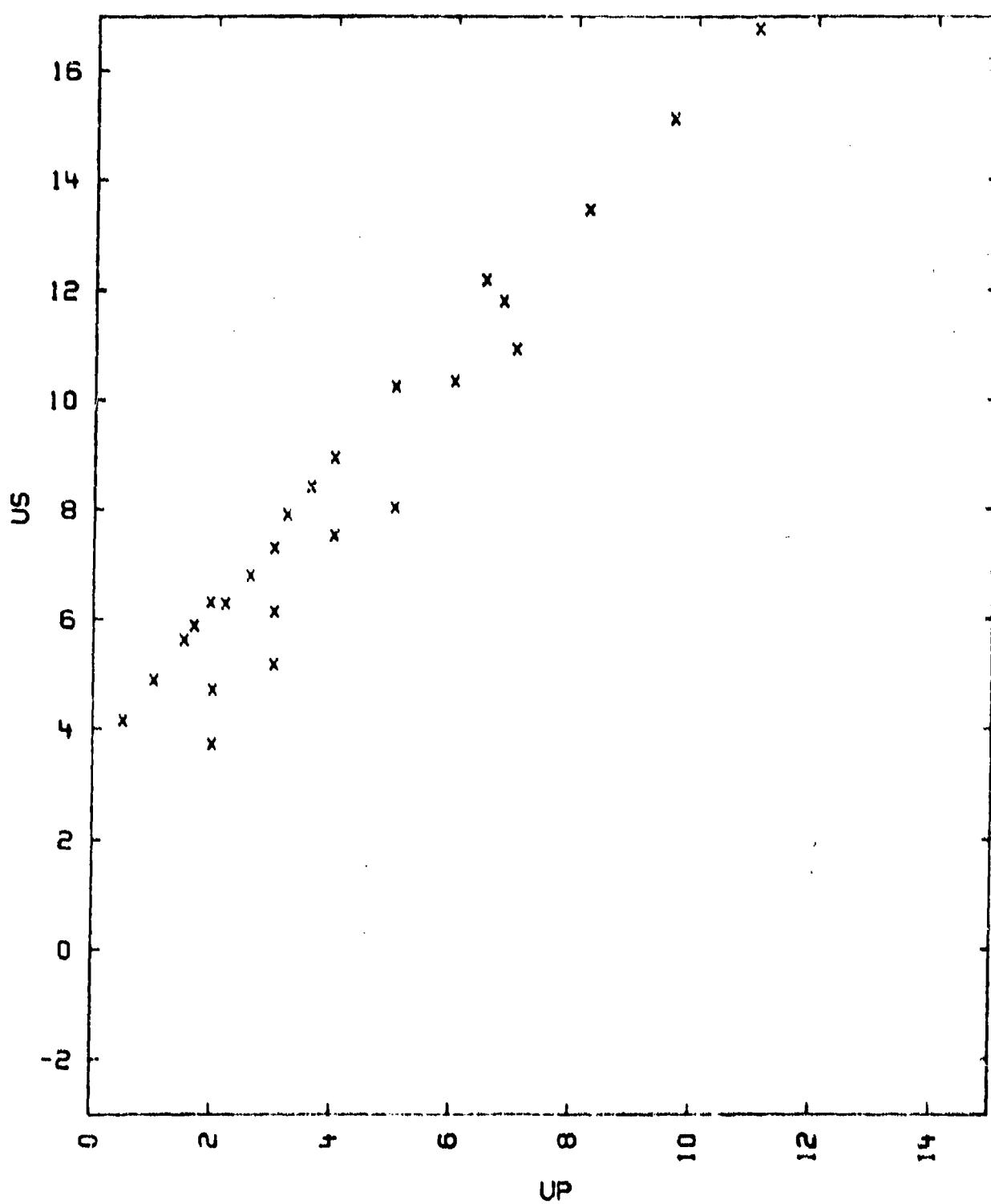
FIT 5: USEFUL FOR POROUS SAMPLES. POROUS DATA DO NOT SHOW THE TRANSITIONS.

3) DATA OF 99-10---2 AND 3 SHOW THE TRANSITION POINT AT UP = 2.05 AND 1.94 RESPECTIVELY FOR SHOCKS TRAVELING ALONG THE 100 CRYSTAL AXIS. UP = 1.66 IS THE ESTIMATED TRANSFORMATION POINT FOR FOR SHOCKS ALONG THE 111 DIRECTION.

TABLE I

SODIUMCHLORIDE SUMMARY

99-10---0



99-10---1
SODIUM CHLORIDE

NA-CL

$$V_0 = 0.463 \text{ CC}/\text{G}$$

$$V_{01} = 0.4617 \text{ CC}/\text{G}$$

$$C_B = 3.32 \text{ KM}/\text{SEC}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS. SH DESIGNATES SAMPLE HOLDER.

TABLE

RHO0	US	UP	P	V/V0	SH	UP(SH)
2.16	4.16	0.59	53	0.862	CU	0.37
-	4.73	0.98	100	0.794	AL	0.70
-	5.29	1.33	152	0.748	AL	1.10
-	5.41	1.55	182	0.719	FE	1.03
-	5.59	1.59	193	0.714	AL	1.32
-	5.66	1.71	209	0.699	AL	1.42
-	5.96	1.85	236	0.690	AL	1.54
-	6.18	2.07	276	0.667	AL	1.74
-	7.35	3.24	547	0.588	AL	2.80
-	8.91	4.10	790	0.540	FE	2.80

$$US = 3.40 + 1.35 UP \text{ KM}/\text{SEC}$$

$$\Sigma \sigma US = 0.06$$

FOR UP BETWEEN 0.6 AND 4.1 KM/SEC

COMMENTS:

- 1) SOURCE: AL'TSHULER, L.V., KULESHOVA, L.V. AND PAVLOVSKII, M.N.
SOVIET PHYS.-JETP, VOL. 12, P. 10 (1961)
- 2) EXPERIMENTAL TECHNIQUE A
DATA REDUCTION TECHNIQUE B.
- 3) THE SAMPLES WERE POSITIONED ON PLATES OF CU, AL AND FE AS INDICATED IN COLUMN 6 AND 7 OF THE TABLE.
- 4) THE HUGONIOTS OF THESE PLATE MATERIALS WERE TAKEN FROM
AL'TSHULER, L.V., KORMER, S.B., BAKANOVA, A.A., AND TRUNIN, R.F.
SOVIET PHYSICS JETP VOL 11, P. 573 (1960)
THE UNLOADING ADIABATS WERE OBTAINED BY REFLECTING THE HUGONIOT IN
THE PRESSURE-PARTICLE VELOCITY PLANE.
- 5) CB AS WELL AS THE DEBYE TEMPERATURE 281 DEG. K
HEAT CAPACITY 1CV 0.821 J/G/DEG.
EXPANSION COEFFICIENT 0.000116 PER DEG.
CATION TO ANION DISTANCE 2.814 KX

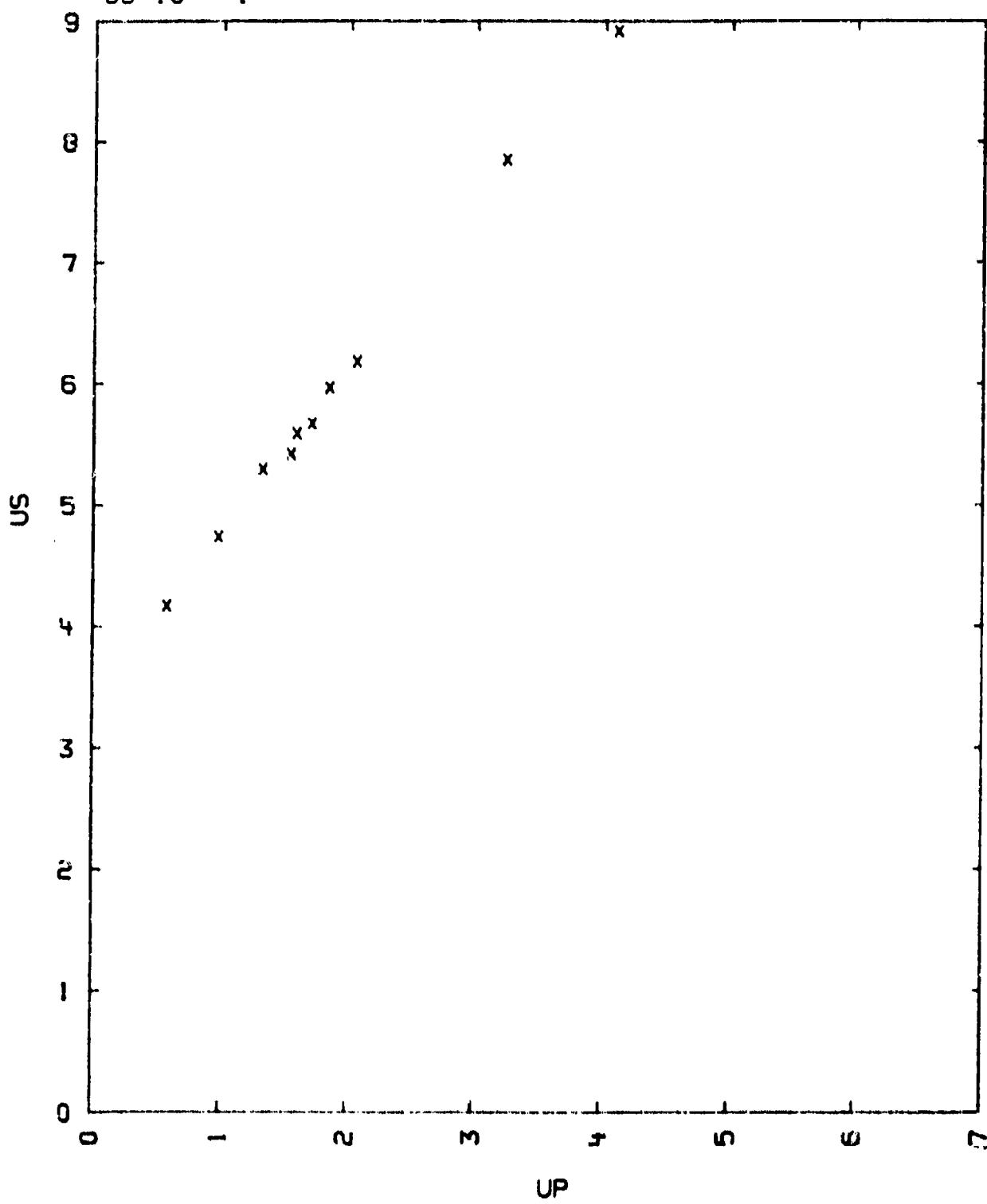
WERE OBTAINED FROM AL'TSHULER, L.V., PAVLOVSKII, M.N. AND
KULESHOVA, L.V. SOVIET PHYSICS-SOLID STATE VOL. 5, P. 203 (1963)

- 6) THE VALUE OF V01 LISTED HAS OBTAINED FROM A CATION TO ANION DISTANCE
OF 2.820 Å. SEE A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC
ASSOCIATION, POLYCRYSTAL BOOK SERVICE, BROOKLYN 1963) 2ND ED.

TABLE I

SODIUM CHLORIDE

99-10---1



99-10---2
 SODIUM CHLORIDE
 NA-CL SINGLE CRYSTAL

$$V_0 = 0.463 \text{ CC/O}$$

$$V_{01} = 0.4622 \text{ CC/O}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC. VELOCITIES IN KM/SEC AND PRESSURE IN KBARS. STND=STANDARD MATERIALS THAT DETERMIN THE PRESSURE:
 PLAL: PLEXIGLASS DEFINES THE AL CROSS-CURVE. AL: ALUMINUM STANDARD ONLY.
 DIR = SHOCK DIRECTION. DEG=DEGREES.

TABLE

RHO0	US	UP	P	V/V0	STND	DIR
2.16	4.92	1.06	110.	0.789	PLAL	(100)
-	4.94	1.08	113.	0.785	-	-
-	4.95	1.05	111.	0.790	-	-
-	4.96	1.09	115.	0.784	-	-
-	5.07	1.10	120.	0.783	-	-
-	5.14	1.17	128.	0.776	-	-
-	5.21	1.26	141.	0.760	-	-
-	5.29	1.32	147.	0.756	-	-
-	5.40	1.34	156.	0.752	-	-
-	5.43	1.42	160.	0.738	-	-
-	5.46	1.44	170.	0.736	-	-
-	5.48	1.41	167.	0.743	-	-
-	5.52	1.41	168.	0.744	-	-
-	5.61	1.56	189.	0.722	-	-
-	5.62	1.46	177.	0.740	-	-
-	5.62	1.50	182.	0.733	-	-
-	5.72	1.54	190.	0.731	-	-
-	5.82	1.69	212.	0.710	-	-
-	5.86	1.69	214.	0.712	-	-
-	5.87	1.71	217.	0.709	-	-
-	5.88	1.60	215.	0.714	-	-
-	5.88	1.73	220.	0.706	-	-
-	5.91	1.69	216.	0.714	-	-
-	5.98	1.73	223.	0.711	-	-
-	6.10	1.85	244.	0.697	-	-
-	6.20	1.95	261.	0.685	-	-
-	6.24	2.02	272.	0.676	-	-
-	5.84	1.74	219.	0.702	AL	-
-	5.93	1.68	215.	0.717	-	-
-	6.15	1.92	255.	0.688	-	-
2.16	6.33	2.05	280.	0.676	-	-
-	6.37	2.14	294.	0.664	-	-
-	6.43	2.36	328.	0.633	-	-
-	6.44	2.27	316.	0.647	-	-
-	6.45	2.39	333.	0.629	-	-
-	6.55	2.46	348.	0.624	-	-
-	6.74	2.50	364.	0.629	-	-
-	6.79	2.62	384.	0.614	-	-

SODIUM CHLORIDE

RHO0	US	UP	P	V/V0	STND	DIR
-	8.81	2.66	391.	0.609	-	-
-	6.88	2.66	395.	0.613	-	-
-	6.95	2.75	413.	0.604	-	-
-	6.99	2.76	417.	0.605	-	-
-	7.01	2.80	424.	0.600	-	-
-	7.15	2.91	449.	0.593	-	-
-	7.27	2.98	465.	0.593	-	-
-	7.43	3.08	484.	0.585	-	-
-	7.71	3.20	533.	0.585	-	-
-	7.95	3.33	572.	0.581	-	-
-	8.22	3.56	632.	0.567	-	-
-	8.34	3.70	682.	0.567	-	-
-	8.59	3.71	688.	0.568	-	-
-	4.79	0.88	80.	0.815	PLAL	(111)
-	5.00	1.04	112.	0.792	-	-
-	5.48	1.41	167.	0.743	-	-
-	5.72	1.54	190.	0.731	-	-
-	5.81	1.66	208.	0.714	-	-
-	5.94	1.97	253.	0.668	-	-
-	5.95	1.71	220.	0.713	-	-
-	5.98	1.81	234.	0.697	-	-
-	6.01	2.03	264.	0.662	-	-
-	6.06	2.05	268.	0.662	-	-
-	5.74	1.61	200.	0.720	AL	-
-	5.86	1.78	225.	0.696	-	-
-	5.99	1.95	252.	0.674	-	-
-	6.00	1.92	249.	0.680	-	-
-	6.08	1.75	255.	0.678	-	-
-	6.08	1.80	256.	0.704	-	-
-	6.25	2.20	297.	0.648	-	-
-	6.42	2.38	330.	0.629	-	-
-	6.90	2.65	395.	0.616	-	-
2.16	4.70	0.60	89.	0.813	PLAL	(110)
-	5.38	1.29	149.	0.759	-	-
-	5.43	1.42	166.	0.738	-	-
-	5.22	1.29	145.	0.753	-	(112)
-	5.36	1.36	157.	0.746	-	-

US = 3.52 + 1.382*UP KM/SEC. NACL STRUCTURE, UP LESS THAN 2.06

S10 US = 0.047 KM/SEC.

US = 3.26 + 1.35*UP KM/SEC. UP BETWEEN 2.2 AND 3.0 KM/SEC.

S10 US = 0.045 KM/SEC.

US = 2.43 + 1.65*UP KM/SEC. UP GREATER THAN 3.1 KM/SEC.

S10 US = 0.035 KM/SEC.

COMMENTS:

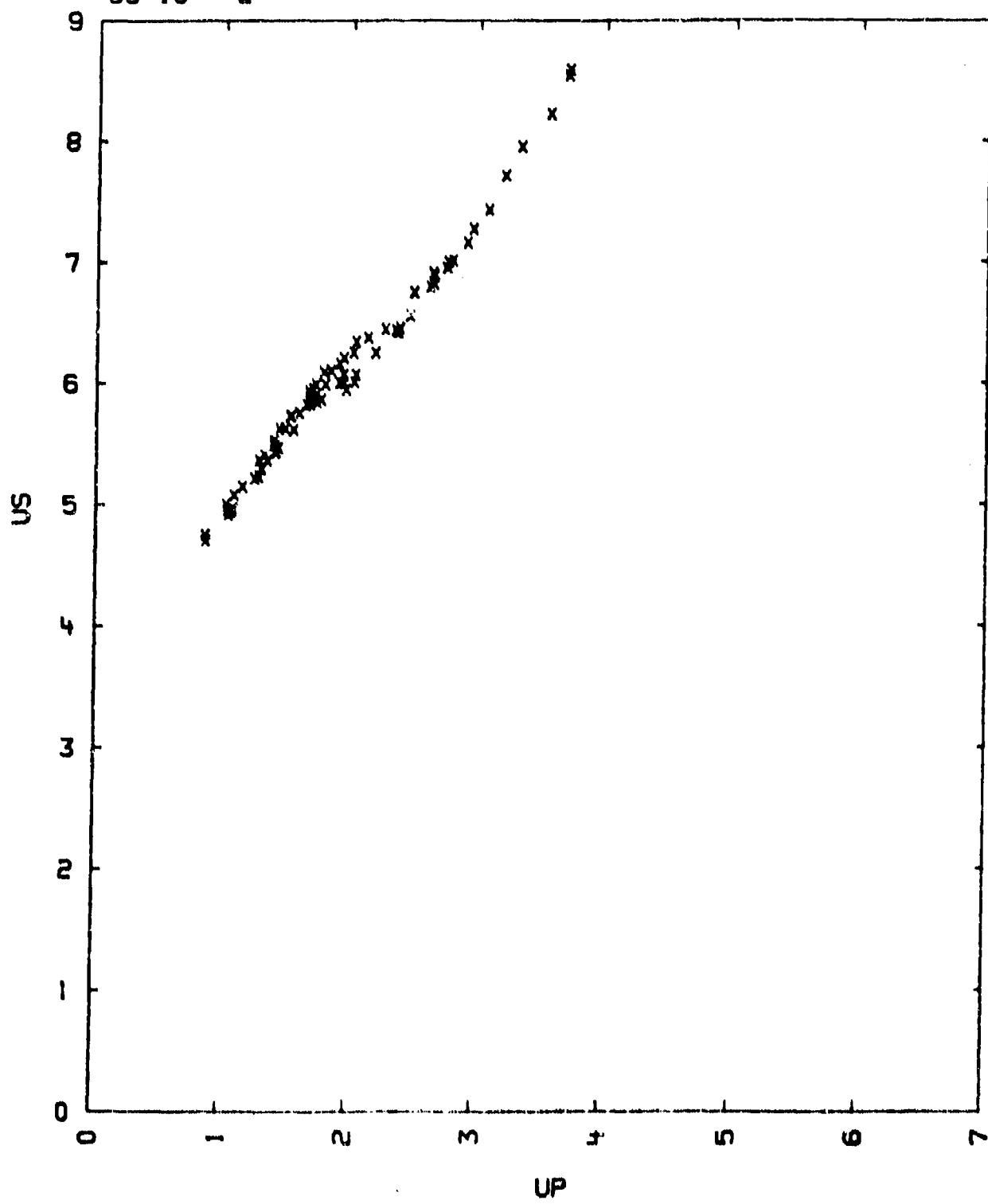
(1) SOURCE: HAUVER, G. E. AND MELANI, A.

B.R.L. REPORT BRL MR 2061 (1970)
BALLISTICS RESEARCH LABS., ABERDEEN PROVING GROUND,
MARYLAND, USA.

- 2) EXPERIMENTAL TECHNIQUE: H FOR THOSE POINTS MARKED WITH PLAL
C1 - - - - - AL
DATA REDUCTION METHOD: B
3) THE AL CROSS CURVE OF THE POINTS MARKED WITH PLAL WAS LOCATED WITH
THE KNOWN P-UP CURVE OF A PLEXIGLAS DISK. FOR THE PLEXIGLAS USED:
 $US = 2.895 + 1.538 \cdot UP$ KM/SEC AND $\rho_{HO} = 1.18$ G/CC
SEE HAUVER, O.E. AND MELANI, A. BRL REPORT NO. 1258, AUGUST 1964.
4) A TRANSITION IS OBSERVED AT $P = 280$ KILOBARS. FOR SHOCKS IN THE (100)
DIRECTION AND AT 220. Kbars IN THE (111) DIRECTION.
5) FURTHER WORK IS IN PROGRESS.
6) THE VALUE OF VD1 WAS OBTAINED FROM A CATION TO ANION DISTANCE OF
2.840 A. SEE A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC
ASSOCIATION, POLYCRYSTAL BOOK SERVICE, BROOKLYN 1953) 2ND ED.

TABLE I

SODIUM CHLORIDE
99-10---2



99-10---3
SODIUM CHLORIDE

NA-CL SINGLE CRYSTAL

100 AXIS

$V_0 = 0.464 \text{ CC}/\text{O}$ $C_L = 4.75 \text{ KM}/\text{SEC}$ $C_D = 3.42 \text{ KM}/\text{SEC}$
 $C_S = 2.40 \text{ KM}/\text{SEC}$

111 AXIS

$V_0 = 0.463 \text{ CC}/\text{O}$ $C_L = 4.42 \text{ KM}/\text{SEC}$ $C_D = 3.42 \text{ KM}/\text{SEC}$
 $C_S = 2.72 \text{ KM}/\text{SEC}$
 $V_{OI} = 0.4622 \text{ CC}/\text{O}$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICROSEC,
AND PRESSURE IN KILOBARS.

TABLE

AXIS	RHO0	US	UFS	UP	P	V/V0	PRESSURE IN AL BASE PLATE
100	2.159	5.94	3.45	1.73	222	0.710	294
100	2.160	5.07	2.22	1.10	120	0.783	162
100	2.154	6.06	3.80	1.86	243	0.693	320
100	2.163	6.24	-	1.97	266	0.684	368
100	2.153	9.03	9.40	4.07	791	0.549	1050
100	2.152	7.72	6.22	3.21	533	0.584	684
100	2.158	6.24	4.08	2.05	277	0.671	368
100	2.157	8.47	8.12	3.77	689	0.555	877
100	2.156	6.34	4.55	2.28	313	0.640	419
100	2.156	6.71	5.34	2.69	389	0.599	519
100	2.157	8.16	7.36	3.42	602	0.581	764
100	2.155	9.05	8.77	4.02	784	0.556	986
100	2.147	6.36	4.89	2.33	318	0.634	427
100	2.141	7.83	6.38	3.19	535	0.593	680
111	2.148	5.88	3.75	1.88	238	0.680	320
111	2.157	5.98	4.07	2.01	260	0.664	351
111	2.163	6.00	-	2.00	259	0.667	348
111	2.153	6.04	4.34	2.09	272	0.654	368
111	2.158	8.76	8.29	3.74	609	0.568	877
111	2.164	6.29	4.58	2.27	308	0.637	419
111	2.161	6.77	5.42	2.60	392	0.604	519
111	2.157	8.11	7.49	3.43	600	0.577	764
111	2.162	9.08	8.72	4.01	787	0.558	986
UNKNOWN	2.165	5.86	-	1.76	223	0.700	298
UNKNOWN	2.151	9.00	9.62	4.15	803	0.539	1022
UNKNOWN	2.153	7.22	6.36	3.01	468	0.583	616
UNKNOWN	2.153	6.45	5.14	2.51	349	0.611	469
UNKNOWN	2.159	8.62	8.19	3.73	604	0.567	874
UNKNOWN	2.155	7.07	5.81	2.80	427	0.604	558

SODIUM CHLORIDE

AXIS	RHO0	US	UFS	UP	P	V/V0	PRESSURE IN
UNKNOWN	2.157	7.10	5.58	2.79	427	0.607	559
US = 3.608 ± 1.334•UP KM/SEC (FOR 100 AXIS)							
SIGMA US = 0.027 FROM UP = 1.10 TO 1.97 KM/SEC							
US = 3.150 ± 1.446•UP KM/SEC (FOR 100 AXIS)							
SIGMA US = 0.098 FROM UP = 3.20 TO 4.07 KM/SEC							
US = 3.635 ± 1.184•UP KM/SEC (FOR 111 AXIS)							
SIGMA US = 0.032 FROM UP = 2.00 TO 2.68 KM/SEC							
US = 2.375 ± 1.675•UP KM/SEC (FOR 111 AXIS)							
SIGMA US = 0.028 FROM UP = 3.74 TO 4.01 KM/SEC							
US = 3.170 ± 1.357•UP KM/SEC (FOR 100, 111 AND UNKNOWN AXIS)							
SIGMA US = 0.098 FROM UP = 2.25 TO 3.01 KM/SEC							
US = 3.234 ± 1.428•UP KM/SEC (FOR 100, 111 AND UNKNOWN AXIS)							
SIGMA US = 0.101 FROM UP = 3.19 TO 4.15 KM/SEC							

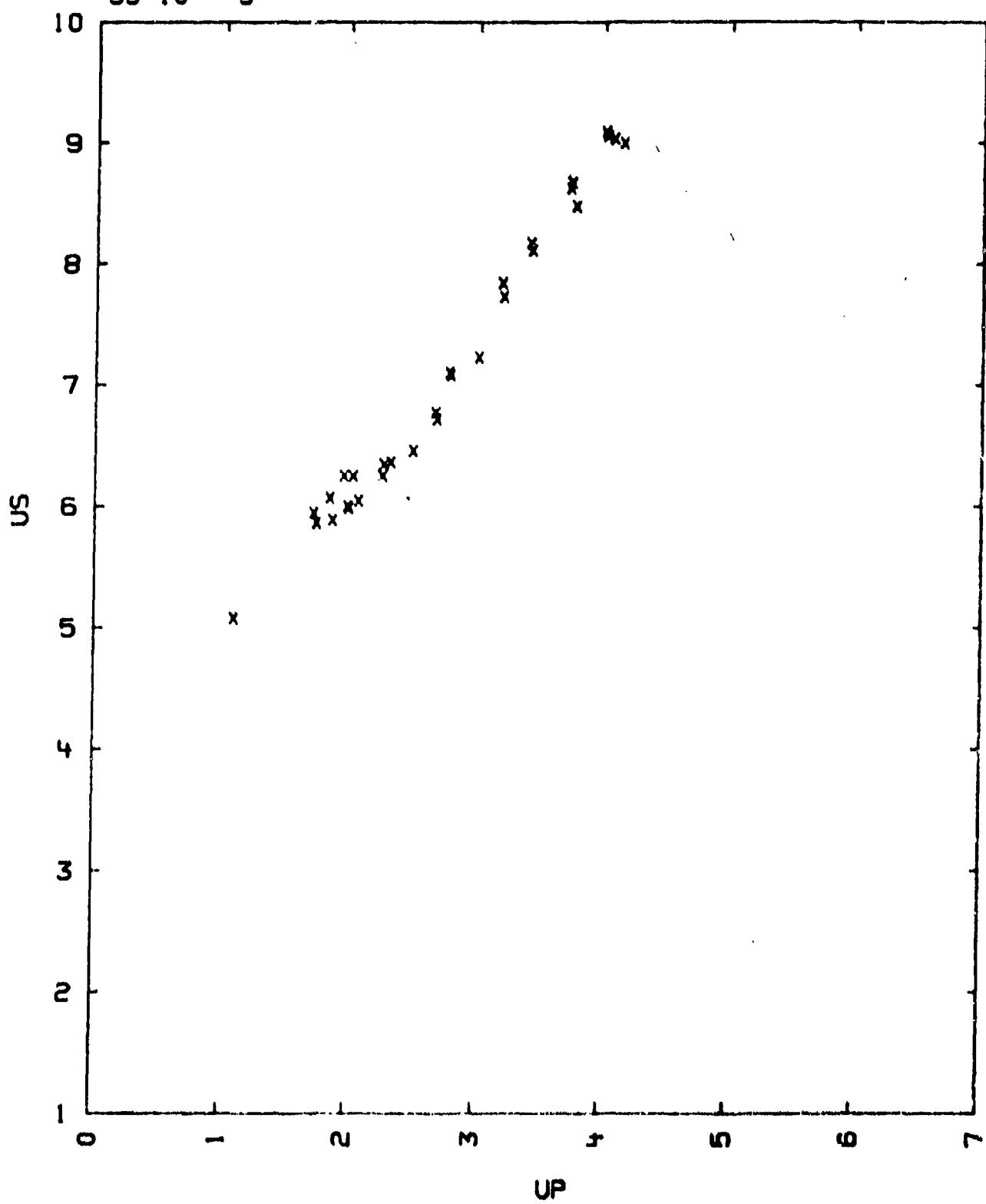
COMMENTS:

- 1) SOURCE: COMPILER
 L. R. L. EQUATION OF STATE FILE
 LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA
- 2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)
 DATA REDUCTION TECHNIQUE B.
- 3) PART OF THE TABULATED DATA ALSO REPORTED BY CHRISTIAN, R. H., IN
 EQUATION OF STATE OF ALKALI HALIDES AT HIGH PRESSURE (THESIS)
 UCRL-4900 MAY 16, 1957 UNIVERSITY OF CALIFORNIA,
 LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.
- 4) A TRANSITION IS OBSERVED AROUND 220 KILOBARS FOR Na-Cl WITH 111 AXIS
 OF ORIENTATION AND AROUND 270 KILOBARS FOR CRYSTALS WITH 100 AXIS OF
 ORIENTATION.
- 5) A STIFFENING OF THE MUGONIOT CAN BE OBSERVED BETWEEN
 468 AND 535 KILOBARS.
- 6) ALSO LISTED IN REFERENCE OF COMMENT 3 ARE:
 DEBYE TEMPERATURE 281 DEG. K
 HEAT CAPACITY (CV) 0.83 J/0/DEG.
 EXPANSION COEFFICIENT 0.000119 PER DEG.
 COMPRESSIBILITY 4.08 PER NEGABAR
 MELTING POINT 808 DEG. C
- 7) THE VALUE OF V01 WAS OBTAINED FROM A LATTICE CONSTANT OF 5.64009 A
 A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
 POLYCRYSTAL BOOK SERVICE 1963) 2ND EDITION.
- 8) SOUND VELOCITIES WERE MEASURED BY H.L. DUNEGAN (SUPPORT ENGINEERING,
 ULTRASONIC GROUP) LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIF.

008/14/77

TABLE I

SODIUM CHLORIDE
99-10---3



99-10---4
SODIUM CHLORIDE

Na-Cl Pressed

$V_0 = 0.466 \text{ CC}/\text{O}$ $C_L = 4.50-4.59 \text{ MM}/\text{SEC}$ $C_O = 3.54 \text{ MM}/\text{SEC}$
 $V_{OI} = 0.4622 \text{ CC}/\text{O}$ $C_S = 2.47 \text{ MM}/\text{SEC}$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN MM/MICROSEC., AND PRESSURE IN KILOGARS.

TABLE

RHO	US	UFS	UP	P	V/V _O	PRESSURE IN AL BASE PLATE
2.135	5.86	3.56	1.78	222	0.698	298
2.146	6.07	4.04	1.99	258	0.672	351
2.145	6.12	3.99	1.98	260	0.677	345
2.145	5.45	2.88	1.39	162	0.750	220
2.151	5.94	3.51	1.74	223	0.707	294
2.138	5.00	2.25	1.11	118	0.779	162
2.142	5.89	-	1.88	237	0.681	320
2.140	4.18	1.14	0.54	48	0.871	69
2.143	5.02	2.34	1.17	126	0.767	173
2.142	5.38	2.82	1.39	160	0.741	218
2.131	5.86	3.40	1.70	212	0.710	283
2.148	8.73	0.28	3.71	696	0.575	870
2.146	6.52	5.19	2.50	350	0.617	469
2.149	6.14	4.14	2.06	273	0.665	388
2.149	8.60	8.23	3.78	693	0.564	870
2.150	6.34	4.65	2.28	312	0.640	419
2.150	8.15	7.22	3.43	601	0.579	764
2.150	8.99	8.44	4.03	779	0.552	986
2.152	8.73	-	3.74	703	0.572	880
2.150	8.57	7.59	3.76	693	0.561	860
2.149	8.70	-	3.74	699	0.570	880
2.151	5.10	2.33	1.11	122	0.782	165
2.153	5.08	2.27	1.10	120	0.783	163
2.150	6.00	3.47	1.77	229	0.704	301
2.152	5.96	3.40	1.66	214	0.721	281
2.153	5.12	2.17	1.07	116	0.787	159
2.150	4.08	2.24	1.15	122	0.760	172
2.152	4.92	2.26	1.01	107	0.795	148

$US = 3.426 + 1.439 UP \text{ MM}/\text{MICROSEC}$ FROM UP = 1.00 TO 1.80 MM/MICROSEC
 $\Sigma \text{SIGMA } US = 0.079$

$US = 3.515 + 1.371 UP \text{ MM}/\text{MICROSEC}$ FROM UP = 3.70 TO 4.03 MM/MICROSEC
 $\Sigma \text{SIGMA } US = 0.098$

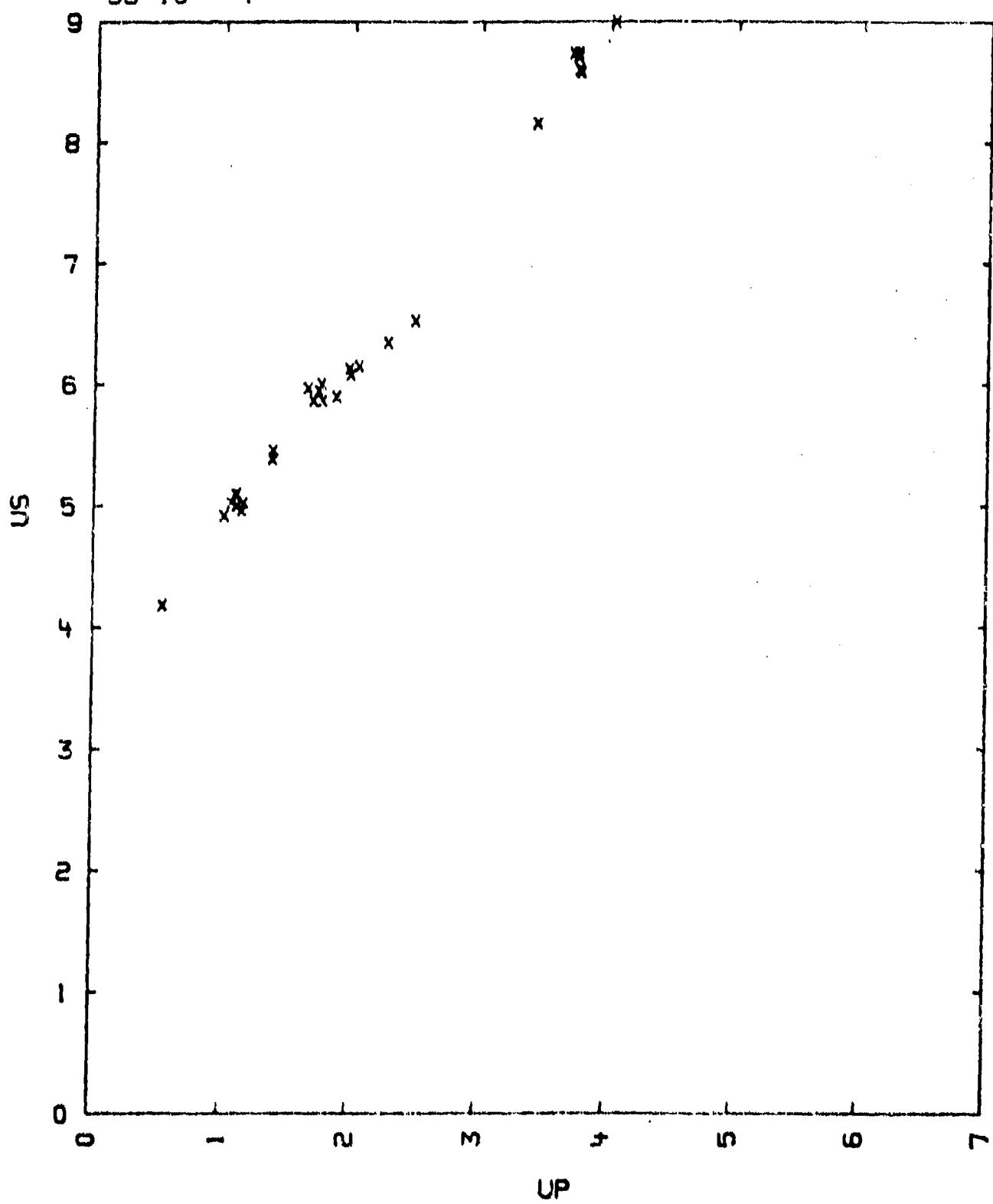
COMMENTS:

- 1) SOURCE: COMPILER
L. R. L. EQUATION OF STATE FILE
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA
- 2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)
DATA REDUCTION TECHNIQUE B.
- 3) THE HUGONIOT FOR PRESSED NA-CL IS CONSISTENT WITH THE SINGLE CRYSTAL HUGONIOT.
- 4) THE TRANSITION BETWEEN 220 AND 270 KILOBARS OBSERVED FOR SINGLE CRYSTAL NA-CL IS LESS PRONOUNCED FOR PRESSED NA-CL.
- 5) THE VALUE OF VOI WAS OBTAINED FROM A LATTICE CONSTANT OF 5.84008 A
A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE 1963) 2ND EDITION.
- 6) SOUND VELOCITIES WERE MEASURED BY H.L. DUNEGAN (SUPPORT ENGINEERING,
ULTRASONIC GROUP) LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIF.

UOG/14/77

TABLE I

SODIUM CHLORIDE
99-10---4



99-10---5
SODIUM CHLORIDE

NA-CL

$$V_0 = 0.4619 \text{ CC}/\text{O}$$

$$V_{01} = 0.4622 \text{ CC}/\text{O}$$

IN THE TABLES BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN KM/SEC., AND PRESSURE IN KILOBARS. ST DESIGNATES THE STANDARD MATERIAL AND UP(ST) IS THE PARTICLE VELOCITY OF THE STANDARD.

TABLE I
SINGLE CRYSTAL

RHO0	US	UP	P	V/V0	ST	UP(ST)
2.165	6.27	2.04	276	0.676	AL	1.72
-	10.39	5.19	1170	0.500	FE	3.60
-	10.75	5.55	1290	0.483	FE	3.85
-	11.61	5.95	1480	0.408	FE	4.16
-	12.14	6.32	1710	0.483	FE	4.56
-	11.84	6.80	1740	0.425	AL	6.03
-	12.96	7.83	2200	0.395	FE	5.44
-	16.84	11.05	4030	0.344	AL	9.95

US = $3.56 + 1.321 \text{ UP KM/SEC.}$ FOR US FROM 6.0 TO 12.0 KM/SEC.
 $\Sigma \text{OMA US} = 0.14 \text{ KM/SEC.}$

US = $3.75 + 1.103 \text{ UP KM/SEC.}$ FOR US FROM 12.0 TO 16.8 KM/SEC.
 $\Sigma \text{OMA US} = 0.07 \text{ KM/SEC.}$

$$V_0 = 0.899-1.009 \text{ CC}/\text{O}.$$

TABLE II
PURCOS

RHO0	US	UP	P	V/V0	ST	UP(ST)
1.430	4.95	2.29	162	0.539	AL	1.60
-	7.27	3.81	397	0.475	FE	2.37
-	8.72	4.66	568	0.452	AL	3.54
-	9.06	4.97	645	0.451	FE	3.15
-	9.93	5.86	804	0.430	FE	3.60
-	10.19	6.00	874	0.413	AL	4.65
-	10.47	6.11	915	0.417	AL	4.76
0.991	4.45	2.53	112	0.431	AL	1.60
-	6.68	4.06	268	0.392	FE	2.37
-	8.33	5.12	424	0.385	AL	3.54
0.991	8.54	5.30	449	0.379	FE	3.15
-	9.54	6.02	570	0.369	FE	3.60
-	10.08	6.60	659	0.348	AL	4.65
-	10.49	6.70	695	0.362	AL	4.76

US = $0.605 + 1.939 \text{ UP} - 0.0393 \text{ UP}^{1/2} \text{ KM/SEC.}$ FOR RHO0 = 1.430 G/CC.

SODIUM CHLORIDE

RHOO US UP P V/VO ST UP(ST)

FOR US BETWEEN 5.0 AND 10.5 KM/SEC. SIGMA US = 0.08 KM/SEC.

US = $0.191 + 1.768 \cdot UP - 0.0370 \cdot UP^{+2}$ KM/SEC. FOR RHOO = 0.891 G/CC.
FOR US BETWEEN 4.5 AND 10.5 KM/SEC. SIGMA = 0.12 KM/SEC.

COMMENTS:

- 1) SOURCE: KORMER, S. B., SINITSYN, M. V., FUNTIKOV, A. I., URLIN, V. O. AND BLINOV, A. V.
SOVIET PHYS-JETP, VOL. 20, P. 811 (1965)
J. EXPTL. THEORET. PHYS. (U.S.S.R.) VOL. 47, P. 1202 (1964)
- 2) EXPERIMENTAL TECHNIQUE A
DATA REDUCTION TECHNIQUE B
- 3) VOI WAS OBTAINED FROM A CATION TO ANION DISTANCE OF 2.920 ANGSTROMS.
SEE A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE, BROOKLYN 1963) 2ND ED.
- 4) THE MEASURED EXPERIMENTAL ERROR IN THE SHOCK VELOCITY BELOW 10 KM/SEC
IS 1 PERCENT OR LESS AND FOR THE HIGHER VALUES THE ERROR IS
APPROXIMATELY 2 PER CENT. THE VALUE OF THE SHOCK VELOCITY WAS
DETERMINED FROM 5-8 EXPERIMENTS.
- 5) ADDITIONAL CONSTANTS LISTED:
HEAT CAPACITY = 0.8935 JOULES/G/DEG.
DANO GAP = 7.7 EV.
- 6) THE ALUMINUM STANDARD HUGONIOT IS CHARACTERIZED BY THE FOLLOWING
RELATIONSHIP: $US = 5.254 + 1.458 \cdot UP - 0.0276 \cdot UP^{+2} + 0.00103 \cdot UP^{+3}$
SIGMA US = 0.013 KM/SEC. FOR UP = 0 TO 10.5 KM/SEC
RHOO = 2.71 G/CC.

TABLE I

SODIUM CHLORIDE
99-10---5

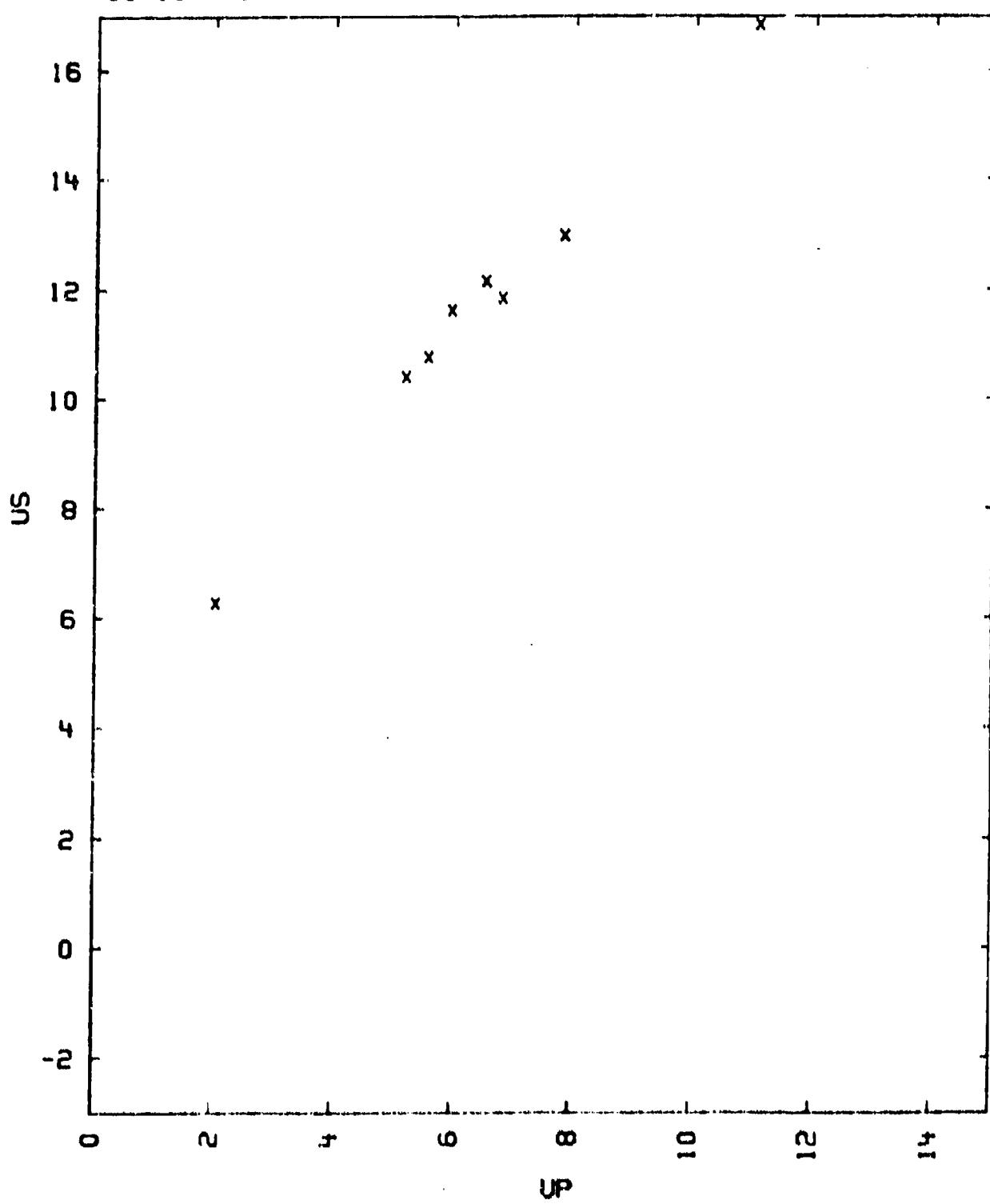
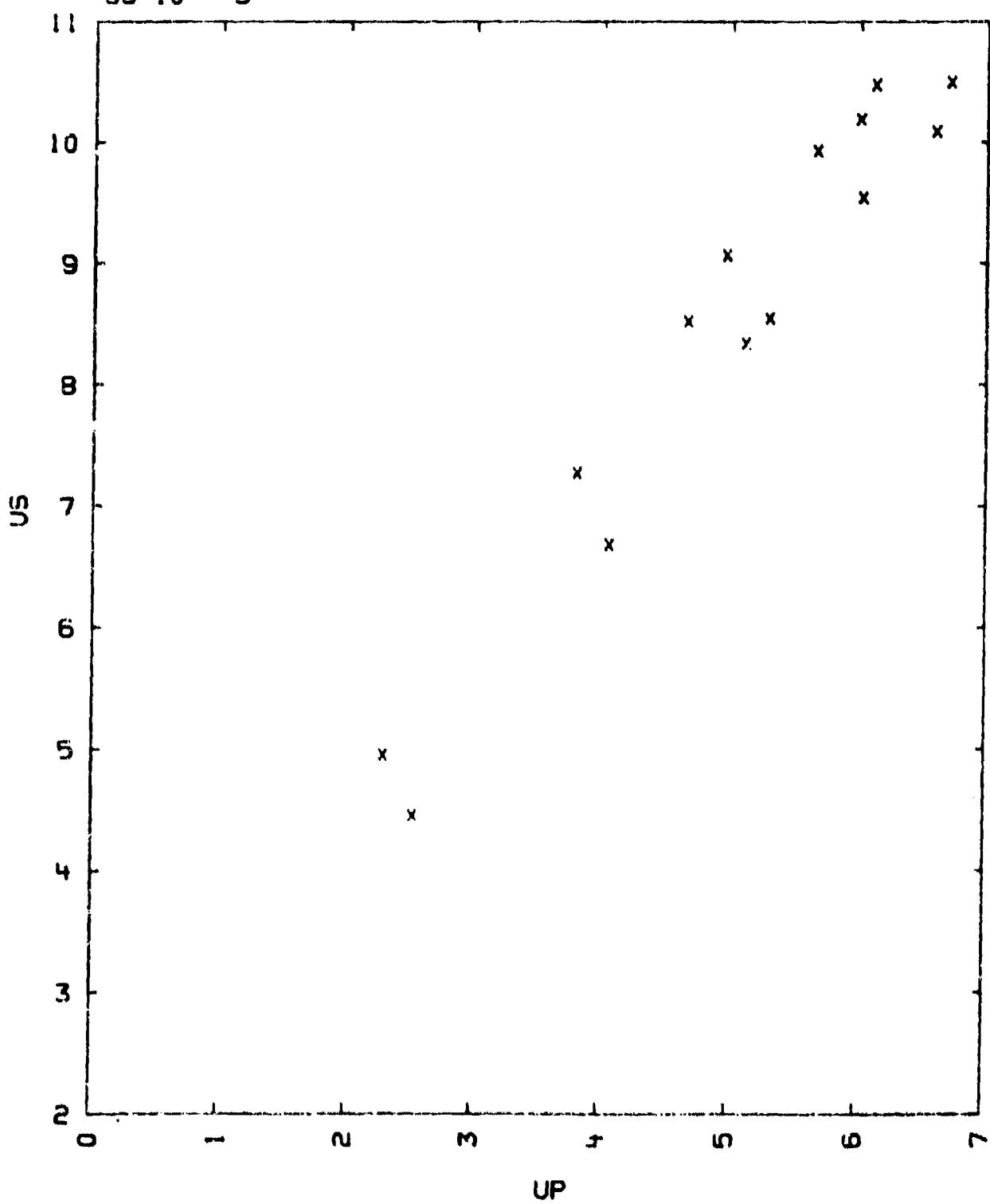


TABLE II

SODIUM CHLORIDE
99-10---5

99-11---1
SODIUM BROMIDE

NA-BR PRESSED

$$V_0 = 0.316 \text{ CC/G}$$

$$V_{01} = 0.3118 \text{ CC/G}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICROSEC,
AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UFS	UP	P	V/V0	PRESSURE IN AL BASE PLATE
3.165	3.38	1.13	0.55	59	0.838	75
3.177	3.34	1.08	0.54	57	0.839	73
3.16	4.00	2.07	1.06	133	0.736	165
3.160	4.29	2.61	1.30	177	0.697	215
3.165	4.38	2.73	1.36	189	0.689	230
3.152	4.79	3.30	1.63	247	0.659	293
3.145	5.10	-	1.83	293	0.641	345
3.158	5.06	3.80	1.85	295	0.635	345
3.17	5.10	3.69	1.89	305	0.630	356

$$US = 2.620 + 1.321 UP \text{ MM/MICROSEC}$$

$$\text{SIGMA US} = 0.037$$

COMMENTS:

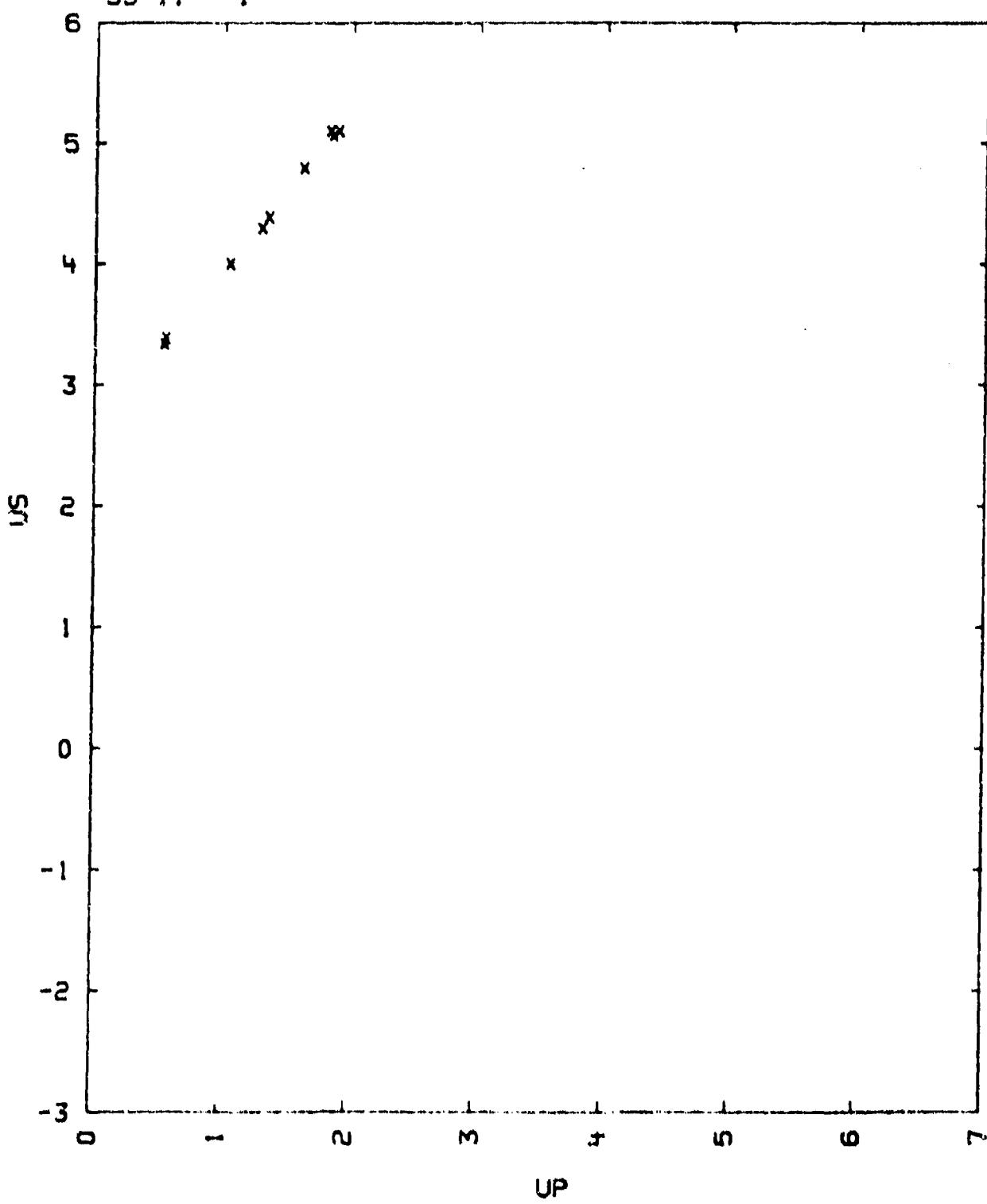
- 1) SOURCE: COMPILER
L. R. L. EQUATION OF STATE FILE
LAURENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA
- 2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)
DATA REDUCTION TECHNIQUE B.
- 3) TABULATED DATA ALSO REPORTED BY CHRISTIAN, R.H., IN
EQUATION OF STATE OF ALKALI HALIDES AT HIGH PRESSURE (THESIS)
UCRL-4900 MAY 16, 1957 UNIVERSITY OF CALIFORNIA,
LAURENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.
- 4) ALSO LISTED IN REFERENCE OF COMMENT 3 ARE:

DEBYE TEMPERATURE	200 DEG. K
HEAT CAPACITY (CV)	0.47 J/G/DEG.
EXPANSION COEFFICIENT	0.000120 PER DEG.
COMPRESSIBILITY	5.08 PER MEGABAR
MELTING POINT	750 DEG. C
- 5) THE VALUE OF V01 WAS OBTAINED FROM A LATTICE CONSTANT OF 5.97299 A
A.C.A. MONOGRAPH NUMBER 5 'AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE 1963' 2ND EDITION.

1406/14/77

TABLE I

SODIUM BROMIDE
99-11---1



99-12---1
SODIUM IODIDE

NA-1

$$V_0 = 0.272 \text{ CC/0}$$

$$V_{01} = 0.2727 \text{ CC/0}$$

$$C_B = 1.96 \text{ KM/SEC}$$

IN THE TABLE BELOW DENSITY IS GIVEN IN G/CC, VELOCITY IN KM/SEC AND PRESSURE IN KILOBARS. SH DESIGNATES SAMPLE HOLDER.

TABLE

RHO0	US	UP	P	V/V0	SH	UP(SH)
3.67	2.95	0.57	62.0	0.8064	CU	0.37
-	4.81	1.82	321.0	0.6215	AL	1.71
-	6.14	2.94	661.0	0.5208	AL	2.82
-	7.24	3.80	1009.0	0.4750	FE	2.80

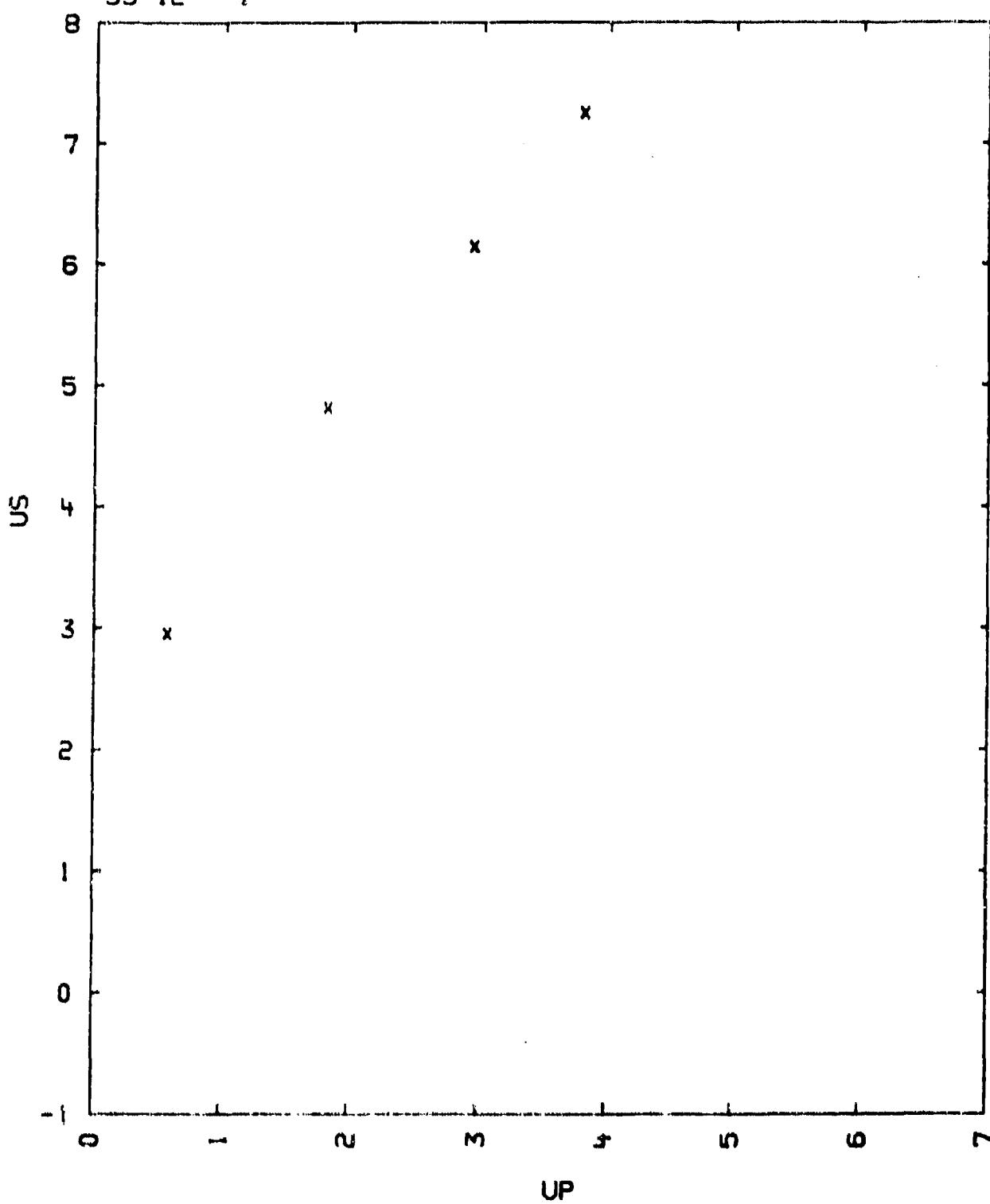
US = $2.09 + 1.576 UP - 0.0597 UP^{0.2}$ KM/SEC
FOR UP FROM 0.5 TO 3.8 KM/SEC
S10 US = 0.063 KM/SEC

COMMENTS:

- 1) SOURCE: AL'TSHULER, L.V., PAVLOSKI, M.M., KULESHOVA, L.V., AND SIMAKOV, O.V.
SOVIET PHYS.-SOLID STATE, VOL. 5, P. 203 (1963)
- 2) EXPERIMENTAL TECHNIQUE A
DATA REDUCTION TECHNIQUE B.
- 3) THE SAMPLES WERE POSITIONED ON PLATES OF CU AL AND FE AS INDICATED IN TABLE COLUMN 6.
THE HUGONIOTS OF FE CU AND AL WERE OBTAINED FROM
AL'TSHULER, L.V., KORMER, S.B., BAKANOVA, A.A. AND TRUNIN, R.F.
JETP VOL 11, P.573 (1960)
- 4) THE AL AND CU ADIABAT WERE OBTAINED BY REFLECTING THE HUGONIOT IN THE
P VS UP PLANE. CORRECTIONS WERE MADE FOR FE.
- 5) OTHER CONSTANTS LISTED ARE: DEBYE TEMPERATURE 140 DEG. K
HEAT CAPACITY (CV) 0.325 J/G/DEG.
CATION TO ANION DISTANCE 3.231 KX
EXPANSION COEFFICIENT 0.000135 PER DEG
- 6) THE VALUE OF V01 WAS OBTAINED FROM A CATION TO ANION DISTANCE OF
3.2375 A. A.C. A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC
ASSN., POLYCRYSTAL BOOK SERVICE, BROOKLYN 1963) 2ND ED.

TABLE I

SODIUM IODIDE
99-12---1



99-12--2
SODIUM IODIDE

NA-1 SINGLE CRYSTAL

$$V_0 = 0.275 \text{ CC}/\text{O}$$

$$V_{OI} = 0.2727 \text{ CC}/\text{O}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICROSEC, AND PRESSURE IN KILOGARS.

TABLE

RHO0	US	UFS	UP	P	V/V0	PRESSURE IN AL BASE PLATE
3.638	3.58	2.12	1.02	134	0.714	162
3.640	4.03	2.70	1.35	200	0.865	253
3.630	4.39	3.35	1.61	259	0.634	297
3.623	4.58	-	1.66	310	0.593	358

$$US = 2.370 + 1.216 UP \text{ MM/MICROSEC}$$

$$\text{SIGMA US} = 0.062$$

COMMENTS:

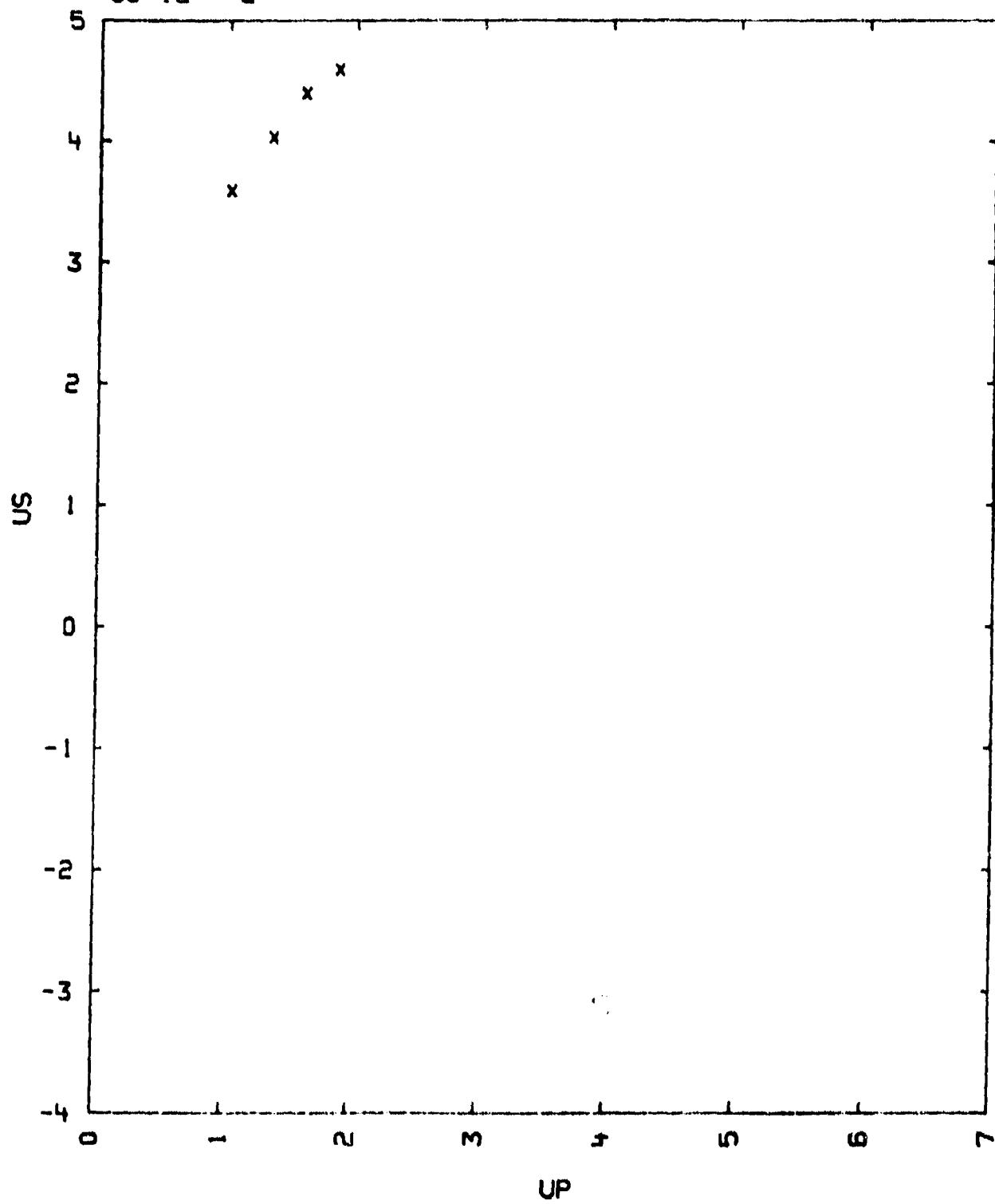
- 1) SOURCE: COMPILER
L. R. L. EQUATION OF STATE FILE
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA
- 2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)
DATA REDUCTION TECHNIQUE B.
- 3) TABULATED DATA ALSO REPORTED BY CHRISTIAN, R.H., IN
EQUATION OF STATE OF ALKALI HALIDES AT HIGH PRESSURE (THESIS)
UCRL-4900 MAY 16, 1957 UNIVERSITY OF CALIFORNIA,
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.
- 4) ALSO LISTED IN REFERENCE OF COMMENT 3 ARE:

DEBYE TEMPERATURE	151 DEG. K
HEAT CAPACITY (CV)	0.33 J/G/DEG.
EXPANSION COEFFICIENT	0.000135 PER DEG.
COMPRESSIBILITY	7.07 PER MEGABAR
MELTING POINT	662 DEG. C
- 5) THE VALUE OF VOI HAS OBTAINED FROM A LATTICE CONSTANT OF 6.475 A
A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE 1963) 2ND EDITION.

TABLE I

SODIUM IODIDE

99-12---2



99-29-24-1---1

JADEITE, BURMA (SODIUM ALUMINUM SILICATE) (SILICATE ROCK)

NA-AL-S12-06

ABOUT 100 VOLUME PERCENT

$$V_0 = 0.300 \text{ CC/G}$$

$$V_{01} = 0.299 \text{ CC/G}$$

$$CL = 8.68 \text{ KM/SEC}$$

$$CO = 6.42 \text{ KM/SEC}$$

THE TABLE LISTS SHOCK AND PARTICLE VELOCITY IN KM/SEC., PRESSURE IN KBARS AND DENSITY IN G/CC. ST DESIGNATES THE SAMPLE HOLDER AND STANDARD MATERIAL.

TABLE

RHO0	US	UP	P	V/V0	US(ST)
3.33	7.84	1.03	269	0.869	6.95
3.33	7.78	1.05	271	0.865	6.97
3.33	7.08	1.19	313	0.847	7.18
3.33	8.22	1.48	401	0.822	7.58
3.33	8.25	1.48	406	0.820	7.60
3.33	8.20	1.51	413	0.814	7.64
3.33	8.80	1.91	560	0.782	8.23
3.33	8.78	1.99	583	0.773	8.33
3.33	9.07	2.31	598	0.745	8.77
3.33	9.05	2.32	701	0.742	8.78
3.34	9.33	2.81	874	0.700	9.42
3.33	9.39	3.02	944	0.678	9.68
3.33	9.42	3.05	959	0.675	9.73
3.35	9.72	3.34	1086	0.657	10.13
3.34	9.83	3.50	1147	0.645	10.33

$$US = 6.54 + 1.124 \cdot UP \text{ KM/SEC. FOR UP LESS THAN 2.4 KM/SEC}$$

$$\text{SIGMA US} = 0.088 \text{ KM/SEC.}$$

$$US = 6.56 + 0.939 \cdot UP \text{ FOR UP GREATER THAN 3.0 KM/SEC}$$

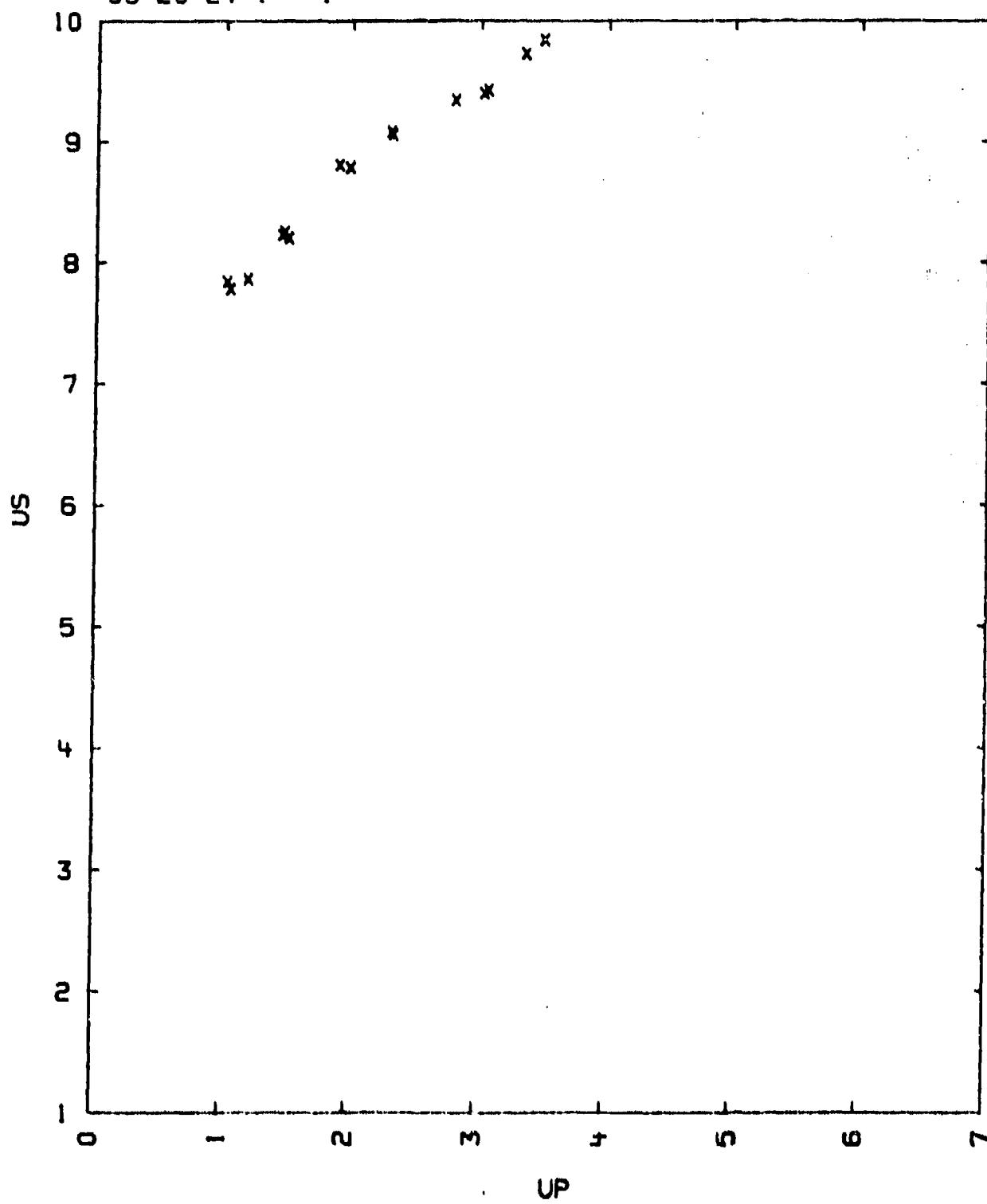
$$\text{SIGMA US} = 0.021 \text{ KM/SEC}$$

COMMENTS :

- 1) SOURCE: MCQUEEN R.G. AND MARSH S.P.
PRIVATE COMMUNICATION
LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION METHOD B STANDARD MATERIAL 2024 ALUMINUM
- 3) VOI WAS OBTAINED FROM THE LATTICE PARAMETERS LISTED IN CRYSTAL DATA DETERMINATIVE TABLES (AMERICAN CRYST. ASSN., 1963)
- 4) SAMPLE OBTAINED THROUGH F. BIRCH. CL FROM F. BIRCH, J. GEOPHYS. RES., VOL 65, P. 1083 (1960)
- 5) FURTHER WORK IN PROGRESS

TABLE I

JADEITE, BURMA (SODIUM ALUMINUM SILICATE) (SILICA
99-29-24-1---1



100-9---1
POTASSIUM FLUORIDE

K-F PRESSED

$$V_0 = 0.401 \text{ CC/G}$$

$$V_{01} = 0.3955 \text{ CC/G}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICROSEC,
AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UFS	UP	P	V/V0	PRESSURE IN AL BASE PLATE
2.483	4.23	-	1.11	117	0.738	162
2.484	4.69	2.84	1.43	168	0.695	225
2.482	5.24	3.55	1.78	232	0.661	304
2.474	6.77	5.40	2.69	450	0.602	553
2.50	4.70	2.78	1.44	169	0.694	228
2.535	4.20	2.27	1.17	124	0.721	171
2.469	3.91	1.88	0.97	94	0.752	136

$$US = 2.324 + 1.650 UP \text{ MM/MICROSEC}$$

$$\text{SIGMA US} = 0.043$$

COMMENTS:

1) SOURCE: COMPILER

L. R. L. EQUATION OF STATE FILE

LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA

2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)

DATA REDUCTION TECHNIQUE B.

3) PART OF THE TABULATED DATA ALSO REPORTED BY CHRISTIAN, R. H., IN
EQUATION OF STATE OF ALKALI HALIDES AT HIGH PRESSURE (THESIS)
UCRL-4900 MAY 16, 1957 UNIVERSITY OF CALIFORNIA,
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.

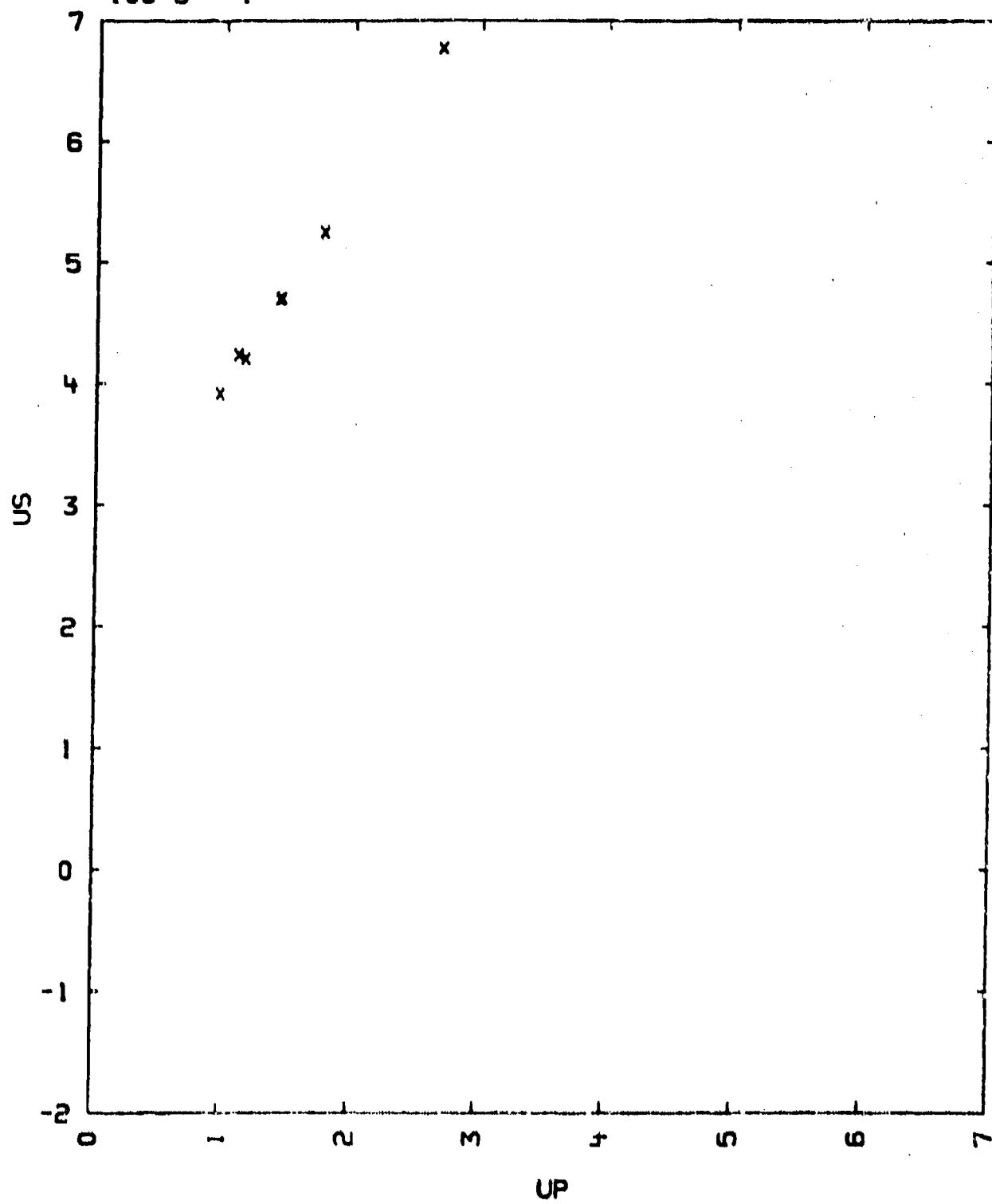
4) ALSO LISTED IN REFERENCE OF COMMENT 3 ARE:

DEBYE TEMPERATURE	321 DEG. K
HEAT CAPACITY (CV)	0.81 J/G/DEG.
EXPANSION COEFFICIENT	0.000100 PER DEG.
COMPRESSIBILITY	3.51 PER MEGABAR
MELTING POINT	856 DEG. C

5) THE VALUE OF V01 WAS OBTAINED FROM A LATTICE CONSTANT OF 3.344 A
A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE 1963) 2ND EDITION.

TABLE I

POTASSIUM FLUORIDE
100-9---1



100-10---1
POTASSIUM CHLORIDE

K-CL

$$V_0 = 0.502 \text{ CC}/\text{O}$$

$$V_{01} = 0.5033 \text{ CC}/\text{O}$$

$$C_B = 3.02 \text{ KM}/\text{SEC}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS. SH DESIGNATES SAMPLE HOLDER.

TABLE

RHO0	US	UP	P	V/V0	SH	UP(SH)
1.99	3.67	0.28	20.0	0.9242	CU	0.17
-	3.63	0.30	41.8	0.8403	CU	0.35
-	3.61	0.38	70.5	0.7299	AL	0.69
-	4.40	1.51	132.0	0.6570	AL	1.14
-	5.21	1.91	198.0	0.6341	AL	1.50
-	5.39	2.20	244.5	0.6064	AL	1.74
-	7.50	3.40	508.0	0.5464	AL	2.82
-	8.56	4.22	716.0	0.5078	FE	2.80

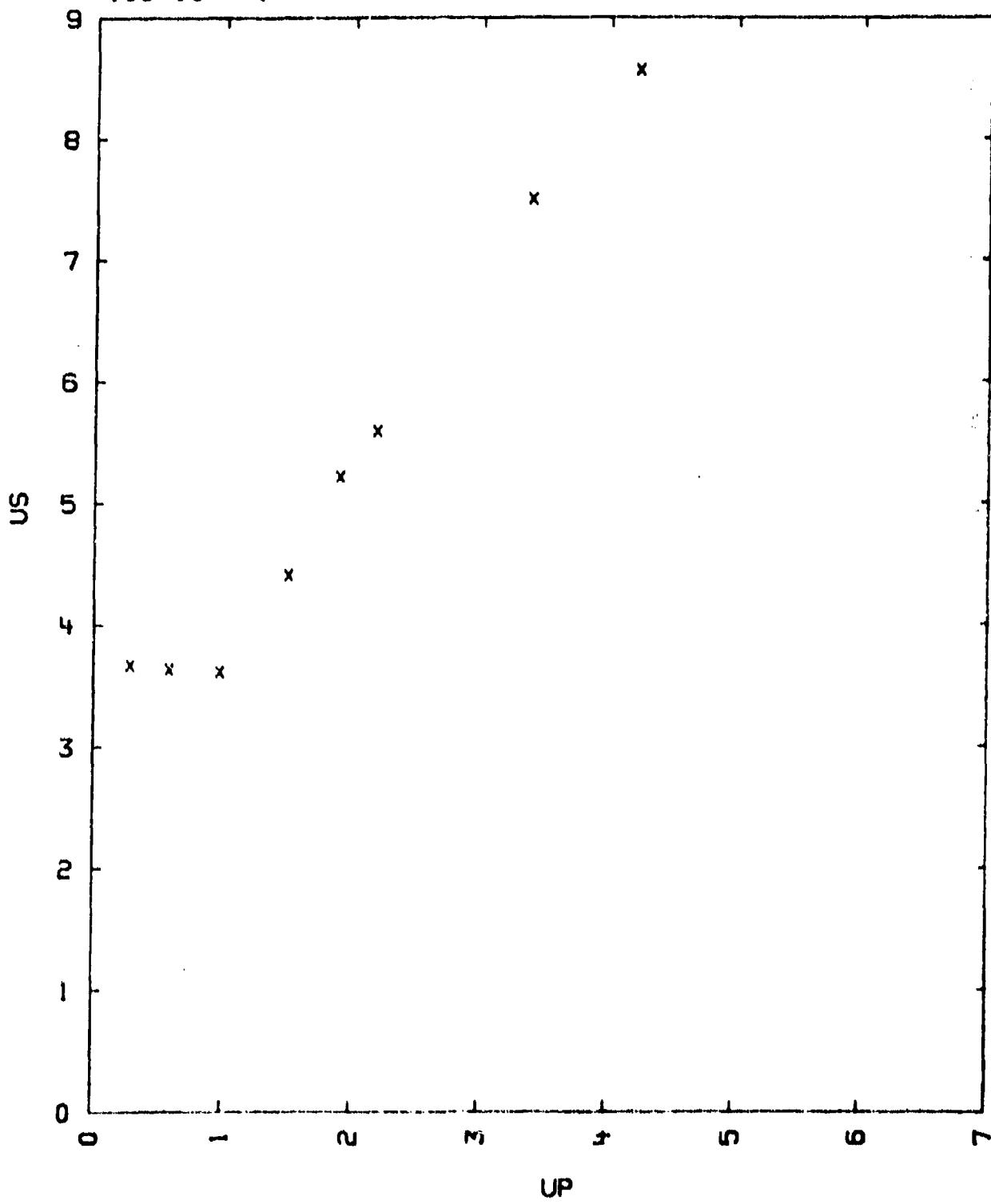
US = 2.15 + 1.54 UP KM/SEC FOR UP BETWEEN 1.0 AND 4.2 KM/SEC
 $SIG US = 0.1$

COMMENTS:

- 1) SOURCE: AL'TSHULER, L.V., PAVLOVSKII, M.M., KULESHOVA, I.V., AND SIMAKOV, O.V.
SOVIET PHYS.-SOLID STATE, VOL. 5, P. 203 (1963)
- 2) EXPERIMENTAL TECHNIQUE A
DATA REDUCTION TECHNIQUE B
- 3) THE SAMPLES WERE POSITIONED ON PLATES OF CU AL AND FE AS INDICATED IN TABLE COLUMN G.
THE MUONIOTS OF FE CU AND AL WERE OBTAINED FROM
AL'TSHULER, L.V., KORMER, S.B., BAKANOVA, A.A. AND TRUNIN, R.F.
JETP VOL 11, P.573 (1960)
- 4) THE AL AND CU ADIABAT WERE OBTAINED BY REFLECTING THE MUONIOT IN THE
P VS UP PLANE. CORRECTIONS WERE MADE FOR IT.
- 5) OTHER CONSTANTS LISTED ARE: DEBYE TEMPERATURE 227 DEG. K
HEAT CAPACITY (CV) 0.862 J/G/DEG.
CATION TO ANION DISTANCE 3.14 KX
EXPANSION COEFFICIENT 0.000100 PER DEG
- 6) POINTS WITH UP = 0.30 OR LESS CORRESPOND TO A MULTIPLE SHOCK WAVE OF
WHICH ONLY THE FIRST WAVE WAS OBSERVED.
- 7) THE VALUE OF V01 LISTED HAS OBTAINED FROM A CATION TO ANION DISTANCE
OF 3.1454 A. A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC
ASSN., POLYCRYSTAL BOOK SERVICE, BROOKLYN 1963) 2ND ED.

TABLE I

POTASSIUM CHLORIDE
100-10---1



K-CL

VC (SINGLE CRYSTAL) = 0.504 CC/G
VOL = 0.5026 CC/GIN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICROSEC,
AND PRESSURE IN KILOBARS.

TABLE

SAMPLE							STANDARD
RHO0	US	UFS	UP	P	V/V0	FORM	P
1.982	4.04	2.36	1.21	97	0.700	CRYSTAL	162
1.984	5.19	3.74	1.88	194	0.636	-	296
1.985	5.54	4.07	2.08	223	0.624	-	344
1.970	4.64	3.08	1.57	144	0.861	PRESSED	230
1.970	5.51	4.24	2.13	232	0.613	-	351
1.953	8.64	9.24	4.34	733	0.498		1022

US = 2.406 + 1.448 UP MM/MICROSEC
SIGMA US = 0.096

COMMENTS:

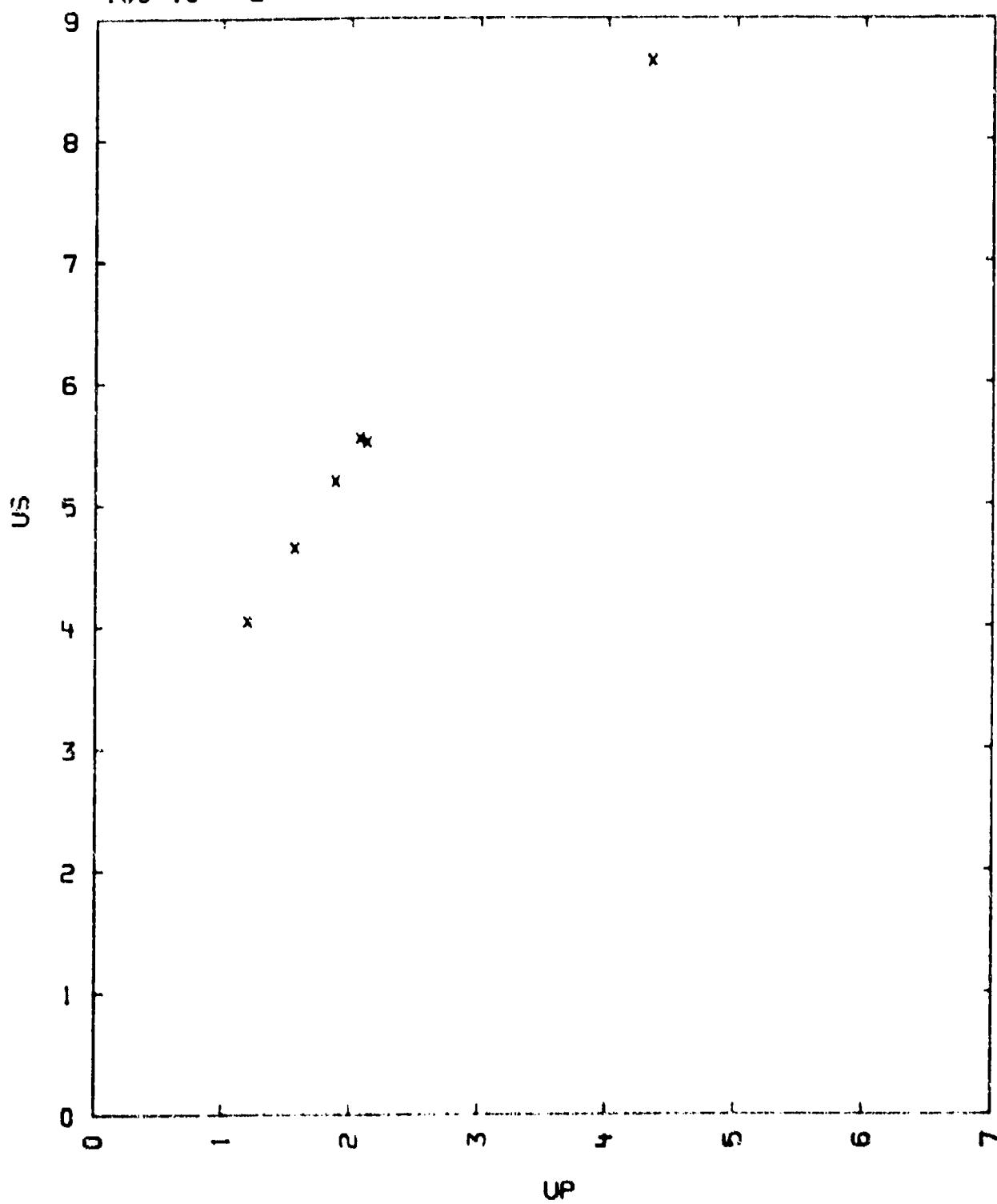
- 1) SOURCE: COMPILER
L. R. L. EQUATION OF STATE FILE
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA
- 2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)
DATA REDUCTION TECHNIQUE B.
- 3) PART OF THE TABULATED DATA ALSO REPORTED BY CHRISTIAN, R. H., IN
EQUATION OF STATE OF ALKALI HALIDES AT HIGH PRESSURE (THESIS)
UCRL-4900 MAY 16, 1957 UNIVERSITY OF CALIFORNIA,
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.
- 4) ALSO LISTED IN REFERENCE OF COMMENT 3 ARE:

DEBYE TEMPERATURE	227 DEG. K
HEAT CAPACITY (CV)	0.65 J/O/DEG.
EXPANSION COEFFICIENT	0.000103 PER DEG.
COMPRESSIBILITY	5.63 PER MEGABAR
MELTING POINT	772 DEG. C
- 5) THE VALUE OF VOL WAS OBTAINED FROM A LATTICE CONSTANT OF 6.29 A
A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL DIKOK SERVICE 1963) PND EDITION.

TABLE I

POTASSIUM CHLORIDE

100-10---2



100-10---3
POTASSIUM CHLORIDE

K-CL

$$V_0 = 0.5020 \text{ CC}/\text{G}$$

$$V_{01} = 0.5033 \text{ CC}/\text{G}$$

IN THE TABLES BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN KM/SEC., AND PRESSURE IN KILOBARS. ST DESIGNATES THE STANDARD MATERIAL AND UP(ST) IS THE PARTICLE VELOCITY OF THE STANDARD.

TABLE I
SINGLE CRYSTAL

RHO0	US	UP	P	V/V0	ST	UP(ST)
1.992	5.62	2.17	240	0.613	AL	1.72
-	9.76	5.35	1040	0.452	FE	3.60
-	9.96	5.74	1140	0.424	FE	3.85
-	10.67	6.16	1310	0.422	FE	4.16
-	10.93	6.10	1330	0.442	FE	4.13
-	11.43	6.71	1530	0.413	FE	4.56
-	11.29	7.10	1600	0.372	AL	6.03
-	12.63	8.02	2020	0.366	FE	5.44
-	16.69	11.38	3790	0.318	AL	9.95

US = 3.60 + 1.142 UP KM/SEC. FOR US FROM 9.7 TO 16.7 KM/SEC.
SIGMA US = 0.25 KM/SEC.

$$V_0 = 0.709 \cdot 1.299 \text{ CC}/\text{G}$$

TABLE II
POROUS

RHO0	US	UP	P	V/V0	ST	UP(ST)
1.41	4.89	2.30	158	0.529	AL	1.60
-	10.34	6.56	958	0.365	FE	4.13
0.794	4.23	2.60	89	0.372	AL	1.60
-	9.95	7.19	566	0.277	FE	4.13

US =

COMMENTS:

- 1) SOURCE: KORMER, S. B., SINITSYN, M. V., FUNKOV, A. I., URLIN, V. D. AND BLINOV, A. V.
SOVIET PHYS-JETP, VOL. 20, P. 811 (1965)
J. EXPTL. THEORET. PHYS. (U.S.S.R.) VOL. 47, P. 1202 (1964)
- 2) EXPERIMENTAL TECHNIQUE A
DATA REDUCTION TECHNIQUE B
- 3) V01 HAS OBTAINED FROM A CATION TO ANION DISTANCE OF 3.1464 ANGSTROMS
A.C.A. MONOGRAPH NUMBER 75 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE, BROOKLYN, N.Y., 1963) 2ND ED.

4) THE MEASURED EXPERIMENTAL ERROR IN THE SHOCK VELOCITY BELOW 10 KM/SEC IS 1 PERCENT OR LESS AND FOR THE HIGHER VALUES THE ERROR IS BETWEEN 1.5 AND 2 PERCENT. THE VALUE OF THE SHOCK VELOCITY WAS DETERMINED FROM 5-B EXPERIMENTS.

5) ADDITIONAL CONSTANTS LISTED:

HEAT CAPACITY = 0.6693 JOULES/G/DEG.
BAND GAP = 7.5 EV.

6) THE ALUMINUM STANDARD HUGONIOT IS CHARACTERIZED BY THE FOLLOWING RELATIONSHIP: $U_S = 5.254 + 1.458 \cdot U_P - 0.0276 \cdot U_P^{1.2} + 0.00103 \cdot U_P^{1.3}$
 $\Sigma \Delta U_S = 0.013 \text{ KM/SEC. FOR } U_P = 0 \text{ TO } 10.5 \text{ KM/SEC}$
 $\rho_{H0} = 2.71 \text{ G/CC.}$

TABLE I

POTASSIUM CHLORIDE
100-10---3

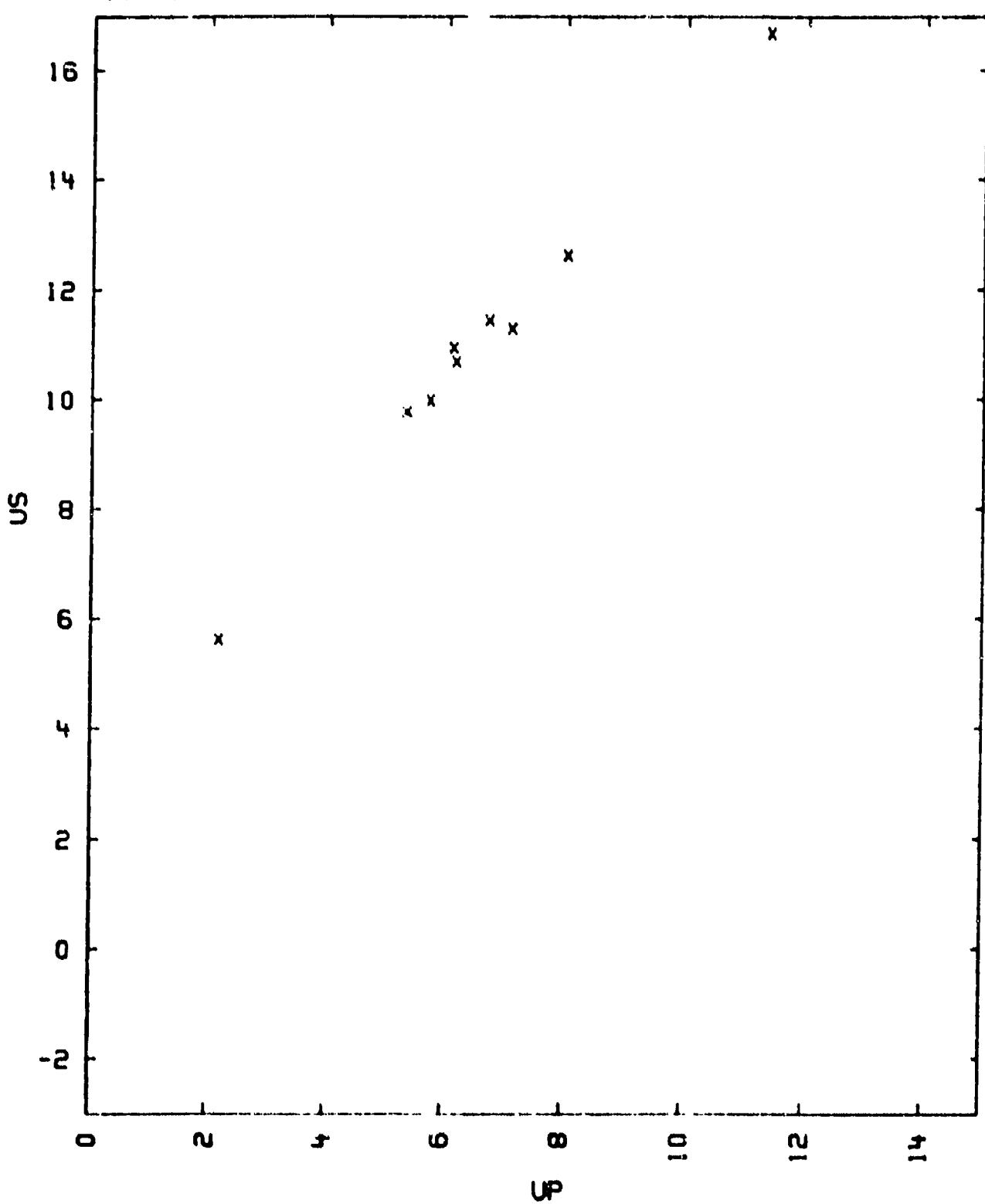
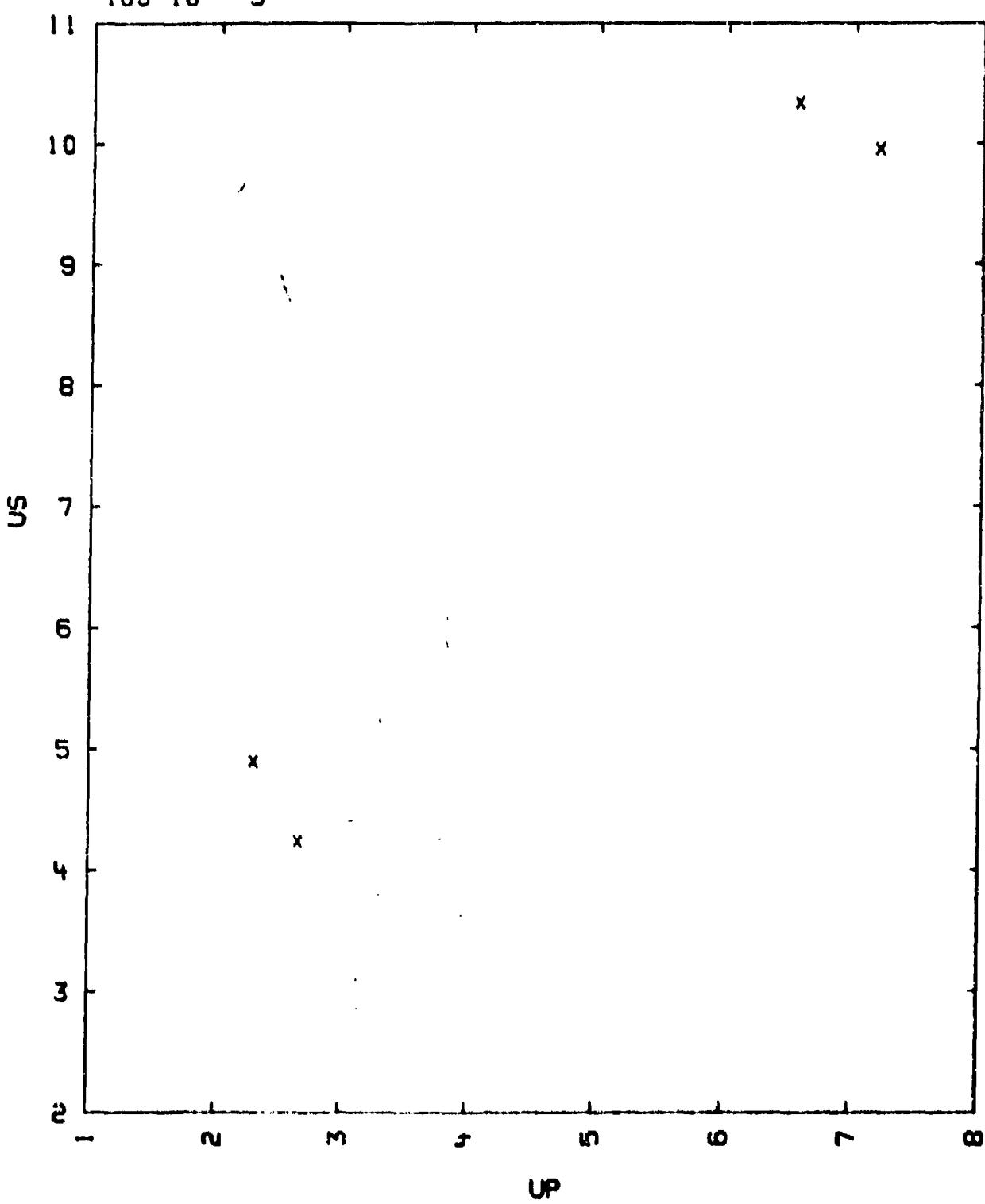


TABLE II

POTASSIUM CHLORIDE
100-10---3



100-10--4
POTASSIUM CHLORIDE

K-CL

CO = 3.04 KM/SEC

VOL = 0.5033 CC/0

THE TABLE LISTS IDEAL DENSITY IN G/CC, PARTICLE VELOCITY AND DERIVED SHOCK SPEED IN KM/SEC, INSTANTANEOUS PRESSURE AND PRESSURE ATTENUATION IN KBAR AND TIME REQUIRED FOR ATTENUATION IN NANoseconds. CRYSTALS WERE SLICE ON (100) AND (111) PLANES. U IS VELOCITY OF SAMPLE PRIOR TO IMPACT UP AND DP ARE THE OBSERVED CHANGES. THE IMPACTED STANDARD IS QUARTZ

TABLE

PLANE	RHO0	US	UP	DUP	P	DP	V/V0	U	TAU
111	1.987	3.48	0.249	0.000	17.2	0.0	0.9284	0.363	
-	-	3.52	0.276	0.000	19.3	0.0	0.9216	0.404	
-	-	3.41	0.332	0.006	22.5	0.9	0.9026	0.480	43.
-	-	3.10	0.419	0.012	25.8	1.8	0.8648	0.590	21.
-	-	3.12	0.398	0.011	24.5	1.6	0.8735	0.557	27.
-	-	3.32	0.361	0.011	23.8	1.7	0.9812	0.518	39.
-	-	3.22	0.384	0.008	24.6	1.0	0.8809	0.546	29.
100	-	3.10	0.429		26.2		0.8830	0.598	
-	-	3.23	0.380		24.4		0.8824	0.541	
-	-	3.39	0.337		22.7		0.9006	0.487	
-	-	3.59	0.287		20.5		0.9202	0.422	
-	-	3.45	0.252		17.3		0.9271	0.366	
-	-	3.10	0.422		26.0		0.8639	0.593	
-	-	2.84	0.550		31.1		0.8067	0.755	
-	-	3.58	0.298		21.2		0.9167	0.438	
-	-	3.53	0.304		21.3		0.9138	0.445	
-	-	3.52	0.276		19.3		0.9216	0.403	
-	-	3.05	0.428		26.0		0.8600	0.600	
-	-	3.14	0.385		24.0		0.8773	0.544	
-	-	3.35	0.309		21.8		0.9130	0.453	
-	-	3.11	0.437		27.0		0.8595	0.615	

US = 3.07 + 1.63*UP KM/SEC FOR UP<0.31 KM/SEC

SIG US = 0.032 KM/SEC

US = 4.22 - 2.62*UP KM/SEC FOR 0.33<UP<0.55 KM/SEC

SIG US = 0.048 KM/SEC

NOTE US = P INTERFACE / (RHO0+UP) NOT EXPERIMENTAL

COMMENTS:

1) SOURCE: MAYER D.B.

BRIT. J. APPL. PHYS. 45, 1208, (1974)

2) EXPERIMENTAL TECHNIQUE: 12 SAMPLE IMPACTED ON QUARTZ QUAGE.

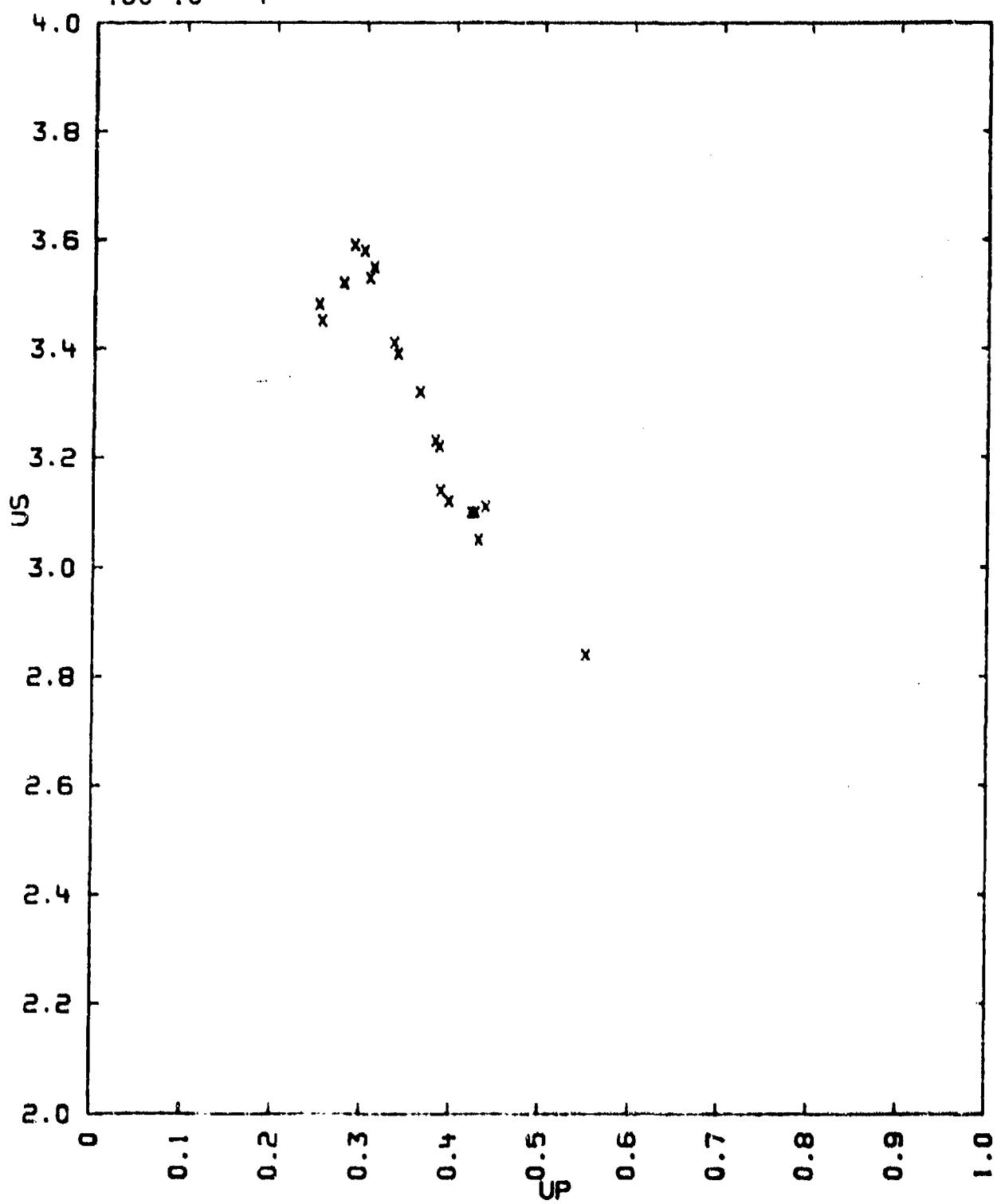
DATA REDUCTION METHOD: 6

3) THE DATA INDICATES THAT TRANSFORMATION FROM THE NA-CL TO THE CS-CL

STRUCTURE IS INCOMPLETE BETWEEN 20.9 AND 31 KBARS, BUT RAPID: MORE THAN 500 G/10. MUSEC). A SUBSEQUENT SLOWER TRANSFORMATION (ABOUT 25 G/10. MUSEC) APPEARS TO GO TO COMPLETION IN THE (1111) SAMPLES.

- 4) VOL CALCULATED FROM THE CUBIC CELL CONSTANT OF 6.29294 ANGSTROM AT 25 DEG.C. WYCKOFF, CRYSTAL STRUCTURES (JOHN WILEY AND SONS N.Y. '63)
- 5) CO WAS CALCULATED FROM THE ELASTIC CONSTANTS C11 = 4.09E+11 AND C12 = 0.706E+11 DYNES/CM²

TABLE I

POTASSIUM CHLORIDE
100-10---4

100-11---1
POTASSIUM BROMIDE

K-BR

$$V_0 = 0.364 \text{ CC}/\text{O}$$

$$V_{01} = 0.3611 \text{ CC}/\text{O}$$

$$C_B = 2.33 \text{ KM}/\text{SEC}$$

IN THE TABLE BELOW DENSITY, IS GIVEN IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS. SH DESIGNATES SAMPLE HOLDER.

TABLE

RHO0	US	UP	P	V/V0	SH	UP(SH)
2.75	3.82	0.27	21.0	0.9050	CU	0.17
-	2.75	0.50	37.5	0.8183	CU	0.30
-	2.89	0.57	45.1	0.8032	CU	0.35
-	2.74	0.61	46.0	0.7782	CU	0.37
-	3.16	0.90	78.2	0.7153	AL	0.69
-	4.51	1.80	223.0	0.6013	AL	1.50
-	4.99	2.05	280.0	0.5900	AL	1.74
-	6.62	3.20	374.5	0.5092	AL	2.82
-	7.68	4.02	849.0	0.4762	FE	2.80

US = 1.93 + 1.44 UP KM/SEC FOR UP BETWEEN 0.8 AND 4.0 KM/SEC
 $S10 \text{ US} = 0.08$

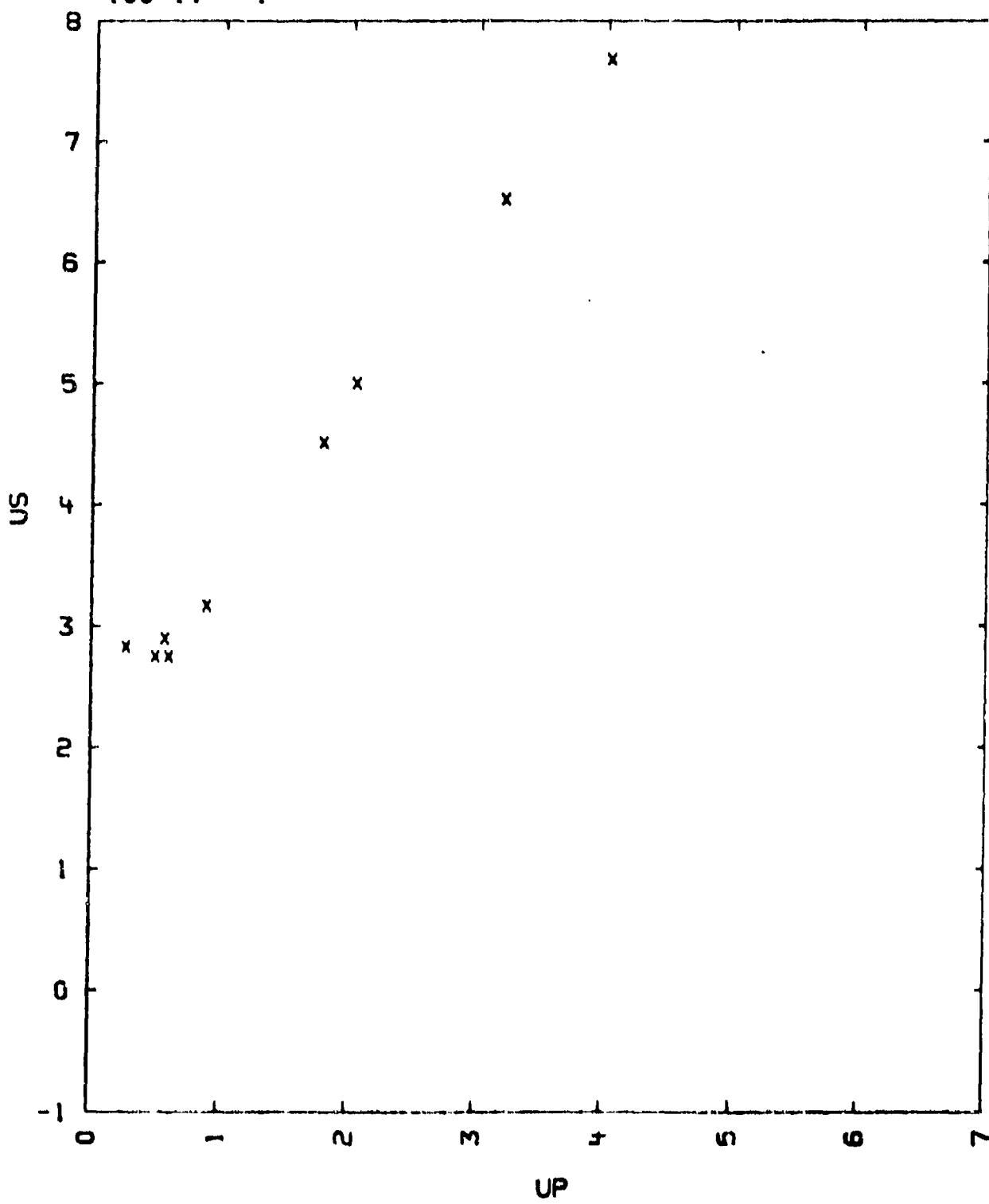
COMMENTS:

- 1) SOURCE: AL'TSHULER, L.V., PAVLOVSKII, M.M., KULESHOVA, L.V., AND SINAOKOV, O.V.
SOVIET PHYS.-SOLID STATE, VOL. 5, P. 203 (1963)
- 2) EXPERIMENTAL TECHNIQUE A
DATA REDUCTION TECHNIQUE B.
- 3) THE SAMPLES WERE POSITIONED ON PLATES OF CU AL AND FE AS INDICATED IN TABLE COLUMN 6.
THE HUGONIOTS OF FE CU AND AL WERE OBTAINED FROM
AL'TSHULER, L.V., KORNER, S.B., BAKANOVA, A.A. AND TRUNIN, R.F.
JETP VOL 11, P.573 (1960)
- 4) THE AL AND CU ADIABAT WERE OBTAINED BY REFLECTING THE HUGONIOT IN THE
P VS UP PLANE. CORRECTIONS WERE MADE FOR FE.
- 5) OTHER CONSTANTS LISTED ARE: DEBYE TEMPERATURE 177 DEG. K
HEAT CAPACITY (CV) 0.416 J/G/DEG.
CATION TO ANION DISTANCE 3.293 KX
EXPANSION COEFFICIENT 0.000118 PER DEG
- 6) POINTS WITH UP = 0.8 OR LESS CORRESPOND TO A DOUBLE SHOCK REGION
IN WHICH ONLY THE FIRST WAVE WAS MEASURED.
- 7) THE VALUE OF V01 LISTED HAS OBTAINED FROM A CATION TO ANION DISTANCE
OF 3.298 A. A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC
ASSN., POLYCRYSTAL BOOK SERVICE, BROOKLYN 1963) 2ND ED.

TABLE I

POTASSIUM BROMIDE

100-11---1



100-11---2
POTASSIUM BROMIDE

K-BR SINGLE CRYSTAL

$$V_0 = 0.387 \text{ CC/G}$$

$$V_{01} = 0.3831 \text{ CC/G}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN MM/MICROSEC., AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UFS	UP	P	V/V0	PRESSURE IN AL BASE PLATE
2.730	3.52	2.25	1.18	112	0.670	165
2.728	4.08	2.94	1.46	161	0.641	225
2.731	4.58	3.63	1.74	218	0.620	293
2.72	4.89	4.07	1.97	264	0.596	347

$$US = 1.564 + 1.704 UP \text{ MM/MICROSEC}$$

$$\text{SIGMA US} = 0.049$$

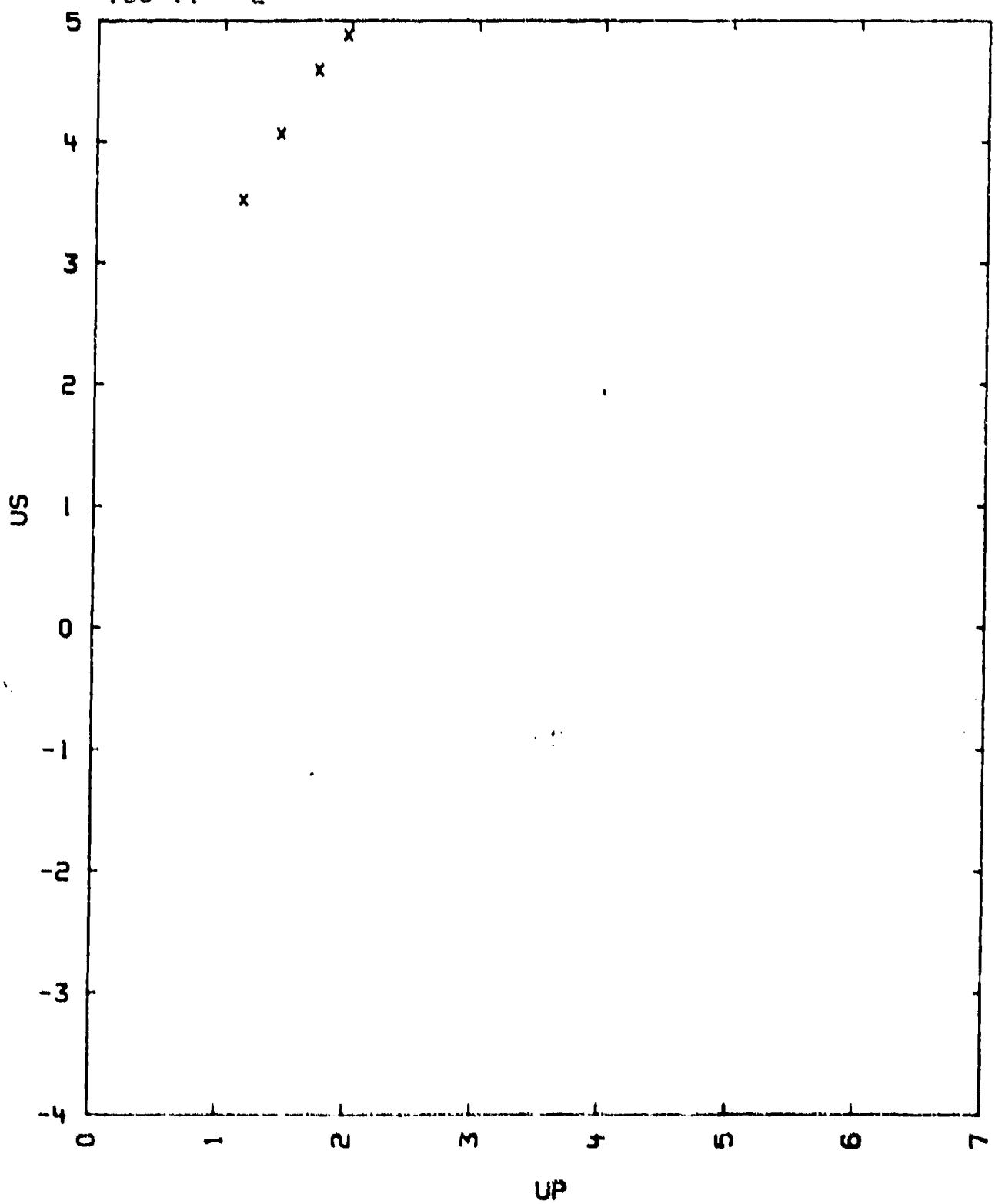
COMMENTS:

- 1) SOURCE: COMPILER
L. R. L. EQUATION OF STATE FILE
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA
- 2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)
DATA REDUCTION TECHNIQUE B.
- 3) TABULATED DATA ALSO REPORTED BY CHRISTIAN, R.H., IN
EQUATION OF STATE OF ALKALI HALIDES AT HIGH PRESSURE (THESIS)
UCRL-4900 MAY 15, 1957 UNIVERSITY OF CALIFORNIA,
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.
- 4) ALSO LISTED IN REFERENCE OF COMMENT 3 ARE:

DEBYE TEMPERATURE	177 DEG. K
HEAT CAPACITY (CV)	0.41 J/G/DEG.
EXPANSION COEFFICIENT	0.000120 PER DEG.
COMPRESSIBILITY	8.70 PER MEGABAR
MELTING POINT	735 DEG. C
- 5) THE VALUE OF V01 HAS OBTAINED FROM A LATTICE CONSTANT OF 5.598 A
A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE 1963) 2ND EDITION.

TABLE I

POTASSIUM BROMIDE
100-11--2



100-11---3
POTASSIUM BROMIDE

K-BR

$$V_0 = 0.3634 \text{ CC/G.}$$

$$V_{01} = 0.3631 \text{ CC/G.}$$

IN THE TABLES BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN KM/SEC., AND PRESSURE IN KILOBARS. ST DESIGNATES THE STANDARD MATERIAL AND UP(ST) IS THE PARTICLE VELOCITY OF THE STANDARD.

TABLE
SINGLE CRYSTAL

RHO0	US	UP	P	V/V0	ST	UP(ST)
2.752	4.95	2.03	276	0.588	AL	1.72
-	8.93	5.09	1250	0.429	FE	3.60
-	9.65	5.83	1550	0.395	FE	4.13
-	10.43	6.39	1830	0.368	FE	4.56
-	10.33	6.57	1870	0.364	AL	6.03
-	12.92	8.80	3130	0.321	FE	6.33
-	15.01	10.60	4380	0.294	AL	9.95

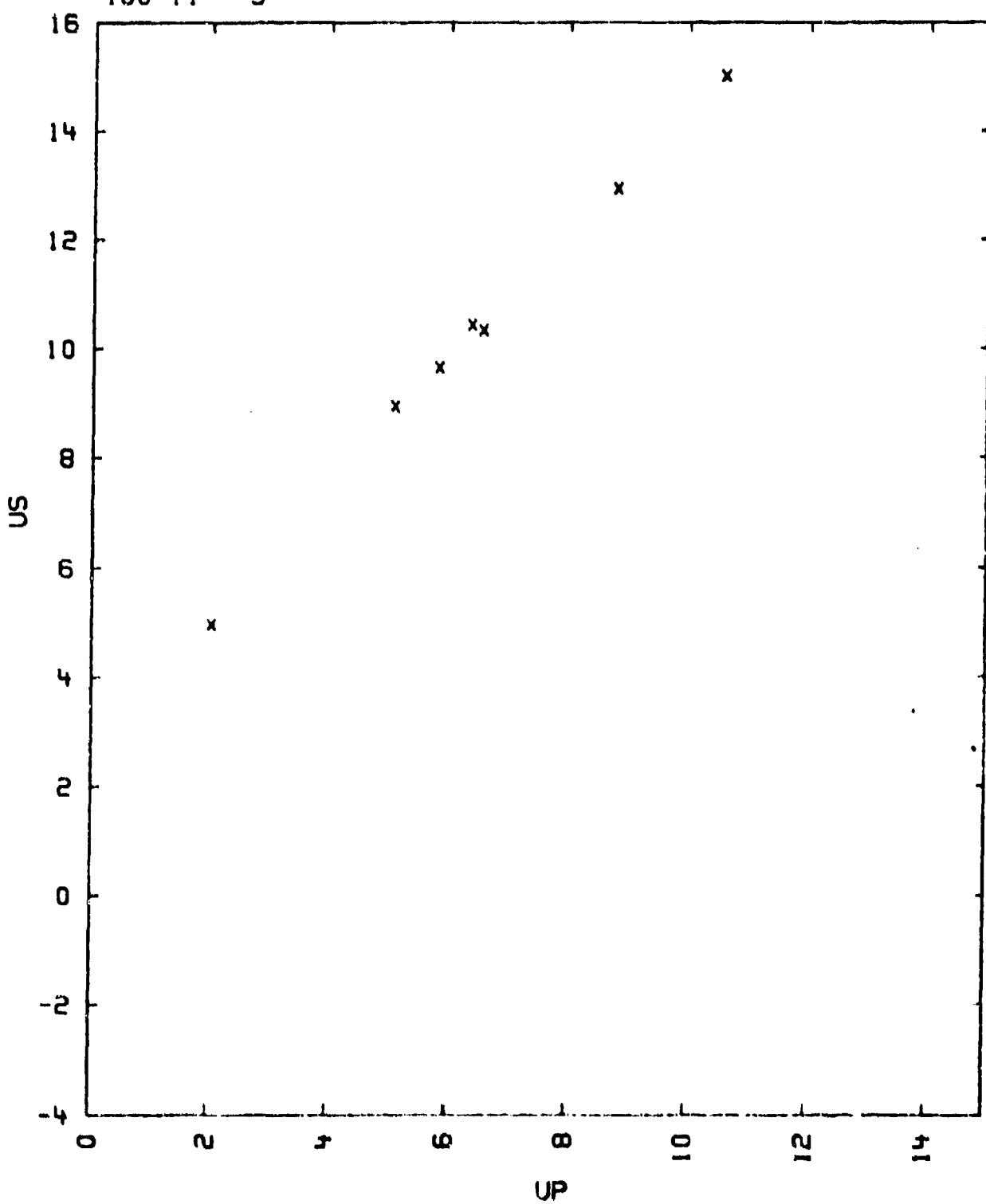
US = $3.23 + 1.106 \cdot UP$ KM/SEC. FOR US FROM 8.9 TO 15.0 KM/SEC.
 $\Sigma \text{SIGMA US} = 0.12$ KM/SEC.

COMMENTS:

- 1) SOURCE: KORMER, S. B., SINITSYN, M. V., FINTIKOV, A. I., URLIN, V. D. AND BLINOV, A. V.
 SOVIET PHYS-JETP, VOL. 20, P. 811 (1965)
 J. EXPTL. THEORET. PHYS. (U.S.S.R.) VOL. 47, P. 1202 (1964)
- 2) EXPERIMENTAL TECHNIQUE A
 DATA REDUCTION TECHNIQUE B
- 3) V01 WAS OBTAINED FROM A LATTICE CONSTANT OF 6.596 ANGSTROMS.
 A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
 POLYCRYSTAL BOOK SERVICE 1963) 2ND ED.
- 4) THE MEASURED EXPERIMENTAL ERROR IN THE SHOCK VELOCITY BELOW 10 KM/SEC
 IS 1 PERCENT OR LESS AND FOR THE HIGHER VALUES THE ERROR IS
 APPROXIMATELY 2 PERCENT. THE VALUE OF THE SHOCK VELOCITY WAS
 DETERMINED FROM 5-8 EXPERIMENTS.
- 5) ADDITIONAL CONSTANTS LISTED:
 HEAT CAPACITY = 0.4194 JOULES/G/DEG.
 BAND GAP = 6.6 EV.
- 6) THE ALUMINUM STANDARD HUGONIOT IS CHARACTERIZED BY THE FOLLOWING
 RELATIONSHIP: $US = 5.254 + 1.458 \cdot UP - 0.0276 \cdot UP^{1.2} + 0.00103 \cdot UP^{1.3}$
 $\Sigma \text{SIGMA US} = 0.013$ KM/SEC. FOR UP = 0 TO 10.5 KM/SEC
 RHO0 = 2.71 G/CC.

TABLE I

POTASSIUM BROMIDE
100-11--3



100-12---1
POTASSIUM IODIDE

K-1 SINGLE CRYSTAL

$$V_0 = 0.321 \text{ CC/G}$$

$$V_{OI} = 0.3120 \text{ CC/G}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN MM/MICROSEC., AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UFS	UP	P	V/V0	PRESSURE IN AL BASE PLATE
3.105	3.28	2.20	1.10	110	0.668	156
3.11	3.70	2.80	1.40	161	0.624	219
3.10	4.22	3.52	1.72	227	0.594	293
3.140	4.47	4.07	1.99	278	0.555	356

$$US = 1.787 + 1.372 UP \text{ MM/MICROSEC}$$

$$\text{SIGMA US} = 0.063$$

COMMENTS:

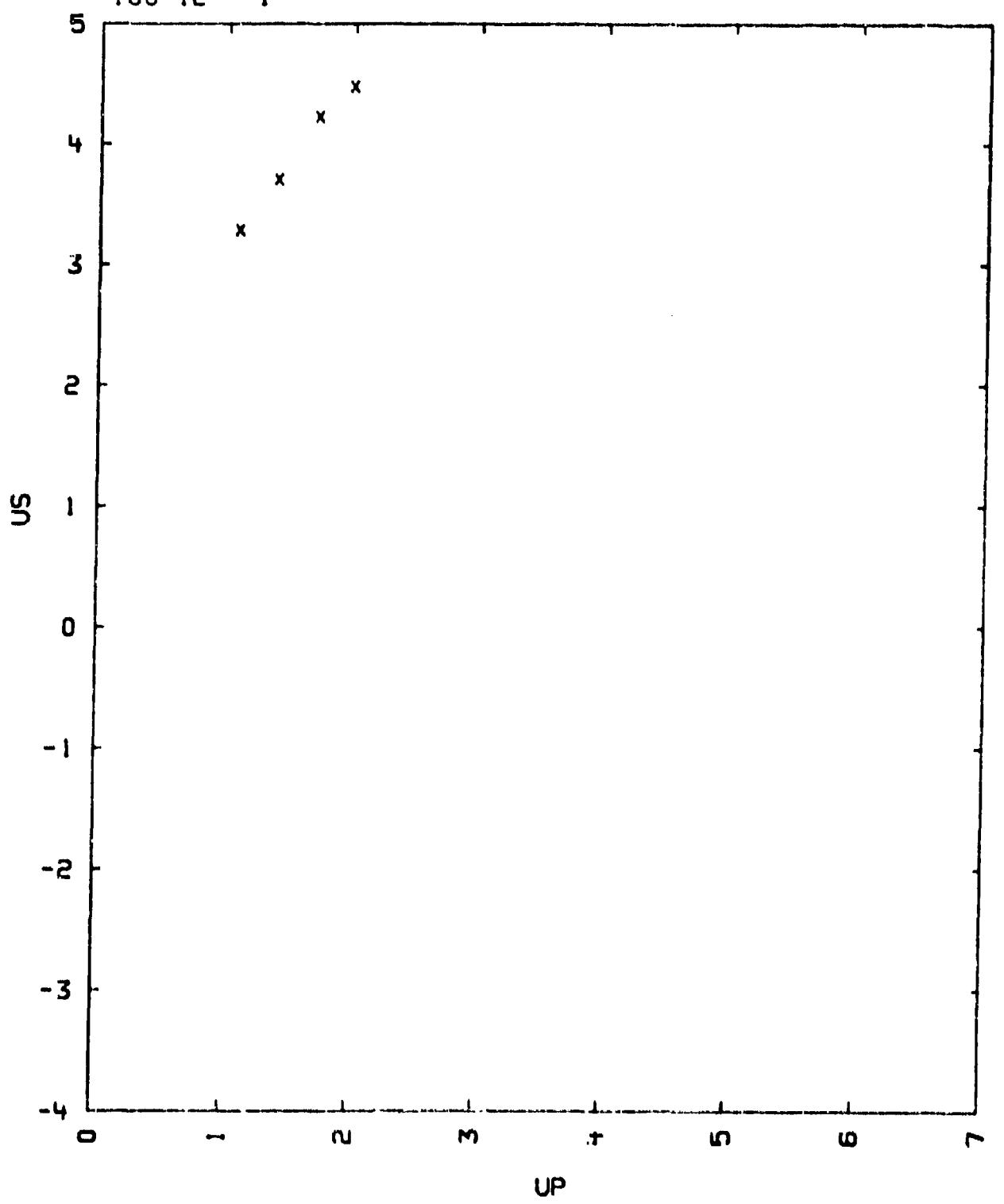
- 1) SOURCE: COMPILER
L. R. L. EQUATION OF STATE FILE
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA
- 2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)
DATA REDUCTION TECHNIQUE B.
- 3) TABULATED DATA ALSO REPORTED BY CHRISTIAN, R.H., IN
EQUATION OF STATE OF ALKALI HALIDES AT HIGH PRESSURE (THESIS)
UCRL-4900 MAY 16, 1957 UNIVERSITY OF CALIFORNIA,
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.
- 4) ALSO LISTED IN REFERENCE OF COMMENT 3 ARE:

DEBYE TEMPERATURE	132 DEG. K
HEAT CAPACITY (CV)	0.30 J/G/DEG.
EXPANSION COEFFICIENT	0.000120 PER DEG.
COMPRESSIBILITY	8.53 PER MEGABAR
MELTING POINT	685 DEG. C
- 5) THE VALUE OF V0I WAS OBTAINED FROM A LATTICE CONSTANT OF 7.066 A
A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE 1963) 2ND EDITION.

TABLE I

POTASSIUM IODIDE

100-12---1



100-29-24-1---

MICROCLINE, ONTARIO (POTASSIUM ALUMINUM SILICATE)

K-AL-S13-08

PURITY SEE COMMENT 3

$V_0 = 0.3905 - 0.3922 \text{ CC}/\text{G}$ $C_L(001) = 6.95 \text{ KM}/\text{SEC}$
 $V_{01} = 0.3902 - 0.3894 \text{ CC}/\text{G}$

THE TABLE LISTS DENSITY IN G/CC, VELOCITY IN KM/SEC., AND PRESSURE IN KBAR
 MAT IS THE BASE PLATE- OR STANDARD MATERIAL: AL=ALUMINUM, BR=BRASS

TABLE

SAMPLE											STANDARD	
RHO0	US1	UPI	P1	V1/V0	US2	UP2	UFS	P2	V2/V0	D	MAT	UFS
2.561	7.19	0.438	80.7	0.939	3.97	1.795	1.99	115.	0.844	3.31	AL	1.69
2.550	7.09	-	79.2	0.938	5.22	2.10	4.04	295.	0.612	4.81	-	3.60
2.561	7.32	-	82.1	0.940	6.44	2.69	5.28	450.	0.587	4.83	-	4.80
2.561	7.56	-	84.8	0.942	6.56	2.66	5.23	455.	0.560	3.32	-	-
2.561	7.14	3.13	572.	0.562				8.12			4.82	BR 4.40
2.561	7.19	-	576.	0.565				6.10			3.32	-

US *

COMMENTS:

- 1) SOURCE: AHRENS T.J., PETERSEN, C.F. AND ROSENBERG, J.T.
J. GEOPHYS. RES. VOL. 74, P. 2727 (1969)
- 2) EXPERIMENTAL TECHNIQUE C1 (INCLINED MIRROR)
DATA REDUCTION METHOD B AND D1 (ELASTIC WAVES)
- 3) THE SAMPLES WERE OBTAINED FROM WARDS NATIONAL SCIENCE ESTABLISHMENT
NO PURITY ANALYSIS IS GIVEN, THE DENSITY IS INSIGNIFICANTLY DIFFERENT
FROM MAXIMUM MICROCLINE FROM PONTISKALK SWITZERLAND (FINNEY AND BAILEY,
Z. KRIST. 119, 1413 (1964))
- 4) VOI FROM TWO SOURCES IN CRYSTAL DATA DETERMINATIVE TABLES, DONNAY AND
ONOIK EDITORS (U.S. DEP. OF COMMERCE, N.B.S. 1973) V2, EDITION 3
- 5) CO WAS TAKEN FROM ALEXANDROV, K.S. AND RYZHOVA, T.V.
BULL. USSR. ACADEMY OF SCIENCES, GEOPHYS. SER. NO. 2, 129 (1962)

TABLE I

MICROCLINE, ONTARIO (POTASSIUM ALUMINUM SILICATE)
100-29-24-1---1

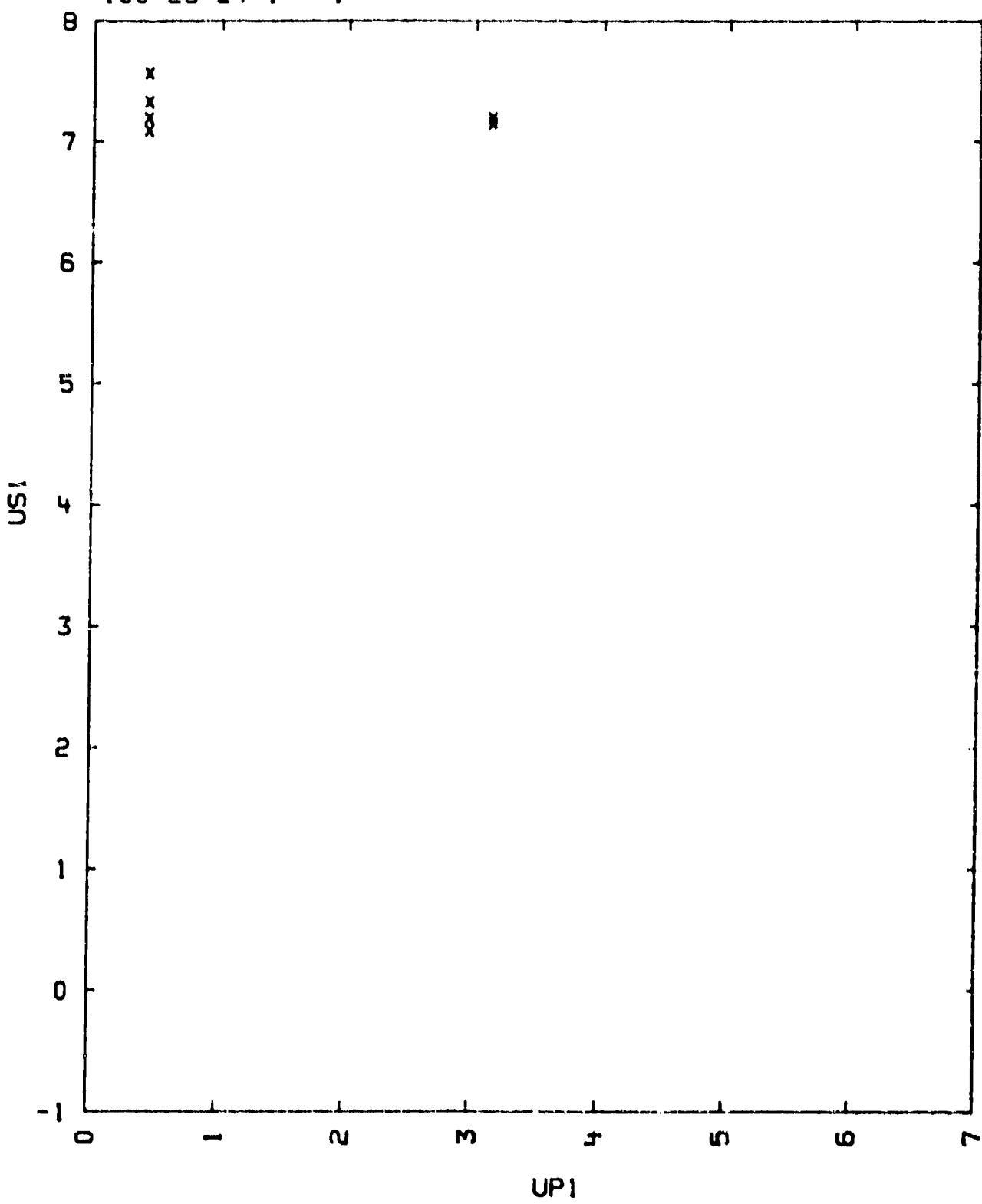
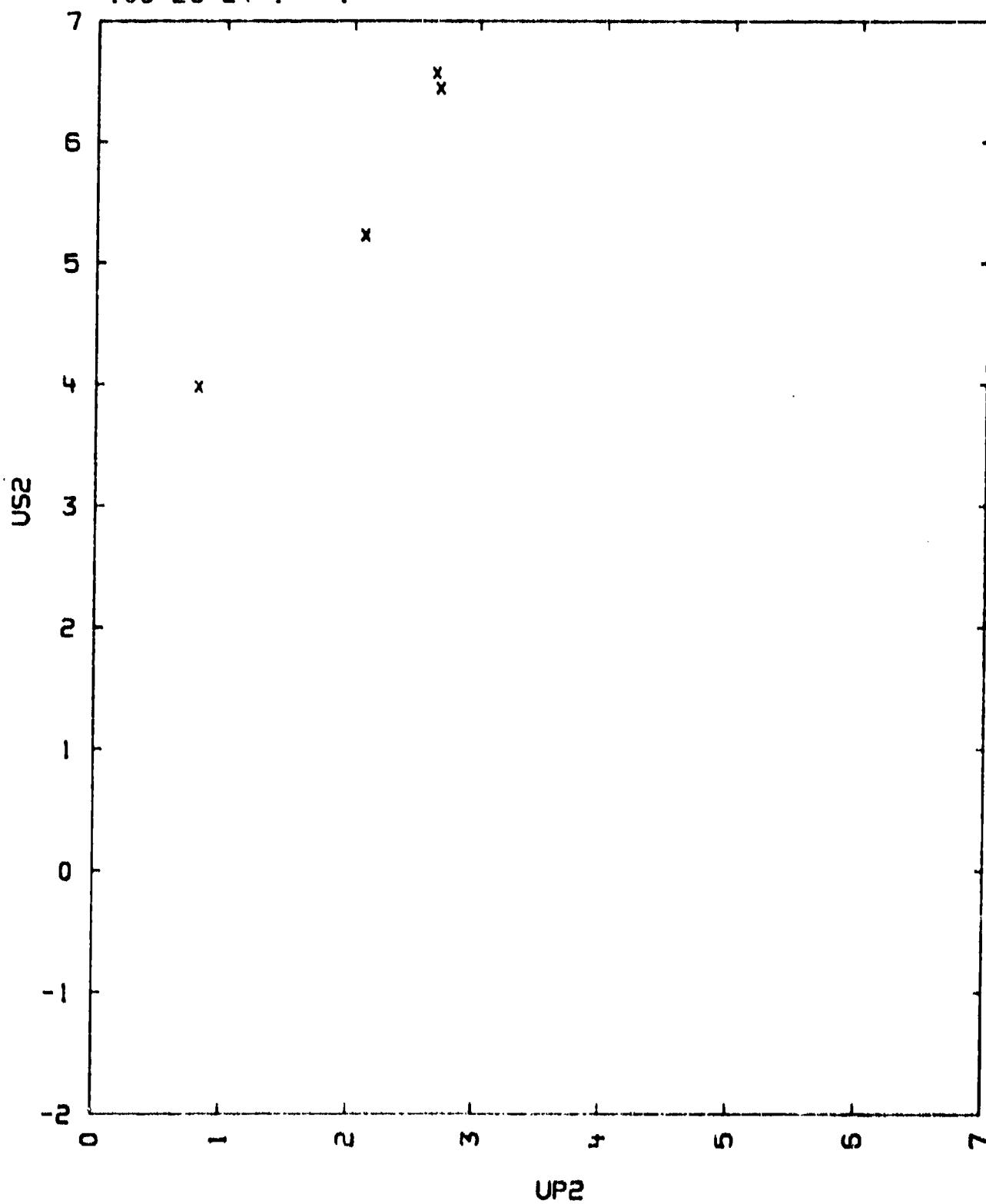


TABLE I

MICROCLINE, ONTARIO (POTASSIUM ALUMINUM SILICATE)
100-29-24-1---1



101-9---1
RUDIDIUM FLUORIDE

RD-F PRESSED

$$\text{V}_0 = 0.265 - 0.270 \text{ CC/G}$$

$$\text{V}_{01} = 0.259 \text{ CC/G}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN MM/MICROSEC., AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UFS	UP	P	V/V0	PRESSURE IN AL BASE PLATE
3.748	4.83	3.81	1.94	351	0.598	363
3.769	4.86	3.45	1.75	307	0.625	341
3.753	3.86	-	1.28	185	0.669	218
3.741	3.67	2.37	1.29	177	0.649	215
3.700	3.22	1.51	0.83	99	0.742	124
3.768	2.86	0.94	0.50	54	0.825	70

$$\text{US} = 2.067 + 1.419 \text{ UP MM/MICROSEC.}$$

$$\text{SIGMA US} = 0.136 \text{ MM/MICROSEC.}$$

COMMENTS:

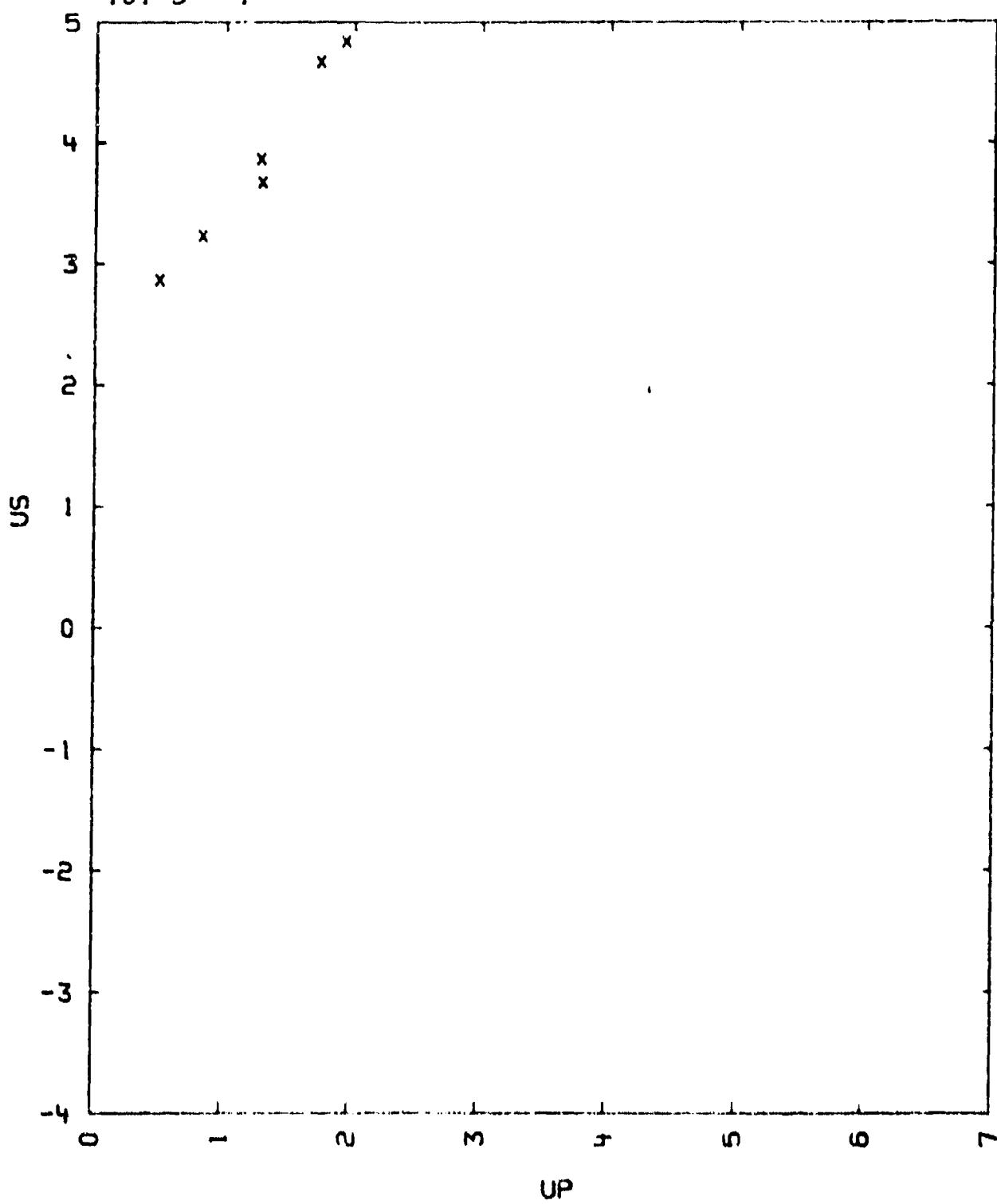
- 1) SOURCE: COMPILER
L. R. L. EQUATION OF STATE FILE
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA
- 2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)
DATA REDUCTION TECHNIQUE B.
- 3) THE FOLLOWING DATA WAS OBTAINED FROM CHRISTIAN, R. H.,
EQUATION OF STATE OF ALKALI HALIDES AT HIGH PRESSURE (THESIS)
UCRL-4900 MAY 16, 1957, UNIVERSITY OF CALIFORNIA
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA

DEBYE TEMPERATURE	238 DEG. K
HEAT CAPACITY (CV)	0.48 J/G/DEG.
EXPANSION COEFFICIENT	0.00010 PER DEG.
COMPRESSIBILITY	4.0 PER MEGABAR
MELTING POINT	775 DEG. C
- 4) THE VALUE OF V01 WAS OBTAINED FROM A LATTICE CONSTANT (F 5.64 A
A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE, BROOKLYN, N.Y., 1963) 2ND ED.

TABLE I

RUBIDIUM FLUORIDE

101-9---1



101-10--1
RUBIDIUM CHLORIDE

RA-CL PRESSED

$$V_0 = 0.369 \text{ CC/G}$$

$$V_{01} = 0.3496 \text{ CC/G}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN MM/MICROSEC., AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UFS	UP	P	V/V0	PRESSURE IN AL BASE PLATE
2.752	3.43	2.25	1.16	109	0.663	162
2.685	3.91	2.81	1.44	151	0.632	218
2.725	4.48	3.67	1.82	222	0.594	304
2.690	4.87	4.04	2.04	268	0.581	360

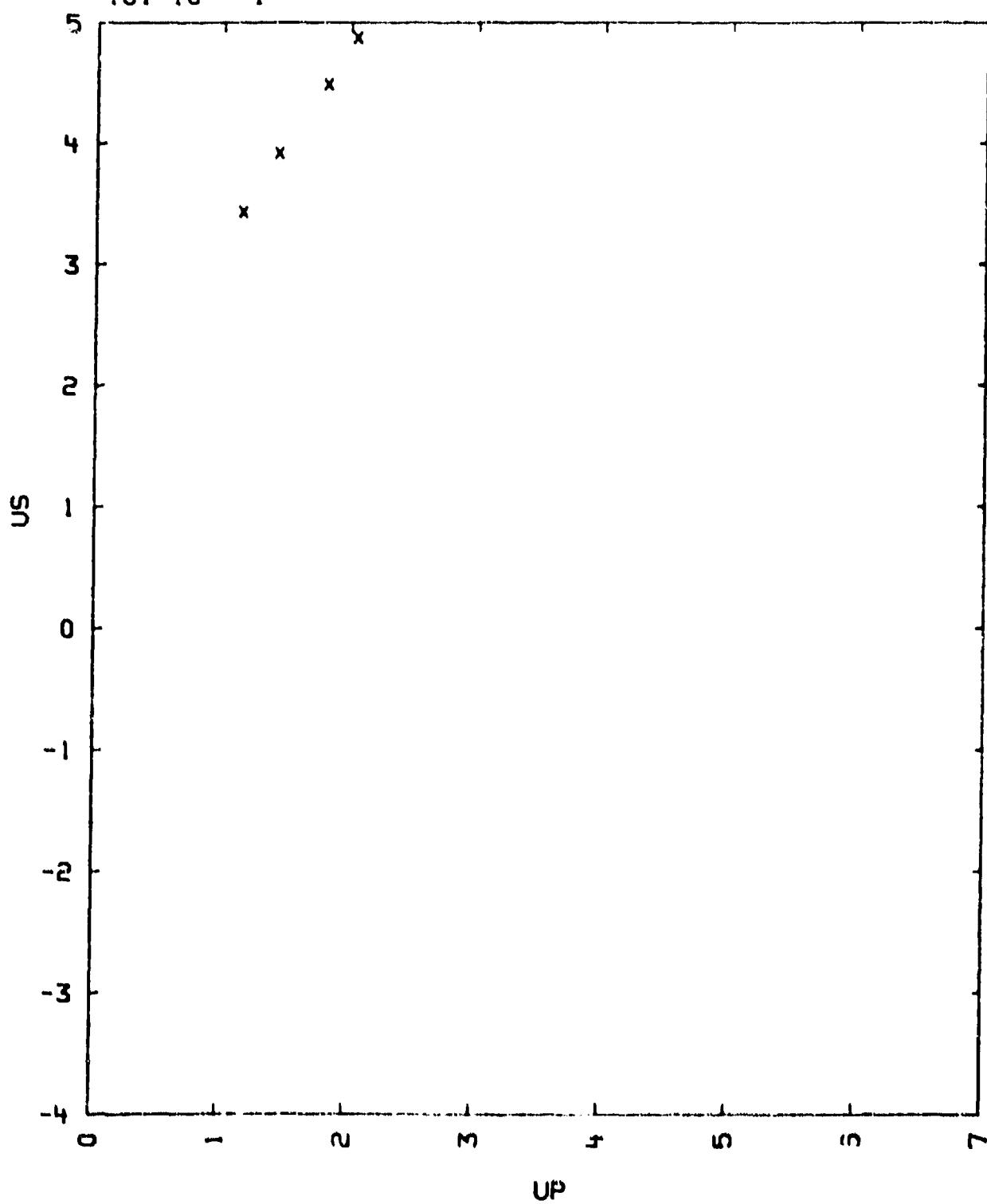
US = 1.565 + 1.615 UP MM/MICROSEC
SIGMA US = 0.024

COMMENTS:

- 1) SOURCE: COMPILER
L. R. L. EQUATION OF STATE FILE
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA
- 2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)
DATA REDUCTION TECHNIQUE B.
- 3) TABULATED DATA ALSO REPORTED BY CHRISTIAN, R.H., IN
EQUATION OF STATE OF ALKALI HALIDES AT HIGH PRESSURE (THESIS)
UCRL-4900 MAY 16, 1957 UNIVERSITY OF CALIFORNIA,
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.
- 4) ALSO LISTED IN REFERENCE OF COMMENT 3 ARE:

DEBYE TEMPERATURE	173 DEG. K
HEAT CAPACITY (CV)	0.40 J/G/DEG.
EXPANSION COEFFICIENT	0.00011 PER DEG.
COMPRESSIBILITY	6.65 PER MEGABAR
MELTING POINT	722 DEG. C
- 5) THE VALUE OF V01 WAS OBTAINED FROM A LATTICE CONSTANT OF 6.548 A
A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE 1963) 2ND EDITION.

TABLE I

RUBIDIUM CHLORIDE
101-10---1

101-11---1
RUBIDIUM BROMIDE

RB-BR PRESSED

$$\begin{aligned} V_0 &= 0.304 \text{ CC/O} \\ V_{01} &= 0.2949 \text{ CC/O} \end{aligned}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN MM/MICROSEC., AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UFS	UP	P	V/V0	PRESSURE IN AL BASE PLATE
3.285	3.16	2.08	1.08	112	0.659	156
3.295	3.62	2.67	1.38	163	0.619	218
3.300	4.16	3.51	1.73	237	0.585	300
3.298	4.44	3.96	1.96	286	0.559	356

$$\begin{aligned} US &= 1.585 + 1.470 UP \text{ MM/MICROSEC} \\ \text{SIGMA US} &= 0.031 \end{aligned}$$

COMMENTS:

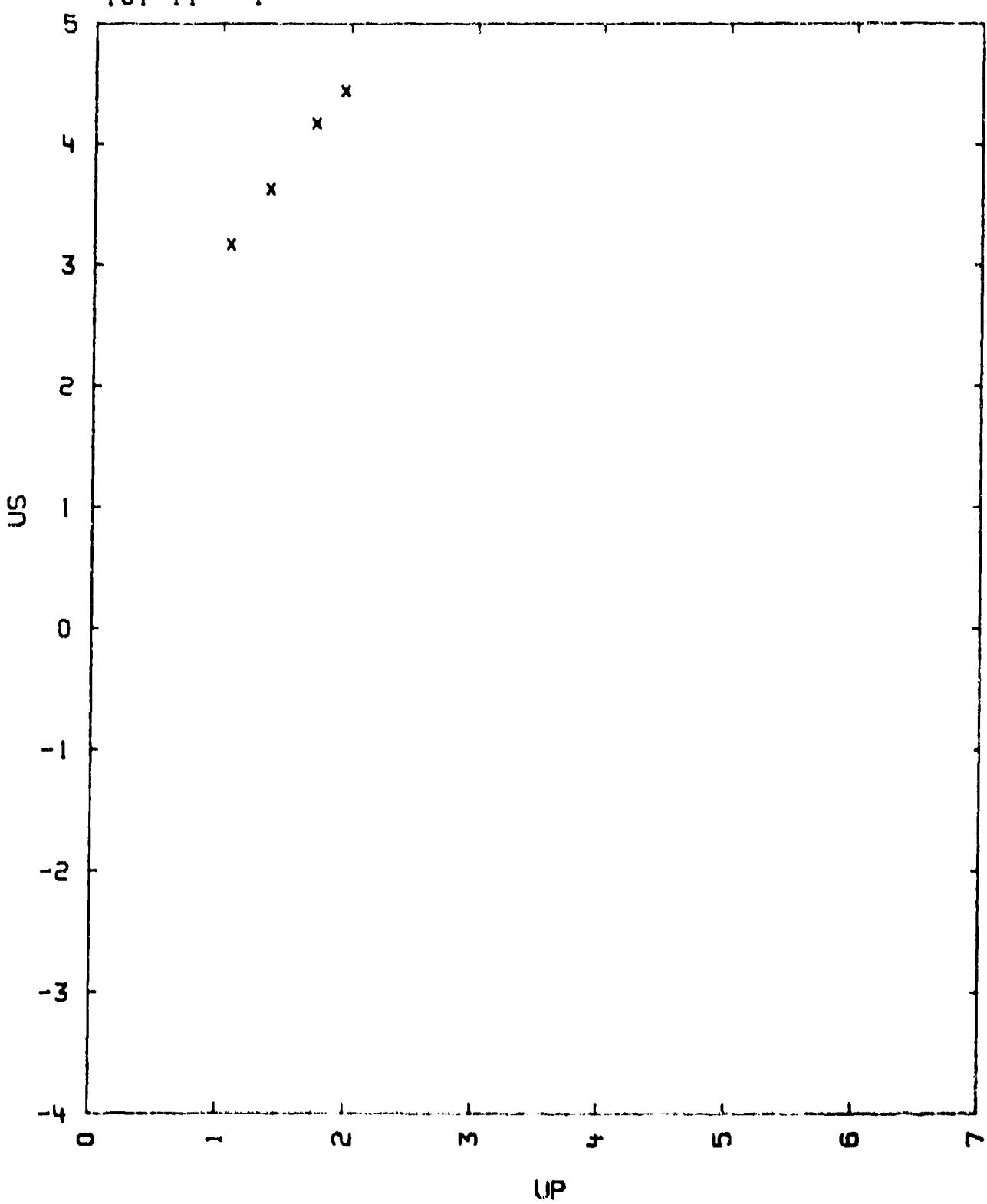
- 1) SOURCE: COMPILER
L. R. L. EQUATION OF STATE FILE
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA
- 2) EXPERIMENTAL TECHNIQUE U (ALUMINUM STANDARD BASE PLATE)
DATA REDUCTION TECHNIQUE B.
- 3) TABULATED DATA ALSO REPORTED BY CHRISTIAN, R.H., IN
EQUATION OF STATE OF ALKALI HALIDES AT HIGH PRESSURE (THESIS)
UCRL-4900 MAY 16, 1957 UNIVERSITY OF CALIFORNIA,
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.
- 4) ALSO LISTED IN REFERENCE OR COMMENT 3 ARE:

DERBY TEMPERATURE	140 DEG. K
HEAT CAPACITY (CV)	0.30 J/G/DEG.
EXPANSION COEFFICIENT	0.00011 PER DEG.
COMPRESSIBILITY	7.94 PER MEGABAR
MELTING POINT	692 DEG. C
- 5) THE VALUE OF V01 WAS OBTAINED FROM A LATTICE CONSTANT OF 6.668 A
A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE 1953) 2ND EDITION.

TABLE I

RUBIDIUM BROMIDE

101-11---1



101-12---1
RUBIDIUM 100IDE

RB-1 PRESSED

$V_0 = 0.288 \text{ CC/G}$
 $V_{01} = 0.2804 \text{ CC/G}$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICROSEC,
AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UFS	UP	P	V/V0	PRESSURE IN AL BASE PLATE
3.500	3.01	2.21	1.11	117	0.631	160
3.448	3.44	2.75	1.37	163	0.603	218
3.457	3.95	3.53	1.73	235	0.562	300
3.480	4.24	4.05	1.91	279	0.550	347

$$US = 1.337 + 1.518 UP \text{ MM/MICROSEC}$$

SIGMA US = 0.021

COMMENTS:

1) SOURCE: COMPILER

L. R. L. EQUATION OF STATE FILE

LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA

2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)

DATA REDUCTION TECHNIQUE B.

3) TABULATED DATA ALSO REPORTED BY CHRISTIAN, R.H., IN

EQUATION OF STATE OF ALKALI HALIDES AT HIGH PRESSURE (THESIS)
UCRL-4900 MAY 16, 1957 UNIVERSITY OF CALIFORNIA,

LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.

4) ALSO LISTED IN REFERENCE OF COMMENT 3 ARE:

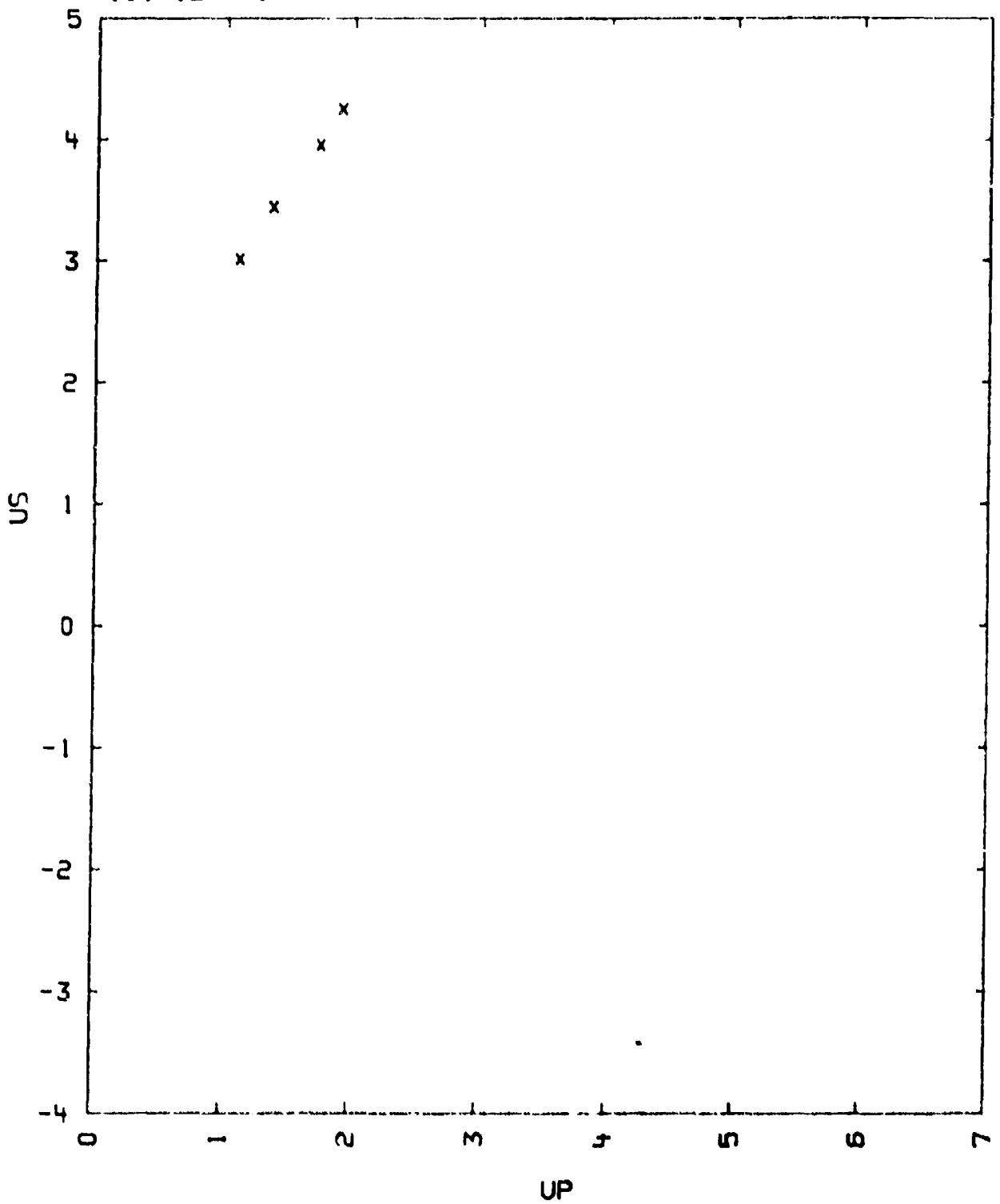
DEBYE TEMPERATURE	110 DEG. K
HEAT CAPACITY (CV)	0.23 J/G/DEG.
EXPANSION COEFFICIENT	1.20 PER DEG.
COMPRESSIBILITY	9.58 PER MEGABAR
MELTING POINT	647 DEG. C

5) THE VALUE OF V01 WAS OBTAINED FROM A LATTICE CONSTANT OF 7.340 A
A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLCRYSTAL BOOK SERVICE 1963) 2ND EDITION.

106/14/77

TABLE I

RUBIDIUM IODIDE
101-12---1



102-10---1
CESIUM CHLORIDE

CS-CL PRESSED

$$V_0 = 0.253 \text{ CC/G}$$

$$V_{01} = 0.2504 \text{ CC/G}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN MM/MICROSEC.
AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UFS	UP	P	V/V0	PRESSURE IN AL BASE PLATE
3.960	2.92	-	0.51	60	0.825	73
3.960	3.75	2.12	1.04	154	0.723	174
3.955	3.65	2.33	1.13	172	0.707	194
3.946	4.47	3.17	1.53	270	0.658	292
3.932	4.70	3.58	1.72	318	0.636	342

$$US = 2.182 + 1.481 UP \text{ MM/MICROSEC}$$

$$\text{SIGMA US} = 0.029$$

COMMENTS:

- 1) SOURCE: COMPILER
L. R. L. EQUATION OF STATE FILE
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA
- 2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)
DATA REDUCTION TECHNIQUE B.
- 3) TABULATED DATA ALSO REPORTED BY CHRISTIAN, R.H., IN
EQUATION OF STATE OF ALKALI HALIDES AT HIGH PRESSURE (THESIS)
UCRL-4900 MAY 16, 1957 UNIVERSITY OF CALIFORNIA,
LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.
- 4) ALSO LISTED IN REFERENCE OF COMMENT 3 ARE:

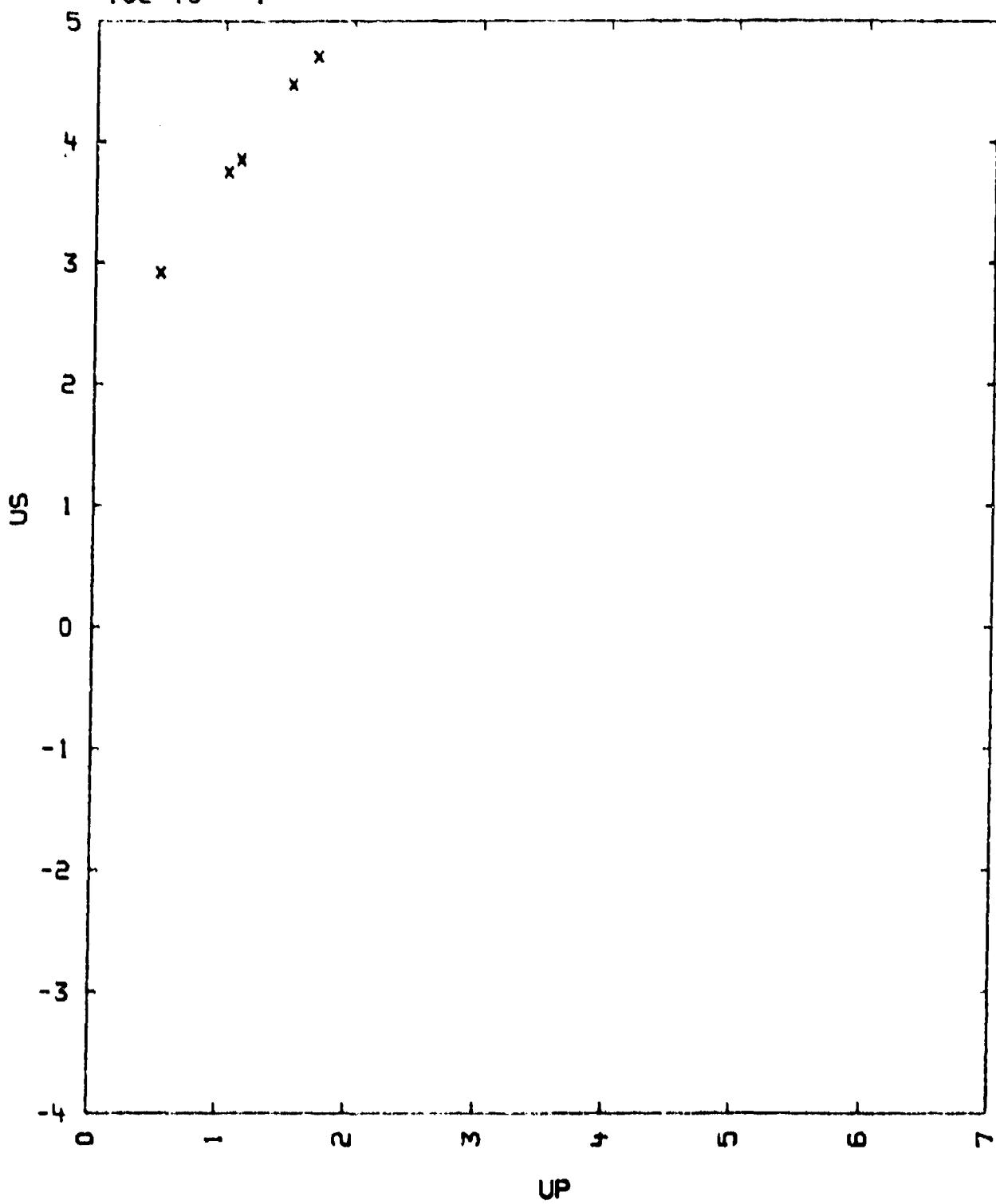
DEBYE TEMPERATURE	150 DEG. K
HEAT CAPACITY (CV)	0.29 J/G/DEG.
EXPANSION COEFFICIENT	0.000138 PER DEG.
COMPRESSIBILITY	5.95 PER MEGABAR
MELTING POINT	645 DEG. C
- 5) THE VALUE OF V01 HAS OBTAINED FROM A LATTICE CONSTANT OF 4.121 A
A.C.A. MONOGRAPH NUMBER 4 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE, BROOKLYN, N.Y., 1963) 2ND ED.

U06/14/77

TABLE I

CESIUM CHLORIDE

102-10---1



102-11---1
CESIUM BROMIDE

CS-BR SINGLE CRYSTAL

$$V_0 = 0.226 \text{ CC/G}$$

$$V_{01} = 0.2244 \text{ CC/G}$$

$$C_0 = 1.89 \text{ KM/SEC}$$

$$C_B = 1.86 \text{ KM/SEC}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICROSEC,
AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UFS	UP	P	V/V0	PRESSURE IN AL BASE PLATE
4.414	3.41	1.84	0.97	146	0.716	160
4.446	3.83	2.57	1.25	213	0.672	230
4.433	4.15	3.16	1.52	280	0.632	296
4.427	4.38	3.58	1.69	328	0.614	343
4.443	6.54	-	3.52	1023	0.461	1009
4.430	6.08	6.73	2.93	786	0.518	773
4.439	4.55	4.00	1.81	366	0.602	378

$$US = 2.253 + 1.256 UP \text{ MM/MICROSEC}$$

$$\text{SIGMA US} = 0.094$$

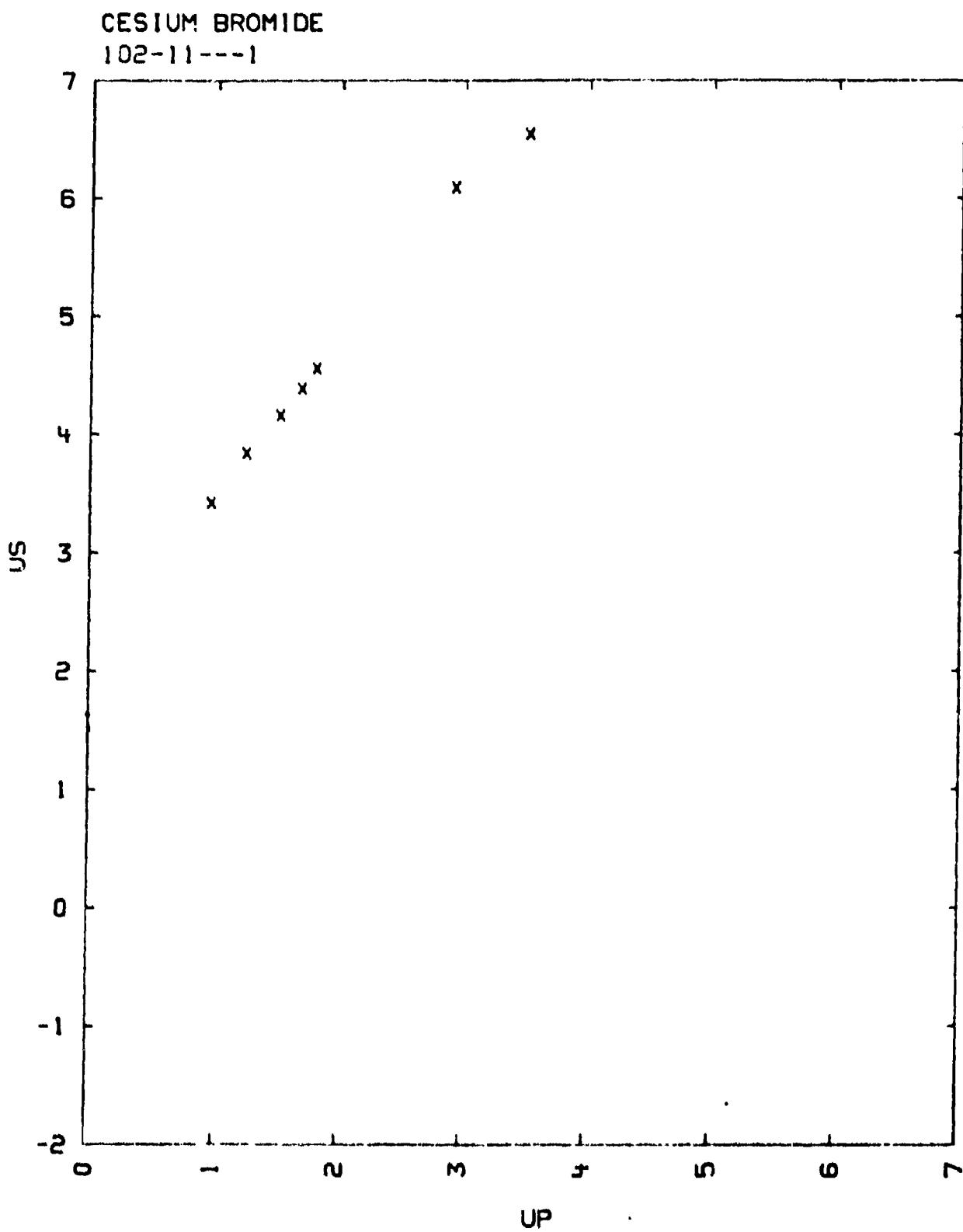
COMMENTS:

- 1) SOURCE: COMPILER
L. R. L. EQUATION OF STATE FILE
LAURENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA
- 2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)
DATA REDUCTION TECHNIQUE B.
- 3) PART OF THE TABULATED DATA ALSO REPORTED BY CHRISTIAN, R. H., IN
EQUATION OF STATE OF ALKALI HALIDES AT HIGH PRESSURE (THESIS)
UCRL-4900 MAY 16, 1957 UNIVERSITY OF CALIFORNIA,
LAURENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.
- 4) ALSO LISTED IN REFERENCE OF COMMENT 3 ARE:

DEBYE TEMPERATURE	114 DEG. K
HEAT CAPACITY (CV)	0.23 J/G/DEG.
EXPANSION COEFFICIENT	0.000116 PER DEG.
COMPRESSIBILITY	7.06 PER MEGABAR
MELTING POINT	638 DEG. C
- 5) THE VALUE OF V01 WAS OBTAINED FROM A LATTICE CONSTANT OF 4.296 A
A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE 1963) 2ND EDITION.
- 6) CO WAS OBTAINED FROM ELASTIC CONSTANTS GIVEN BY
P. J. REDDY AND A. L. RUOFF, PHYS. SOLIDS AT HIGH PRESSURES
IN PRINTS (1965)

U06/14/77

TABLE I



102-11---2
CESIUM BROMIDE

CS-BR

$$V_0 = 0.2247 \text{ CC}/\text{O}$$

$$V_{01} = 0.2244 \text{ CC}/\text{O}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN KM/SEC., AND PRESSURE IN KILOBARS. ST DESIGNATES THE STANDARD MATERIAL AND UP(ST) IS THE PARTICLE VELOCITY IN THE STANDARD

TABLE I
SINGLE CRYSTAL

RHO0	US	UP	P	V/V0	ST	UP(ST)
4.45	3.17	0.75	110	0.763	AL	0.69
-	4.52	1.73	347	0.617	AL	1.70
-	5.92	2.75	720	0.535	AL	2.82
-	8.17	4.60	1670	0.437	FE	3.60
-	9.33	5.69	2360	0.391	AL	6.03
-	13.19	9.29	5450	0.296	AL	9.95

$$US = 2.15 + 1.414 UP - 0.0245 UP^{+2} \text{ KM/SEC. } \text{ SIGMA US} = 0.06 \text{ KM/SEC.}$$

$$V_0 = 0.339 - 0.495 \text{ CC}/\text{O}.$$

TABLE II
POROUS

RHO0	US	UP	P	V/V0	ST	UP(ST)
2.95	3.90	1.99	228	0.490	AL	1.60
-	8.79	5.86	1519	0.334	FE	4.13
2.02	3.71	2.25	169	0.394	AL	1.60
-	8.77	6.33	1122	0.279	FE	4.13

$$US =$$

COMMENTS:

- 1) SOURCE: KURMER, S. B., SINITSYN, M. V., FUNTIKOV, A. I., URLIN, V. D. AND BLINOV, A. V.
SOVIET PHYS-JETP, VOL. 20, P. BII (1965)
J. EXPTL. THEORET. PHYS. (U.S.S.R.) VOL. 47, P. 1202 (1964)
- 2) EXPERIMENTAL TECHNIQUE A
DATA REDUCTION TECHNIQUE B
- 3) V01 WAS CALCULATED FROM A LATTICE CONSTANT OF 4.296 ANGSTROMS.
A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE 1963) 2ND ED.
- 4) THE MEASURED EXPERIMENTAL ERROR IN THE SHOCK VELOCITY BELOW 10 KM/SEC
IS 1 PERCENT OR LESS AND FOR THE HIGHER VALUES THE ERROR IS
APPROXIMATELY 1.5 PERCENT. THE VALUE OF THE SHOCK VELOCITY WAS

UOB/14/77

DETERMINED FROM S-B EXPERIMENTS.

5) ADDITIONAL CONSTANTS LISTED:

HEAT CAPACITY = 0.2355 JOULES/G/DEG.

BAND GAP = 6.0 EV.

- 6) THE ALUMINUM STANDARD HUGONIOT IS CHARACTERIZED BY THE FOLLOWING
RELATIONSHIP: $U_S = 5.254 + 1.458 \cdot U_P - 0.0276 \cdot U_P^{+2} + 0.00103 \cdot U_P^{+3}$
 $\Sigma \Omega_M U_S = 0.013 \text{ KM/SEC. FOR } U_P = 0 \text{ TO } 10.5 \text{ KM/SEC}$
 $\rho_{H_0} = 2.71 \text{ G/CC.}$

TABLE I

CESIUM BROMIDE

102-11---2

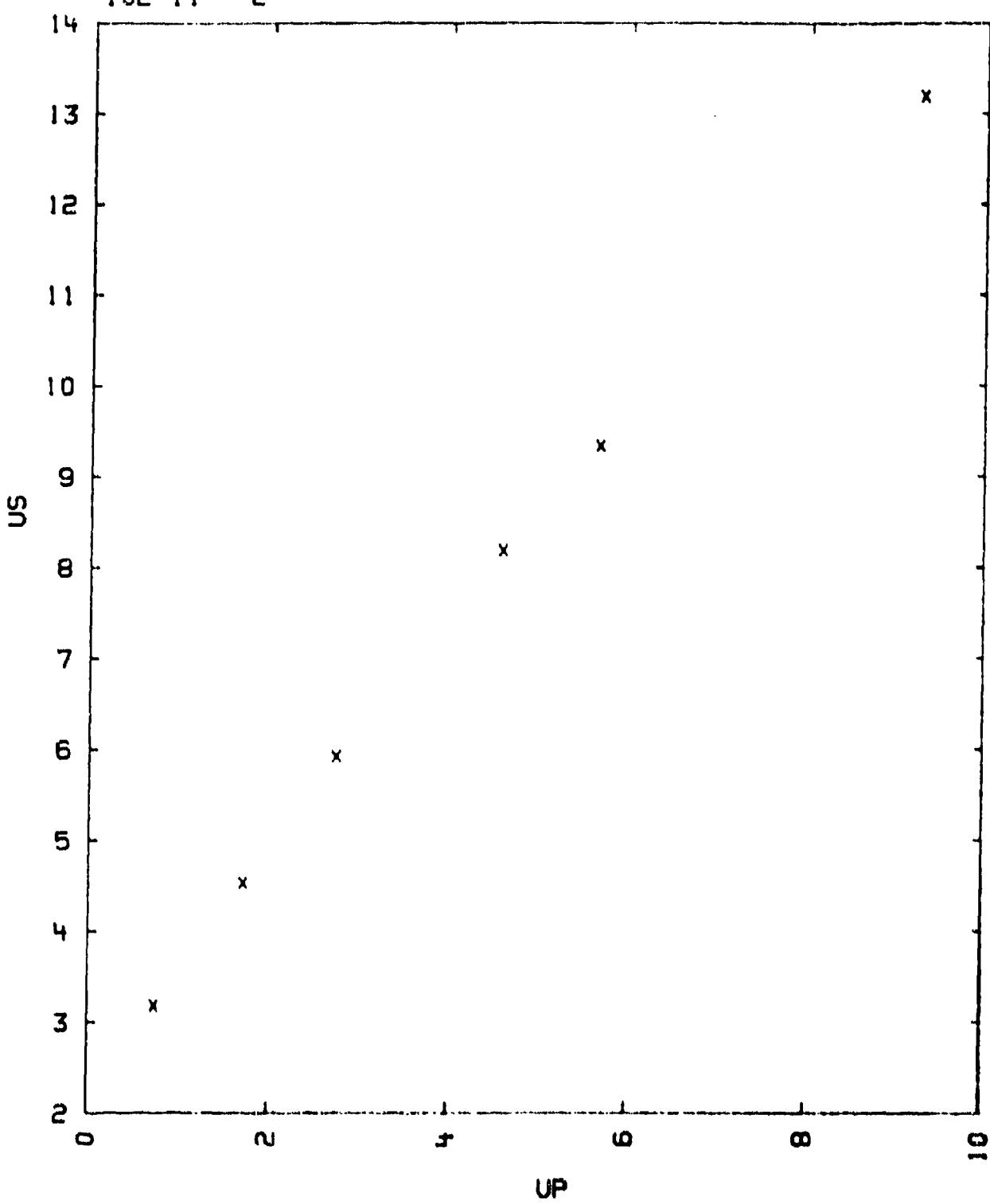
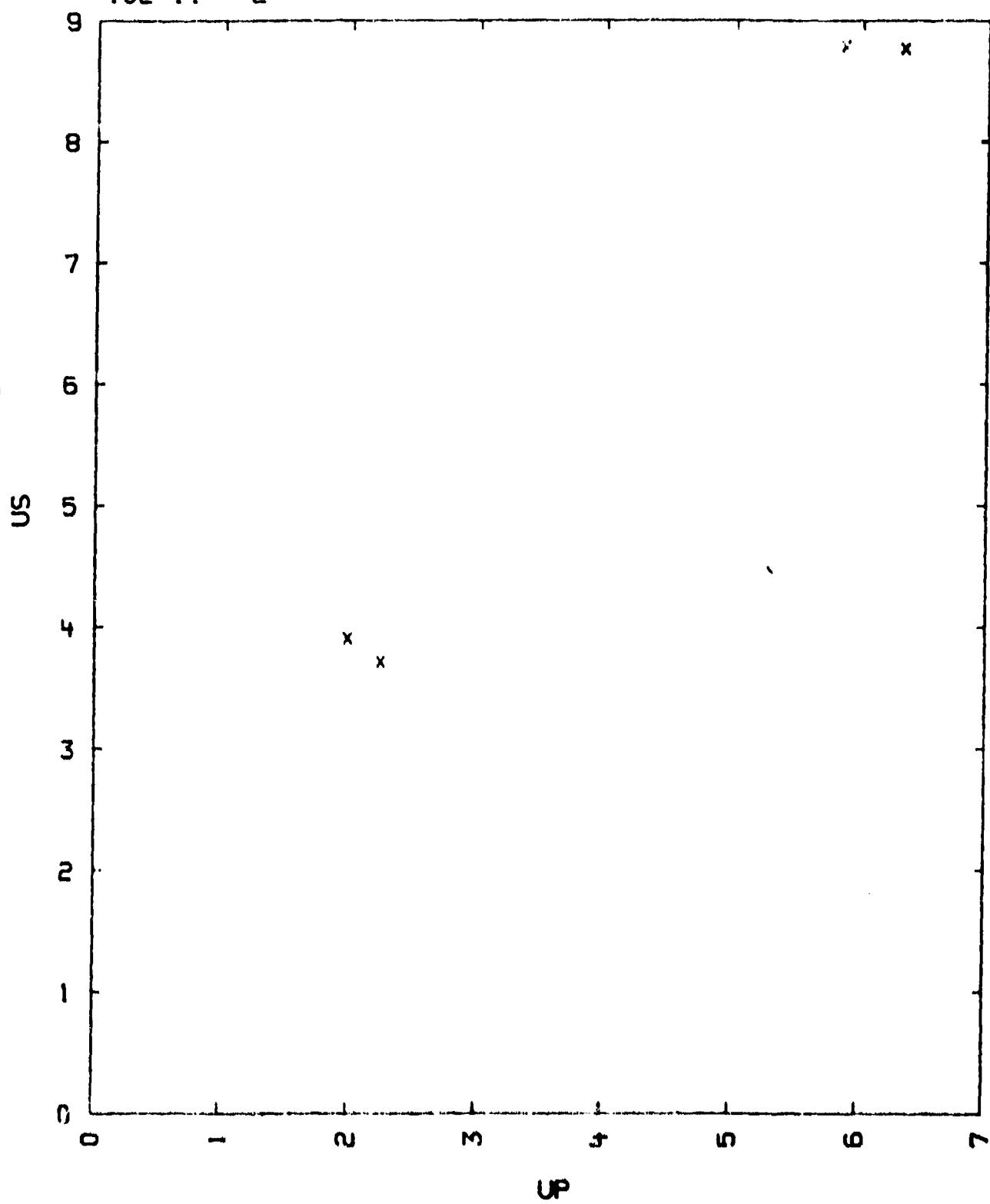


TABLE II

CESIUM BROMIDE
102-11--2



102-12---1
CESIUM IODIDE

CS-1

$V_0 = 0.2217 \text{ CC}/\text{O}$
 $V_{01} = 0.2208 \text{ CC}/\text{O}$

 $C_B = 1.54 \text{ KM}/\text{SEC}$

IN THE TABLE BELOW DENSITY IS GIVEN IN G/CC, VELOCITY IN KM/SEC AND PRESSURE IN KILOBARS. SH DESIGNATES SAMPLE HOLDER.

TABLE

RHO0	US	UP	P	V/V0	SH	UP(SH)
4.51	2.57	0.56	64.0	0.7837	CU	0.37
-	2.80	0.81	102.5	0.7137	AL	0.69
-	3.98	1.56	279.5	0.6086	AL	1.50
-	4.32	1.79	348.3	0.5848	AL	1.74
-	5.63	2.80	710.0	0.5025	AL	2.82
-	6.64	3.68	1100.2	0.4464	FE	2.80

 $US = 1.61 + 1.63 UP - 0.0706 UP^2 \text{ KM}/\text{SEC}$

FOR UP FROM 0.5 TO 3.7 KM/SEC

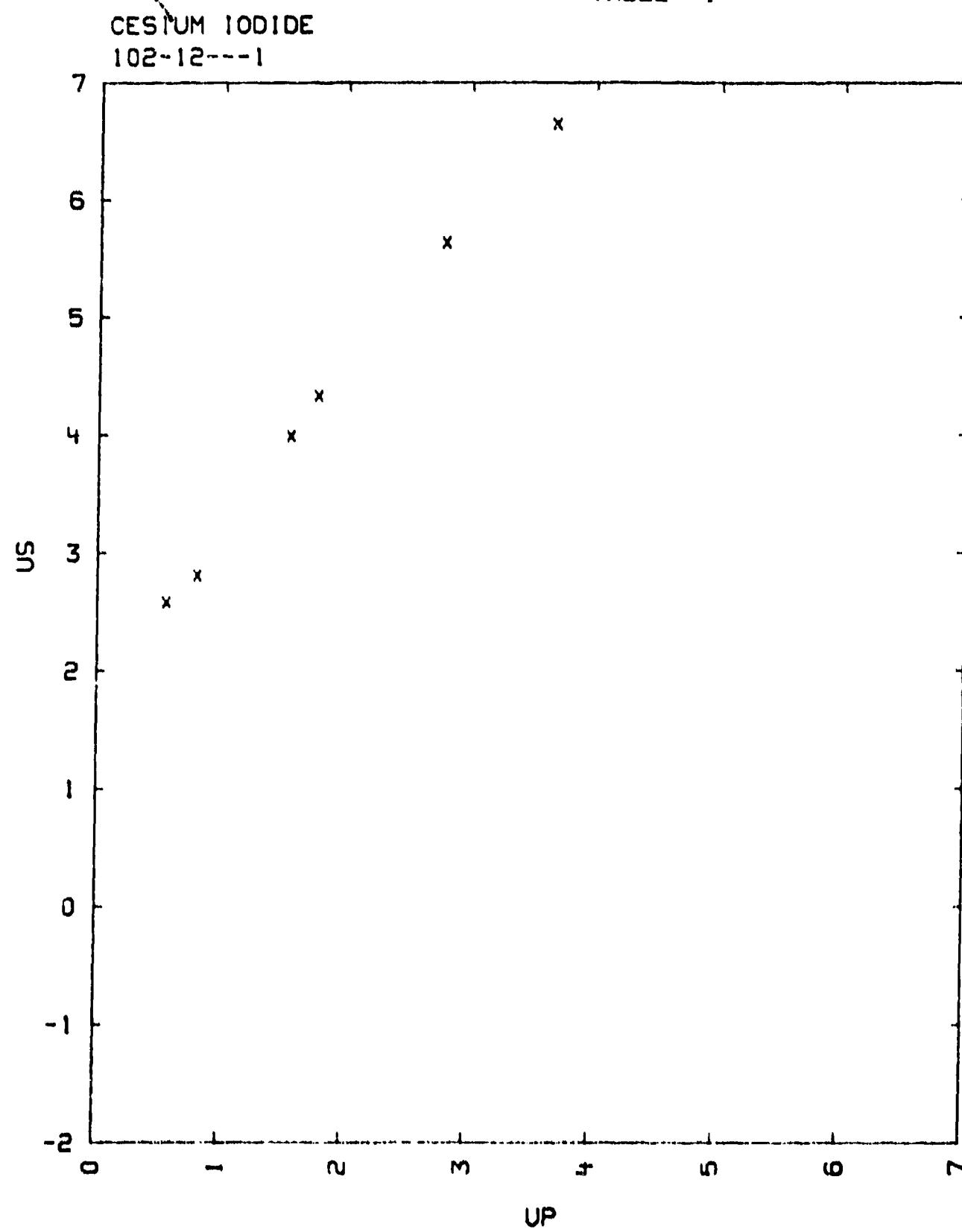
 $SIG US = 0.055$

COMMENTS:

- 1) SOURCE: AL'TSHULER, L.V., PAVLOVSKII, M.M., KULESHOVA, L.V., AND SIMAKOV, G.V.
SOVIET PHYS.-SOLID STATE, VOL. 5, P. 203 (1963)
- 2) EXPERIMENTAL TECHNIQUE A
DATA REDUCTION TECHNIQUE B.
- 3) THE SAMPLES WERE POSITIONED ON PLATES OF CU AL AND FE AS INDICATED IN TABLE COLUMN 6.
THE HUGONIOTS OF FE CU AND AL WERE OBTAINED FROM
AL'TSHULER, L.V., KORMER, S.B., BAKANOVA, A.A. AND TRUNIN, R.F.
JETP VOL 11, P.573 (1960)
- 4) THE AL AND CU ADIABAT WERE OBTAINED BY REFLECTING THE HUGONIOT IN THE
P VS UP PLANE. CORRECTIONS WERE MADE FOR FE.
- 5) OTHER CONSTANTS LISTED ARE: DEBYE TEMPERATURE 100 DEG. K
HEAT CAPACITY (CV) 0.185 J/G/DEG,
CATION TO ANION DISTANCE 3.950 KK
EXPANSION COEFFICIENT 0.000146 PER DEG
- 6) THE VALUE OF V_{01} WAS OBTAINED FROM A CATION TO ANION DISTANCE OF
3.955 A. A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSN.,
POLYCRYSTAL BOOK SERVICE, BROOKLYN 1963) 2ND ED.

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TABLE I



102-12---2
CESIUM IODIDE

CS-I SINGLE CRYSTAL

$V_0 = 0.223 \text{ CC}/\text{O}$
 $V_{OI} = 0.2208 \text{ CC}/\text{O}$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN MM/MICROSEC,
AND PRESSURE IN KILOBARS

TABLE

RHO0	US	UFS	UP	P	V/V0	PRESSURE IN AL BASE PLATE
4.481	3.12	1.96	1.00	140	0.680	160
4.493	3.51	-	1.23	195	0.649	220
4.481	3.95	-	1.32	233	0.665	298
4.481	4.19	3.62	1.72	323	0.590	345
4.486	3.24	1.98	0.98	144	0.694	164

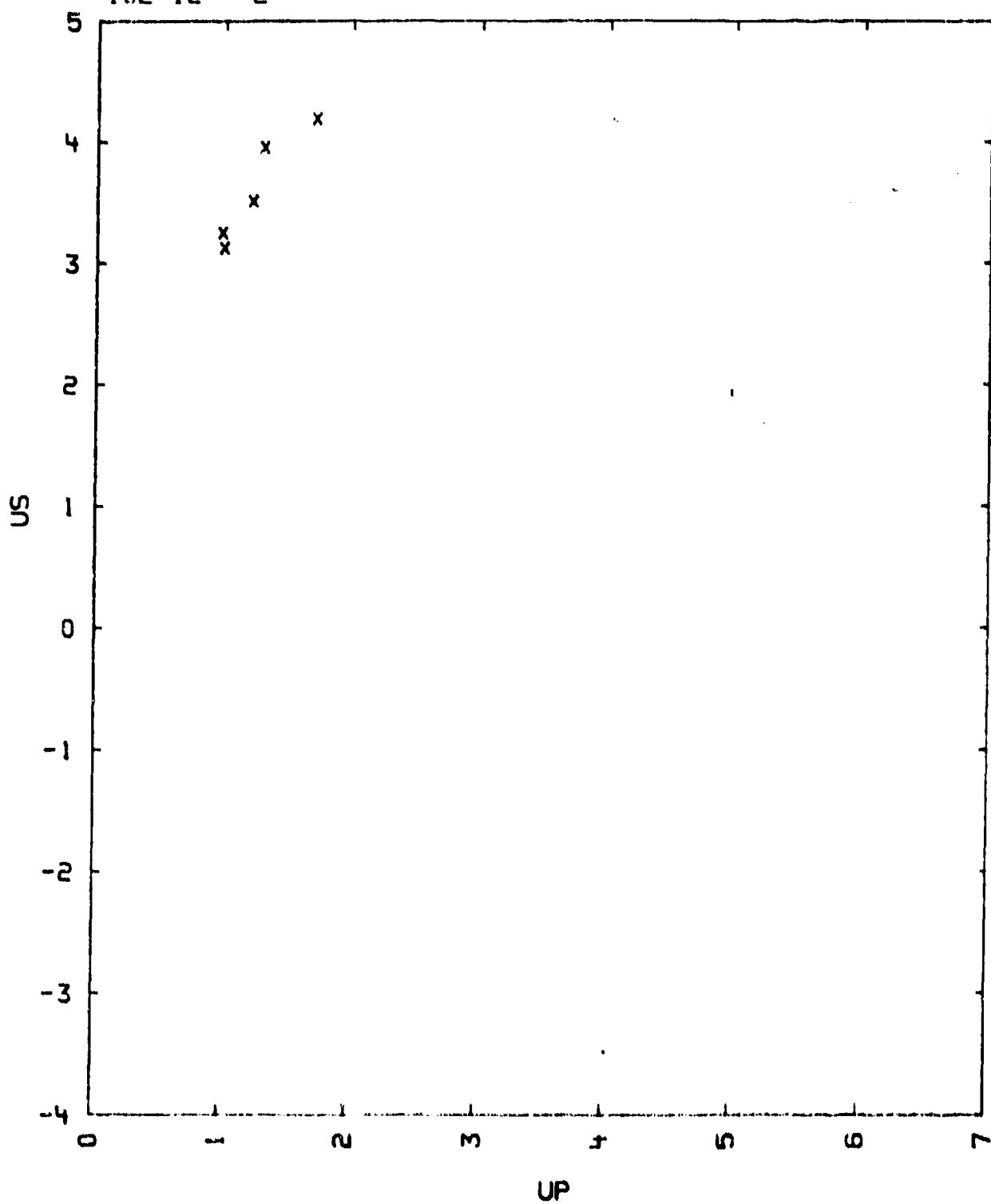
$US = 1.785 + 1.452 UP \text{ MM/MICROSEC}$
 $\text{SIGMA US} = 0.171$

COMMENTS:

- 1) SOURCE: COMPILER
 L. R. L. EQUATION OF STATE FILE
 LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA
- 2) EXPERIMENTAL TECHNIQUE B (ALUMINUM STANDARD BASE PLATE)
 DATA REDUCTION TECHNIQUE B.
- 3) PART OF THE TABULATED DATA ALSO REPORTED BY CHRISTIAN, R. H., IN
 EQUATION OF STATE OF ALKALI HALIDES AT HIGH PRESSURE (THESIS)
 UCRL-4900 MAY 16, 1957 UNIVERSITY OF CALIFORNIA,
 LAWRENCE RADIATION LABORATORY, LIVERMORE, CALIFORNIA.
- 4) ALSO LISTED IN REFERENCE OF COMMENT 3 ARE:
 DIEBYE TEMPERATURE 95 DEG. K
 HEAT CAPACITY (CV) 0.19 J/G/DEG.
 EXPANSION COEFFICIENT 0.000145 PER DEG.
 COMPRESSIBILITY 8.57 PER MEGABAR
 MELTING POINT 630 DEG. C
- 5) THE VALUE OF V01 WAS OBTAINED FROM A LATTICE CONSTANT OF 4.5687 A
 A.C.A. MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
 POLYCRYSTAL BOOK SERVICE 1963) 2ND EDITION.

TABLE I

CESIUM IODIDE
102-12---2



102-12---3
CESIUM IODIDE

CS-1

$$V_0 = 0.222 \text{ CC/G}$$

$$V_{01} = 0.2208 \text{ CC/G}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC,
AND PRESSURE IN KILOBARS.

TABLE

SAMPLE					BASE PLATE	
RHO0	US	UP	P	V/V0	MATERIAL	UP
4.51	7.08	3.90	1245	0.449	AL	4.03
-	7.60	4.30	1474	0.434	FE	3.34
-	9.31	5.88	2469	0.368	SN	4.55
-	13.26	9.28	5540	0.300	AL	7.96

$$US = 2.63 + 1.14 UP \text{ KM/SEC}$$

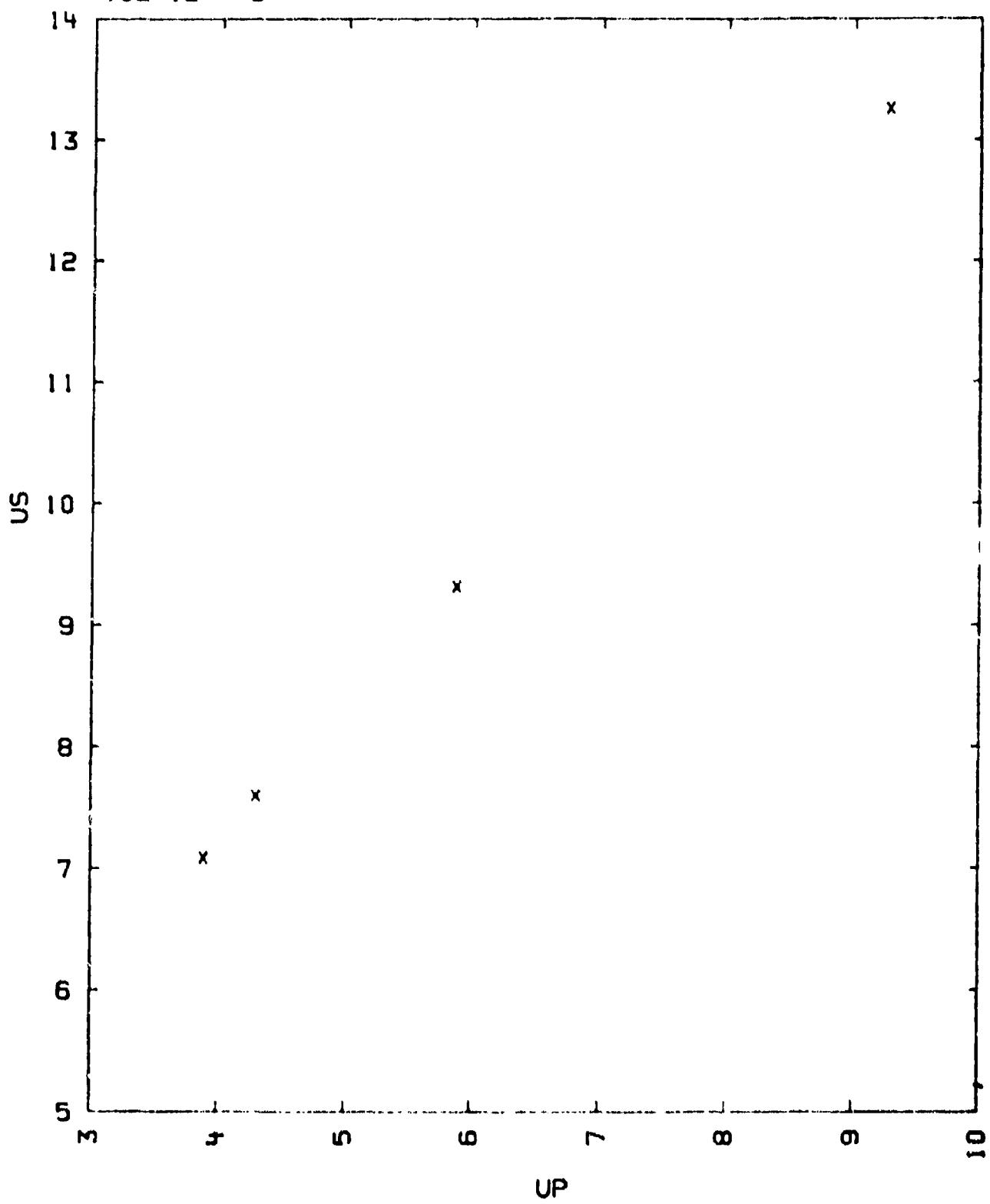
$$\text{SIGMA US} = 0.050 \text{ KM/SEC}$$

COMMENTS:

- 1) SOURCE: PAVLOVSKII, M. N., VASHCHENKO, V. YA., SIMAKOV, G. V.
FIZ VOL. 7, P. 1212 (1965).
SOVIET PHYSICS-SOLID STATE VOL. 7, P. 972 (1965) (TRANS.).
- 2) EXPERIMENTAL TECHNIQUE A.
DATA REDUCTION TECHNIQUE B
- 3) THE VALUE OF V01 WAS OBTAINED FROM A LATTICE CONSTANT OF 4.5667 Å
A.C.A. MONOGRAPH NO.5, CRYSTAL DATA DETERMINATIVE TABLES
(AMERICAN CRYSTALLOGRAPHIC ASSOCIATION, 1963) 2ND EDITION.

TABLE I

CESIUM IODIDE
102-12---3



102-12--4
CESIUM IODIDE, POROUS

CS-1

$$\rho_0 = 0.398 \text{ CC/G}$$

$$\rho_{01} = 0.2208 \text{ CC/G}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC,
AND PRESSURE IN KILOBARS.

TABLE

SAMPLE			BASE PLATE			
RHO0	US	UP	P	V/V0	MATERIAL	UP
2.51	2.07	1.04	54	0.500	AL	0.69
-	2.88	1.60	116	0.451	AL	1.14
-	3.59	2.00	180	0.443	AL	1.50
-	3.42	3.41	463	0.371	AL	2.70
-	5.55	3.34	465	0.383	AL	2.82
-	6.56	4.23	697	0.355	FE	2.80
-	6.77	4.44	754	0.344	AL	3.71
-	6.99	4.66	817	0.337	FE	3.08
-	9.59	6.75	1620	0.296	FE	4.55

$$US = 0.89 + 1.32 UP \text{ KM SEC}$$

$$\Sigma US = 0.157 \text{ KM/SEC}$$

COMMENTS:

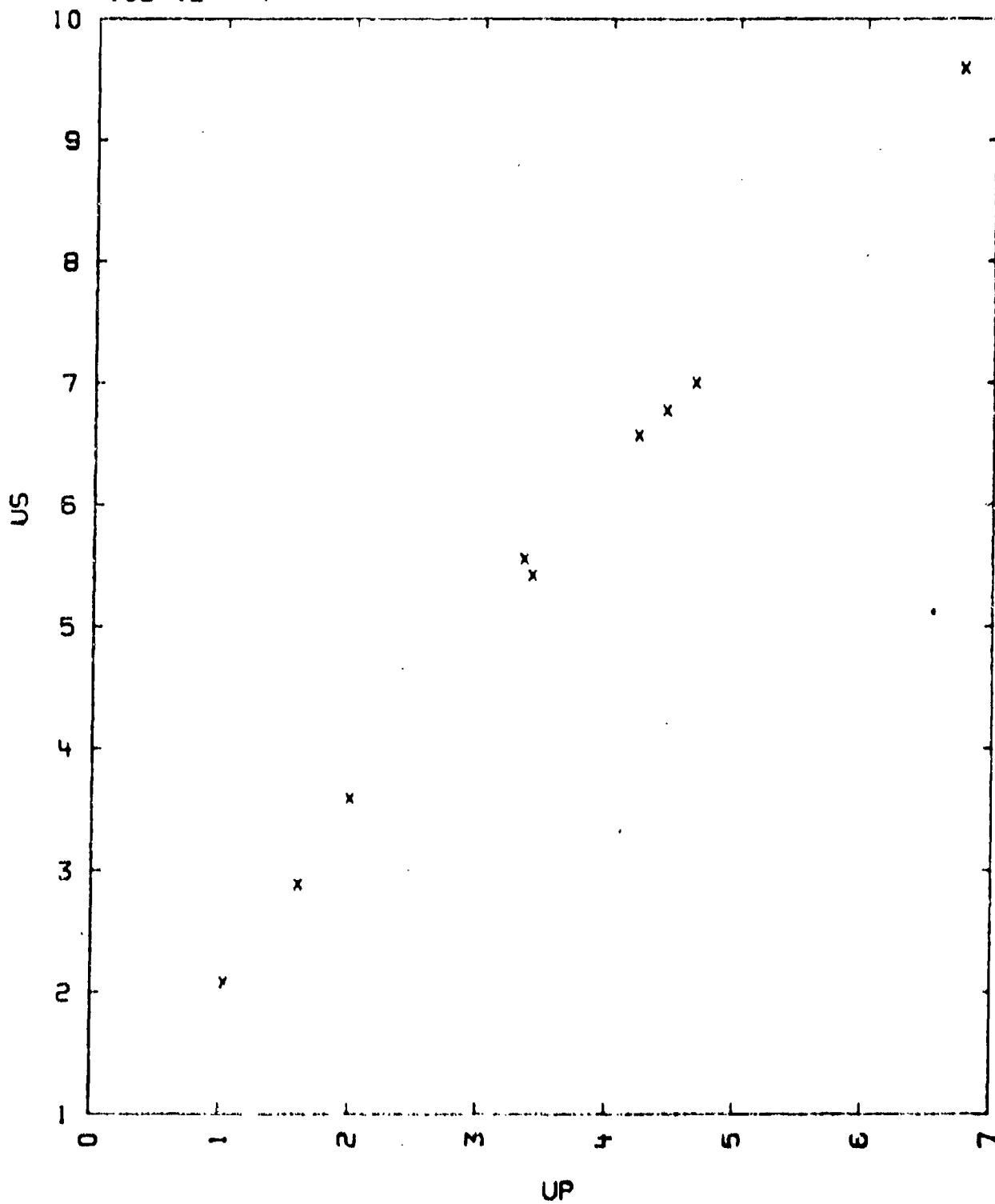
- 1) SOURCE: PAVLOVSKII, M. N., VASHCHENKO, V. YA., SIMAKOV, G. V.
FIZ VOL. 7, P. 1212 (1965).
SOVIET PHYSICS-SOLID STATE VOL. 7, P. 972 (1965)
- 2) EXPERIMENTAL TECHNIQUE A.
DATA REDUCTION TECHNIQUE B
- 3) THE VALUE OF V01 WAS OBTAINED FROM A LATTICE CONSTANT OF 4.5667 A
A.C.A. MONOGRAPH NO.5, CRYSTAL DATA DETERMINATIVE TABLES
(AMERICAN CRYSTALLOGRAPHIC ASSOCIATION, 1963) 2ND EDITION.

U06/14/77

TABLE I

CESIUM IODIDE, POROUS

102-12---4



EDIT TEST

BOX V72 PLTR

TV80LIB DD80 OUTPUT..... 12:35:47U 06/14

309 FRAMES PLOTTED

UNCL

BOX V72 PLTR

15:48:15 06/14/77U

XEROX+FILM

EDIT TEST

BOX V72 PLTR

TV80LIB DD80 OUTPUT..... 12:46:34U 06/14

EDIT TEST

BOX V72 PLTR

TV80LIB DD80 OUTPUT..... 12:46:34U 06/14

SECTION B

HYDROCARBONS

U06/14/77

23-812-4)---1
POLYETHYLENE



$$V_0 = 1.09 \text{ CC}/\text{O}$$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN MM/MICROSEC., AND PRESSURE IN KILOBARS.

TABLE

RHO0	US	UP	P	V/V0
.917	1.86	0.115	1.96	.9382
-	1.90	0.170	2.95	.9105
-	3.14	0.625	18.1	.8010
-	4.80	1.33	58.8	.723
-	4.88	1.44	64.5	.705

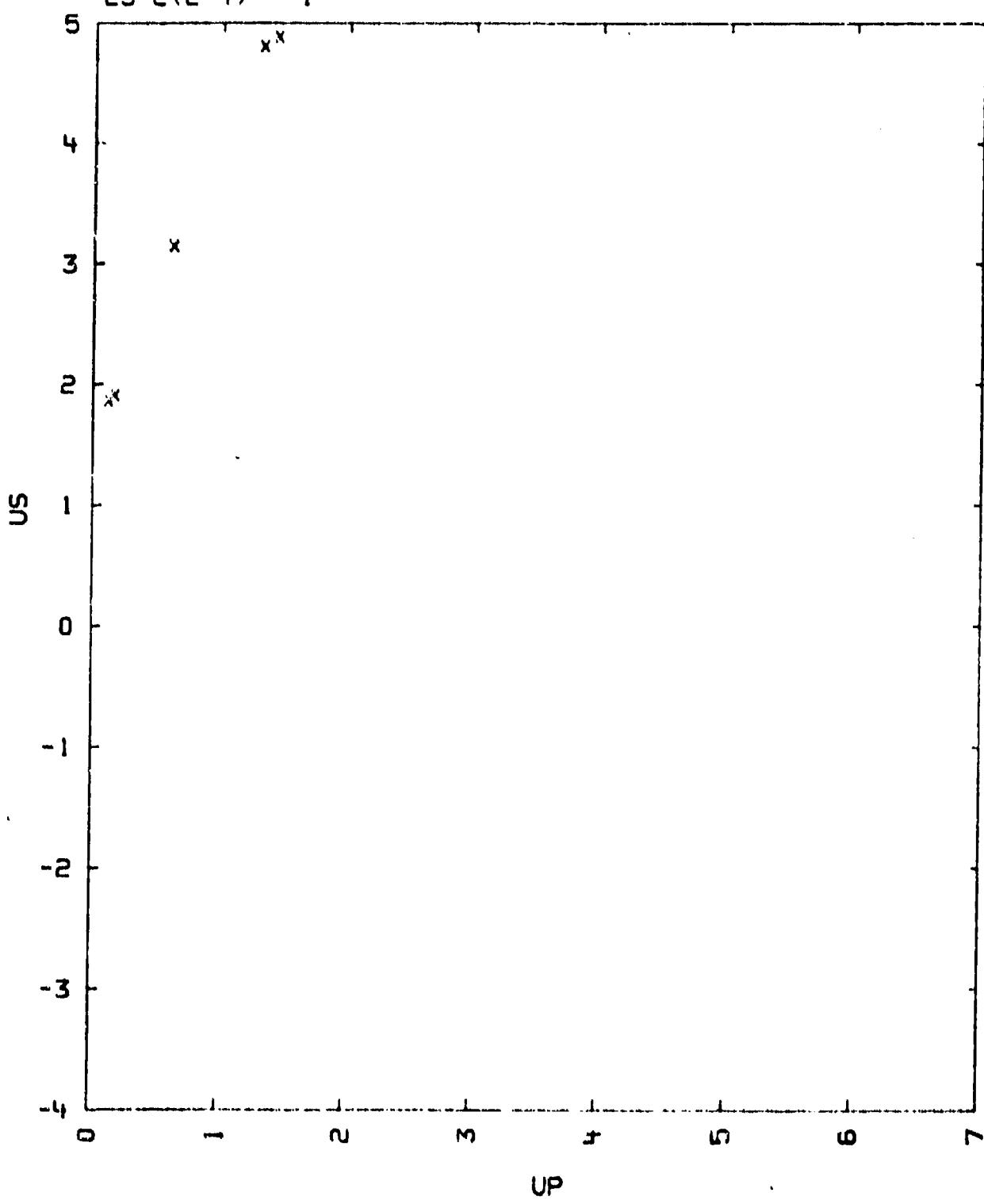
$$US = 1.57 + 2.37 UP \text{ KM/SEC. SIG.US} = 0.1 \text{ KM/SEC.}$$

COMMENTS:

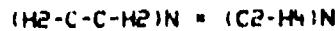
- 1) SOURCE: WAGNER, M. H., WALDORF, W. F. AND LOUIE, N. A.
REPORT NO. AFSC-TDR-62-66, VOL. I (1962)
WORK DONE AT DOWNEY, CALIFORNIA.
- 2) EXPERIMENTAL TECHNIQUE A
DATA REDUCTION TECHNIQUE B
IN THE TABLE UP = (1/2)UFS.
- 3) ACCURACY IS LIMITED BECAUSE ASSEMBLY DIMENSIONS ALLOW RELATIVELY
LARGE DEVIATIONS FROM ONE-DIMENSIONALITY.

TABLE I

POLYETHYLENE
23-2(2-4)---1



23-212-41---2
POLYETHYLENE GAMMA-IRRADIATED



$$V_0 = 1.082 \text{ TO } 1.096 \text{ CC/G}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC., VELOCITIES IN KM/SEC., AND PRESSURE IN KILOBARS.

TABLE

RHO _U	US	UP	P	V/V ₀
0.918	7.25	2.89	192.4	0.601
-	6.91	2.62	166.	0.621
-	6.32	2.29	132.9	0.638
-	6.05	2.11	117.	0.651
-	5.90	1.98	107.2	0.664
-	5.66	1.81	94.0	0.680
-	5.66	1.81	94.0	0.680
-	5.63	1.81	93.5	0.679
-	5.62	1.81	93.4	0.678
-	5.63	1.81	93.5	0.678
-	5.17	1.59	75.5	0.693
-	5.04	1.47	68.0	0.708
-	4.65	1.23	52.5	0.735
-	4.58	1.25	52.6	0.727
-	4.02	0.83	30.6	0.794
-	4.00	0.80	29.4	0.800
-	3.92	0.82	29.5	0.792
-	3.45	0.44	13.9	0.872
-	3.44	0.44	13.9	0.872

$$US = 2.704 + 1.594 \cdot UP \text{ KM/SEC.}$$

$$S10 US = 0.055 \text{ KM/SEC.}$$

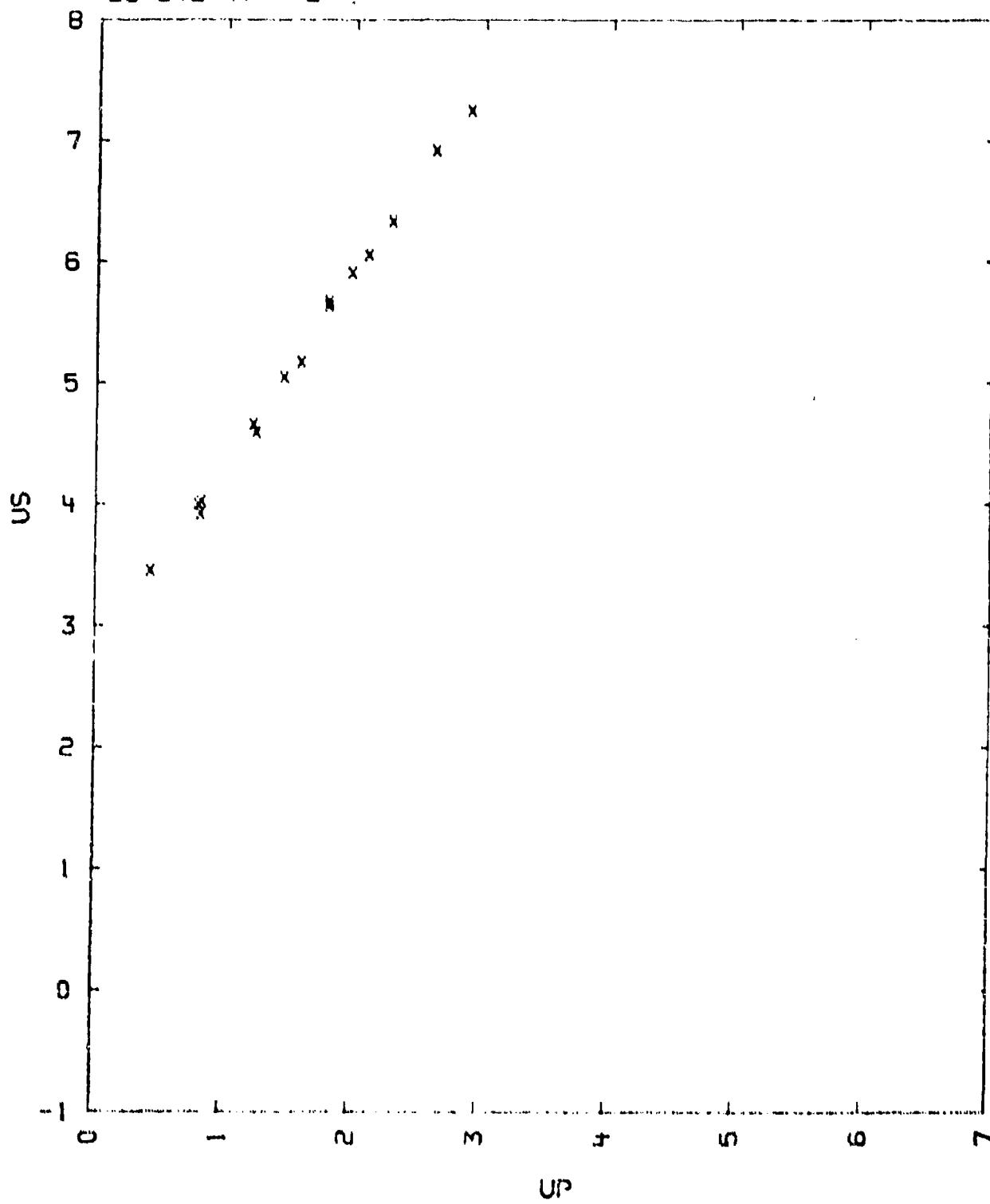
COMMENTS:

- 1) SOURCE: HAUVER, O. E.
TECHNICAL NOTE NO. 162B (1966)
PRIVATE COMMUNICATION JAN. 1969
BALLISTIC RESEARCH LABORATORIES, ABERDEEN PROVING GROUND,
MARYLAND.
- 2) EXPERIMENTAL TECHNIQUE A.
DATA REDUCTION TECHNIQUE B.
STANDARD MATERIAL ALUMINUM 2024 ALLOY.
AND PLEXIGLASS: US = $2.702 + 1.544 \cdot UP$ KM/SEC.
 $\rho_{HO} = 1.18 \text{ G/CC.}$
- 3) THE SAMPLES WERE 3.18 MM THICK AND 12.70-MM IN DIAMETER. THE SURFACES
WERE FLAT AND PARALLEL TO WITHIN A SIGMA OF 0.002 MM.
- 4) THE SAMPLES WERE IRRADIATED WITH A COBALT-60 GAMMA SOURCE. THE

SAMPLES RECEIVED DOSES THAT RANGED FROM 0-2.0110¹⁰ RAD. IT WAS CONCLUDED THAT THE RADIATION DOSES USED DID NOT PRODUCE ANY MEASURABLE CHANGE IN THE HUGONIOT.

- 5) SAMPLES OF PLEXIGLASS AND POLYETHYLENE WERE PLACED ON A 2024 ALUMINUM PLATE. THE AL RELEASE CURVE WAS TAKEN TO BE A MIRROR IMAGE OF THE HUGONIOT: RICE ET. AL., SOLID STATE PHYSICS, VOL 6 (ACADEMIC PRESS, NEW YORK, 1958) PAGE 1FF. THE PLEXIGLAS HUGONIOT POINT ESTABLISHED THE POSITION OF THE CROSS CURVE.
INTERMEDIATE PRESSURES WERE OBTAINED BY PLACING DISKS OF 23B BRASS MO AND W DISKS BETWEEN THE POLYETHYLENE SAMPLES AND THE AL PLATE. ALL CROSS CURVES WERE REFLECTED HUGONIOTS.

TABLE I

POLYETHYLENE GAMMA-IRRADIATED
23-2(2-4)---2

23-212-41---3
POLYETHYLENE (ALATHON 7050)

$\text{INR-C-C-H}_2\text{IN} + \text{IC}_2\text{-H}_4\text{IN}$

$$V_0 = 1.04 \text{ CC/0}$$

THE TABLE LISTS DENSITY IN G/CC., VELOCITIES IN KM/SEC., AND PRESSURE IN KBAR.

TABLE

RHO0	US	UP	P	V/V0
0.96	7.09	2.55	174.	0.640
-	5.81	1.80	100.	0.690
-	5.05	1.24	60.1	0.754
-	4.31	0.79	32.7	0.817
-	3.74	0.44	15.8	0.882

$$\text{US} = 3.06 + 1.57 \cdot \text{UP} \text{ KM/SEC.}$$

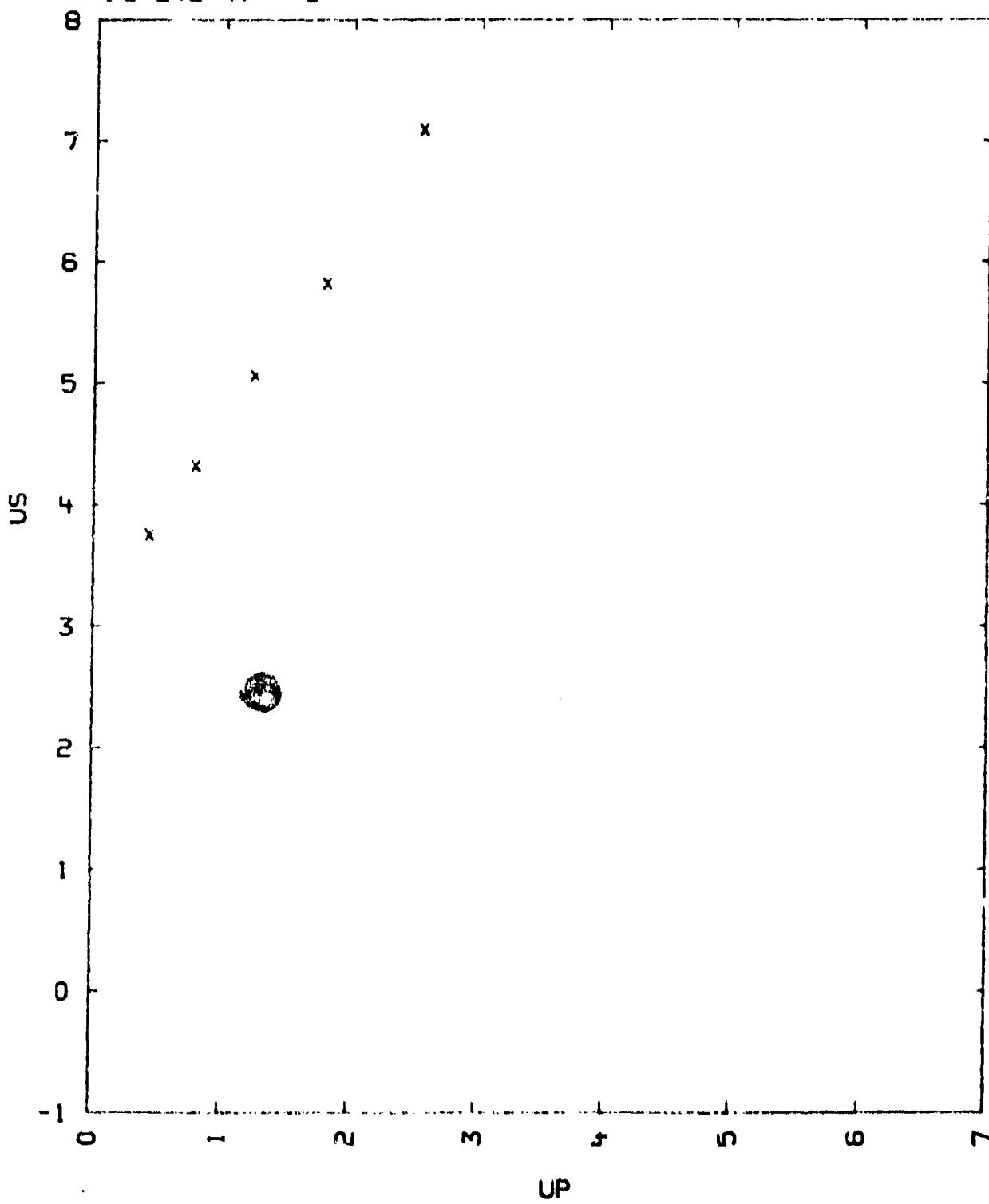
$$\text{SIG US} = 0.053 \text{ KM/SEC.}$$

COMMENTS:

- 1) SOURCE: MAUER, G. F. AND MELLANI, A.
PRIVATE COMMUNICATION, JAN 1969
BALLISTICS RES. LAB., ABERDEEN PROVING GROUNDS
MARYLAND, USA.
- 2) EXPERIMENTAL TECHNIQUE: H
DATA REDUCTION TECHNIQUE: B
STANDARD MATERIAL: PLEXIGLAS
 $\text{UP} = 2.02 + 0.94 \cdot \text{UP}$ KM SEC. $\text{RHOO} = 1.18 \text{ G/CC.}$
- 3) THE SAMPLES AND STANDARD ARE PLACED ON AN ALUMINUM PLATE. THE RELEASE CURVE OF THE AL PLATE WAS DETERMINED FROM THE PLEXIGLAS SHOCK VELOCITY.

TABLE I

POLYETHYLENE (ALATHON 7050)
23-2(2-4)---3



23-212-41--4
POLYETHYLENE

(H₂-C-C-H₂)_n = (C₂H₄)_n

$$V_0 = 1.066 \text{ CC/G}$$

THE TABLE LISTS STRESS IN KBAR., VELOCITIES IN KM/SEC., AND DENSITY IN G/CC. N. IS THE NUMBER OF EXPERIMENTS THAT DETERMIN THE POINT. MAT IS THE PROJECTILE MATERIAL AND U IS VELOCITY BEFORE IMPACT. POLY = POLY-ETHYLENE.

TABLE

N	RHO ₀	SAMPLE				STANDARD	
		U _S	U _P	P	V/V ₀	U	MAT
1	0.938	2.96	0.396	11.0	0.866	0.749	POLY
1	-	2.81	0.573	9.85	0.867	0.722	-
1	-	2.52	0.230	5.44	0.9087	0.282	AL
4	-	2.08	0.161	3.15	0.9224	0.306	POLY
1	-	2.15	0.115	2.32	0.9465	0.260	-

$$U_S = 1.71 + 3.01 \cdot U_P \text{ KM/SEC.}$$

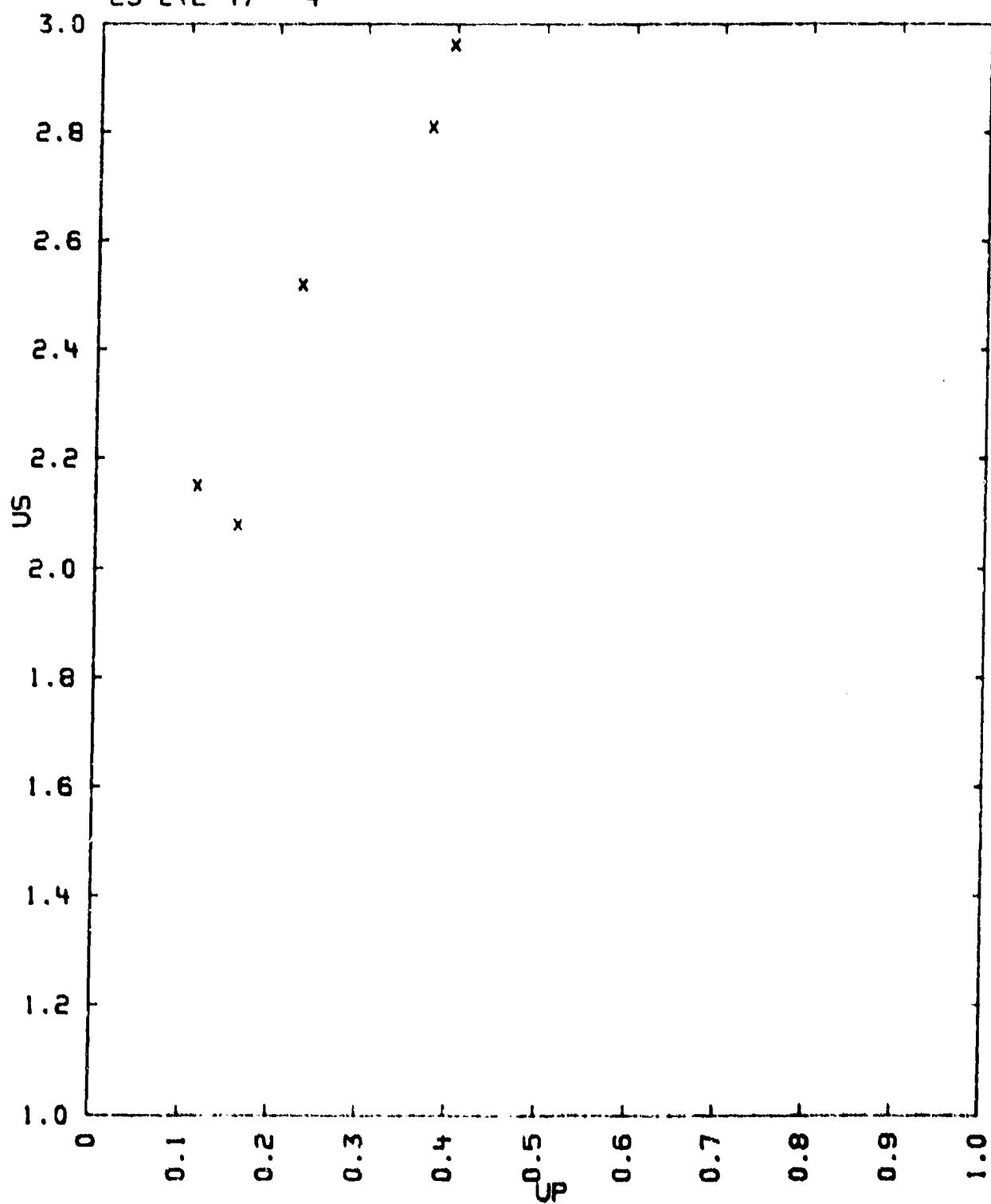
$$S10.U_S = 0.11 \text{ KM/SEC.}$$

COMMENTS:

- 1) SOURCE: ANDERSON G. D., MURRI H. J., ALVERSON R. C., HANAGUD S. V.
TECHNICAL REPORT AFWL-TR-67-24
STANFORD RES. INST., MENLO PARK, CALIF., U.S.A.
- 2) EXPERIMENTAL TECHNIQUE: II AND A
DATA REDUCTION TECHNIQUE: C
- 3) THE UNCERTAINTY IN P MAY BE ESTIMATED TO BE ABOUT PLUS OR MINUS 5
PERCENT FROM THE 4 EXPERIMENTS (7 POINTS) DETERMINING THE 4TH TABLE
ENTRY. THE MAXIMUM UNCERTAINTY IN U_S IS ABOUT 10 PERCENT
- 4) THE WAVES SHOWED A BROAD SHOCK FRONT WITH AN INITIAL STRESS INCREASE
TO 0.8P IN ABOUT 0.03 MICROSECONDS FOLLOWED BY A SLOWER RISE TO
THE MAXIMUM STRESS LISTED IN THE TABLE. THE VALUES OF U_P AND V/V₀
CALCULATED FROM THE RANKINE-HUGONIOT CONDITIONS FOR A SINGLE STRESS
STEP ARE THEREFORE ONLY NOMINAL VALUES.

TABLE I

POLYETHYLENE
23-2(2-4)---4



25-212-4)---5

PARAFFIN

H₃-C-(C(H₂))N-C-H₃

$$V_0 = 1.09 + 1.11 \text{ CC}/\text{O}$$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC, PRESSURE IN KILOBARS
AND DENSITY IN G/CC.

TABLE

-----SAMPLE-----					----STANDARD----		
RHO0	US	UP	P	V/V0	MATERIAL	US(ST)	
0.919	4.47	1.06	44.	0.7629	2024 AL	6.22	
0.904	5.00	1.32	60.	0.7360	2024 AL	6.46	
0.918	5.15	1.39	66.	0.7301	2024 AL	6.53	
0.918	4.97	1.41	64.	0.7163	2024 AL	6.53	
0.919	5.41	1.46	73.	0.7301	2024 AL	6.60	
0.918	5.75	1.81	96.	0.6852	2024 AL	6.91	
0.919	5.88	1.81	98.	0.6922	2024 AL	6.92	
0.904	6.49	2.43	143.	0.6256	2024 AL	7.48	
0.918	6.75	2.47	153.	0.6341	2024 AL	7.54	
0.919	6.67	2.51	154.	0.6237	2024 AL	7.57	
0.919	7.05	2.53	154.	0.6411	2024 AL	7.61	
0.918	7.25	2.90	193.	0.6000	2024 AL	7.95	
0.918	7.81	3.18	228.	0.5928	2024 AL	8.24	
0.918	8.13	3.31	247.	0.5929	2024 AL	8.38	
0.919	8.55	3.68	289.	0.5646	2024 AL	8.74	
0.918	8.58	3.70	291.	0.5688	2024 AL	8.76	
0.919	9.02	3.86	320.	0.5721	CU	7.30	
0.918	9.43	4.08	353.	0.5673	2024 AL	9.16	
0.919	9.13	4.10	344.	0.5509	2024 AL	9.16	
0.919	9.71	4.31	385.	0.5561	2024 AL	9.39	
0.919	10.39	4.60	439.	0.5573	CU	8.00	
0.919	10.17	4.63	433.	0.5447	2024 AL	9.72	
0.919	10.09	4.74	440.	0.5302	CU	8.13	
0.918	10.93	5.08	530.	0.5169	2024 AL	10.35	
0.919	10.76	5.30	524.	0.5074	2024 AL	10.36	
0.919	10.83	5.33	530.	0.5078	2024 AL	10.39	

$$US = 2.980 + 1.531 \cdot UP \text{ KM/SEC}$$

$$\text{SIOMA US} = 0.173 \text{ KM/SEC}$$

COMMENTS:

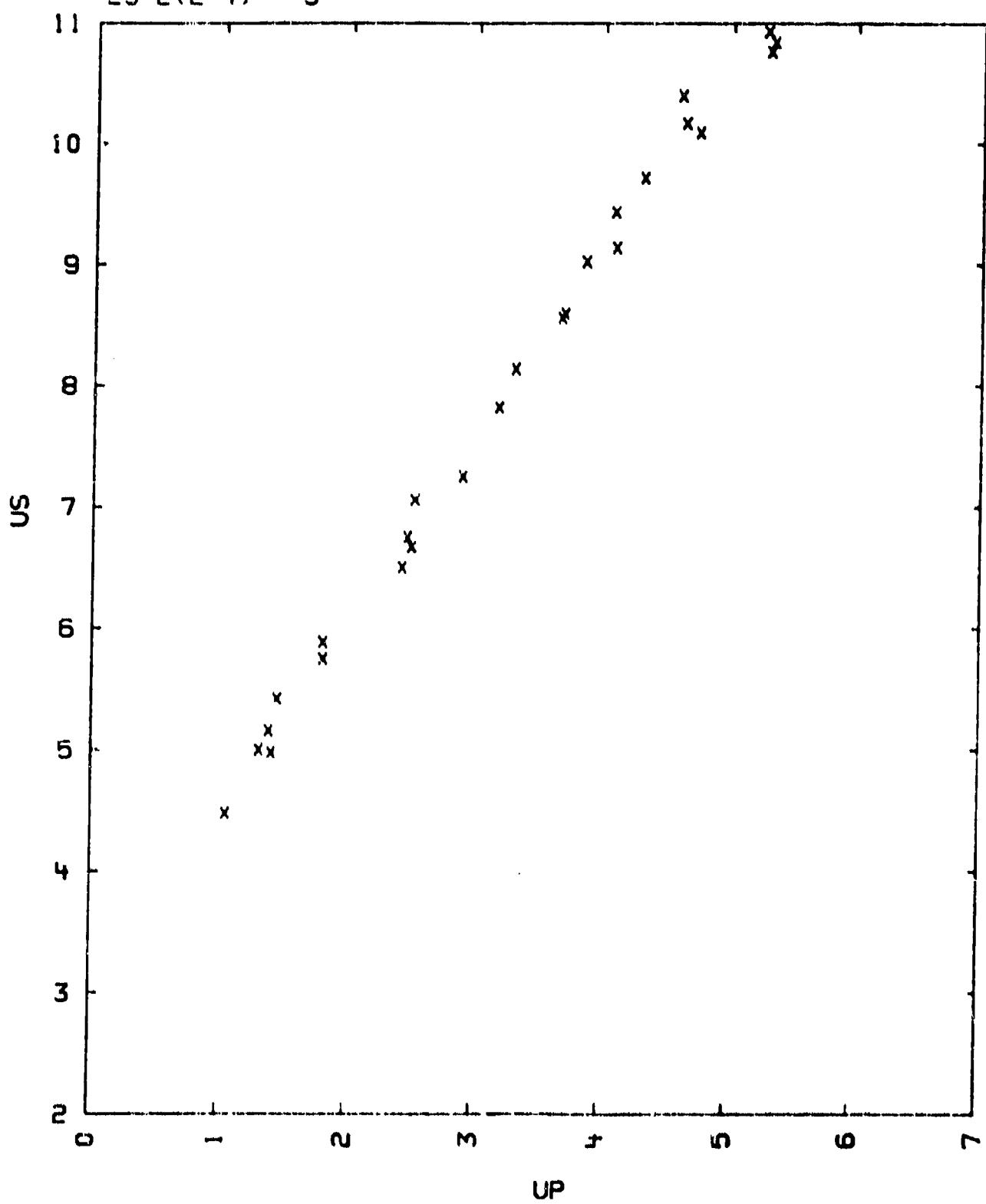
- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.H., FRITZ, J.H.,
AND CARTER, H.J.
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.), ACADEMIC
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE : B

DATA REDUCTION TECHNIQUE : B

U06/14/77

TABLE I

PARAFFIN
23-2(2-4)---5



23-212-41--6
POLYETHYLENE

IC2-H4 IN

$V_0 = 1.095 \text{ CC}/\text{G}$

$C_L = 2.04 \text{ KM}/\text{SEC}$

$C_0 = 1.89 \text{ KM}/\text{SEC}$

$V_0 = 1.034 \text{ CC}/\text{G}$

$C_S = 0.66 \text{ KM}/\text{SEC}$

$C_0 = 2.22 \text{ KM}/\text{SEC}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBARS
AND DENSITY IN G/CC.

TABLE

-----SAMPLE----- STANDARD-----

RHO0	US	UP	UFS	P	V/V0	MATERIAL US(ST)
0.913	4.70	1.17		50.	0.751	2024 AL 6.32
0.920	4.98	1.40		64.	0.719	2024 AL 6.53
0.916	5.01	1.48	2.805	68.	0.705	921-T AL 6.40
0.916	5.01	1.49	-	68.	0.703	921-T AL 6.40
0.913	5.43	1.72		85.	0.683	2024 AL 6.81
0.916	5.60	1.77		91.	0.684	2024 AL 6.87
0.916	5.63	1.83	3.562	94.	0.675	921-T AL 6.74
0.916	5.57	1.83	-	93.	0.671	921-T AL 6.74
0.913	6.17	2.23		126.	0.639	2024 AL 7.29
0.909	6.15	2.35		131.	0.618	2024 AL 7.40
0.913	6.49	2.41		143.	0.629	2024 AL 7.47
0.916	6.54	2.44		146.	0.627	2024 AL 7.50
0.916	6.58	2.46	4.821	148.	0.626	921-T AL 7.38
0.916	6.58	2.46		148.	0.626	921-T AL 7.38
0.916	6.67	2.49	4.906	152.	0.627	921-T AL 7.41
0.916	6.64	2.50	-	152.	0.623	921-T AL 7.41
0.916	6.63	2.52	4.960	153.	0.620	921-T AL 7.44
0.916	7.47	3.04		208.	0.593	2024 AL 8.09
0.916	7.56	3.08	6.200	213.	0.593	921-T AL 8.02
0.916	7.51	3.09	-	213.	0.588	921-T AL 8.02
0.916	8.42	3.66		282.	0.565	2024 AL 8.71
0.916	8.41	3.77		290.	0.552	2024 AL 8.78
0.916	9.07	4.11	8.352	341.	0.547	921-T AL 9.11
0.916	9.04	4.12	-	341.	0.544	921-T AL 9.11
0.916	9.03	4.14		342.	0.541	2024 AL 9.17
0.916	8.98	4.15		341.	0.538	2024 AL 9.18
0.916	9.55	4.21		393.	0.528	2024 AL 9.55
0.916	9.57	4.53		397.	0.527	2024 AL 9.58
0.916	9.97	4.03		441.	0.515	2024 AL 9.86

US = 2.901 + 1.481 * UP KM/SEC

SIOMA US = 0.074 KM/SEC

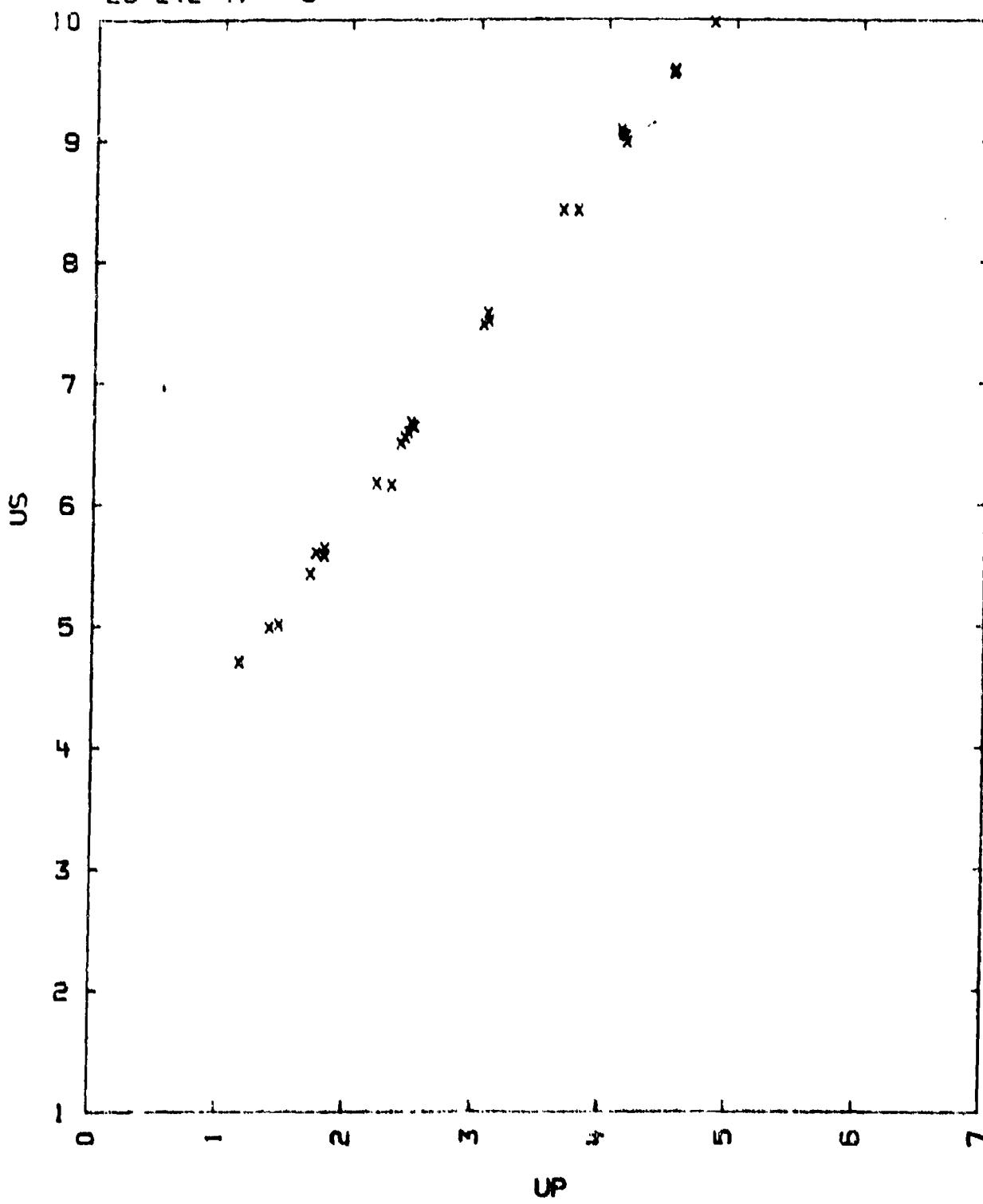
COMMENTS:

U08/14/77

- 1) SOURCE: MCQUEEN, R.G., MARSH, S.P., TAYLOR, J.W., FRITZ, J.M.,
AND CARTER, W.J.
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.) (ACADEMIC
PRESS, NEW YORK, 1970) CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: B
DATA REDUCTION TECHNIQUE: B (STANDARD BASE PLATE AS SHOWN)
- 3) THE SMALL VALUES OF UFS INDICATE THAT THE SHOCKED SAMPLES DECOMPRESS
TO A DENSITY LARGER THAN RHO0.
- 4) $V(DP/DE) = 1.64$

TABLE I

POLYETHYLENE
23-2(2-4)---6



23-2(6-6)---1

BENZENE

C6-H6 99. WT. PERCENT

T0 = 12 TO 30 DEG. C
V0 = 1.127 TO 1.152 CC/G

CD(22 DEG. C.) = 1.31 KM/SEC.

THE TABLE LISTS TEMPERATURE IN DEG. C., VELOCITIES IN KM/SEC., DENSITY IN G/CC. AND PRESSURE IN KBAR. US AND DUP ARE THE UNCERTAINTIES IN US AND UP

TABLE

T	RH00	SAMPLE					P	V/V0	STANDARD	
		US	DUS	UP	DUP	US(ST)			US(ST)	DUS(ST)
22	0.877	2.78	0.01	0.61	0.09	15.	0.779	5.93	0.07	
29	0.869	2.72	0.01	0.73	0.04	17.	0.730	6.02	0.03	
28	0.870	2.96	0.02	0.73	0.05	19.	0.753	6.02	0.04	
28	0.870	3.31	0.01	0.90	0.03	26.	0.730	6.16	0.04	
24	0.875	3.44	0.01	0.97	0.03	29.	0.719	6.22	0.03	
20	0.879	3.47	0.01	0.98	0.04	30.	0.719	6.23	0.03	
19	0.880	3.85	0.01	1.22	0.03	41.	0.684	6.43	0.02	
32	0.866	3.89	0.01	1.31	0.02	44.	0.663	6.50	0.02	
14	0.885	4.05	0.01	1.31	0.03	47.	0.676	6.52	0.02	
22	0.877	4.05	0.01	1.34	0.03	47.	0.669	6.54	0.02	
18	0.881	4.09	0.01	1.45	0.09	52.	0.646	6.62	0.07	
29	0.869	4.38	0.01	1.63	0.03	62.	0.627	6.78	0.02	
29	0.869	4.52	0.01	1.72	0.01	67.	0.620	6.86	0.01	
14	0.885	4.79	0.02	1.78	0.05	75.	0.630	6.92	0.04	
27	0.871	4.77	0.02	1.81	0.02	75.	0.620	6.95	0.02	
28	0.870	5.00	0.02	2.04	0.10	89.	0.591	7.14	0.08	
28	0.870	5.28	0.01	2.17	0.02	99.	0.589	7.26	0.01	
24	0.875	5.64	0.01	2.21	0.02	106.	0.596	7.31	0.02	
19	0.880	5.52	0.02	2.26	0.04	110.	0.591	7.35	0.03	
30	0.868	5.71	0.01	2.50	0.03	124.	0.562	7.36	0.03	
12	0.887	6.00	0.03	2.75	0.03	147.	0.541	7.80	0.03	
27	0.871	5.93	0.02	2.82	0.02	145.	0.525	4.83	0.02	
23	0.876	6.17	0.02	3.24	0.08	175.	0.475	8.20	0.06	
28	0.870	6.22	0.04	3.35	0.06	181.	0.462	8.28	0.07	
28	0.870	6.43	0.03	3.57	0.03	200.	0.445	8.48	0.03	
29	0.874	6.82	0.06	3.83	0.09	229.	0.438	8.74	0.06	
19	0.881	7.23	0.01	4.06	0.04	259.	0.418	8.87	0.04	
26	0.872	7.18	0.03	4.12	0.08	257.	0.422	9.00	0.06	
27	0.871	7.25	0.05	4.20	0.09	267.	0.420	9.08	0.08	
34	0.875	7.66	0.05	4.53	0.06	304.	0.406	9.39	0.05	
23	0.876	8.24	0.05	4.92	0.07	356.	0.403	9.57	0.06	
23	0.876	8.61	0.04	5.15	0.07	489.	0.402	10.00	0.06	
18	0.881	8.91	0.07	5.32	0.15	418.	0.403	10.17	0.12	
27	0.871	8.82	0.08	5.36	0.12	412.	0.393	10.18	0.10	
25	0.874	9.97	0.08	5.45	0.11	427.	0.392	10.28	0.09	

US = A + B*UP WITH A = 1.99 KM/SEC.,
SIG.A = 0.05 KM/SEC.,
FOR UP BETWEEN 0.3 AND 2.5 KM/SEC ANDB = 1.58
SIG.B = 0.03

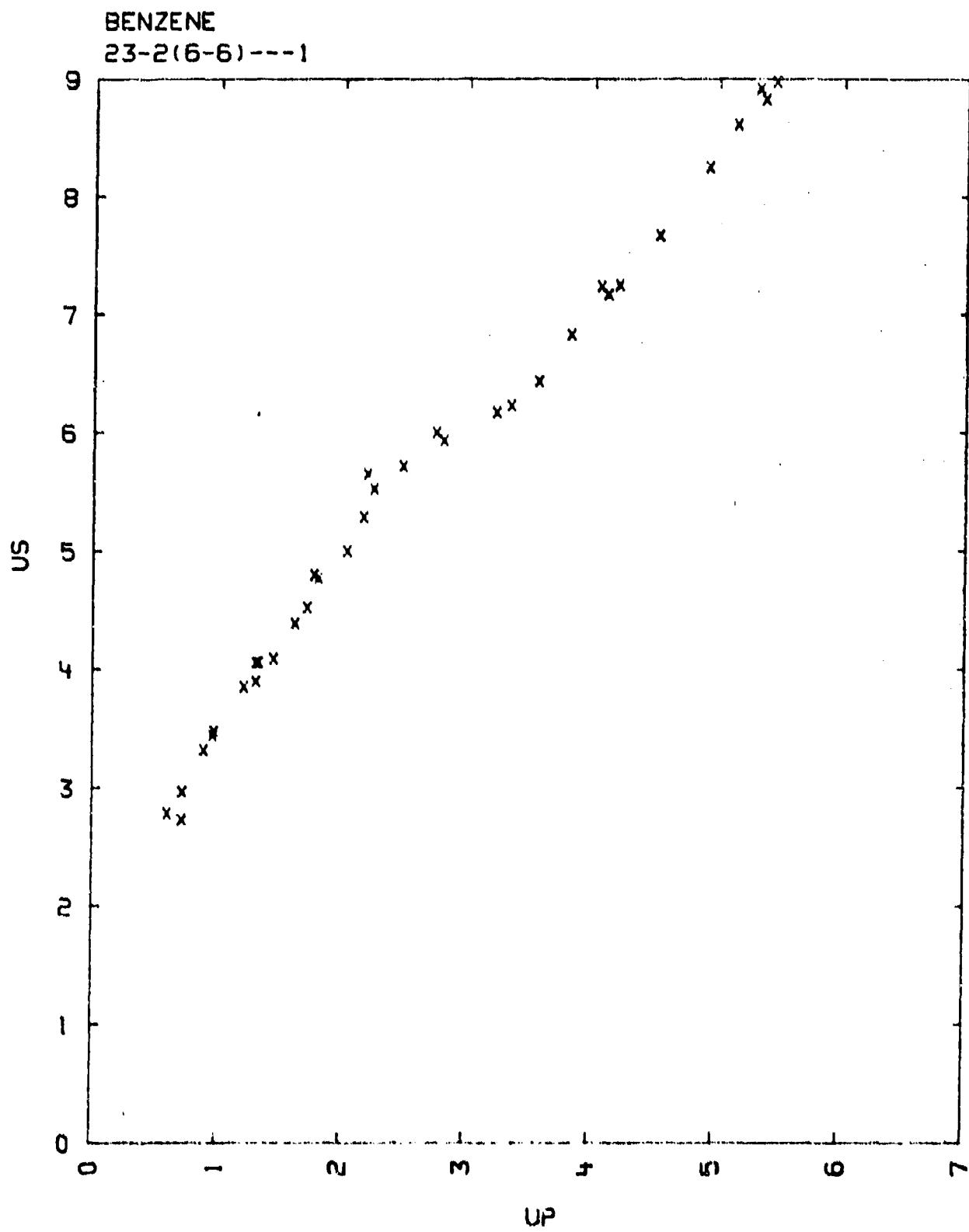
10/14/77

A = 1.68 KM/SEC., B = 1.34
SIG.A = 0.12 KM/SEC SIG.B = 0.03
FOR UP BETWEEN 3.4 AND 5.5 KM/SEC

COMMENTS:

- 1) SOURCE: DICK R. D.
REPORT: LA-3915, APRIL 1968 (THESIS)
LOS ALAMOS SCIENTIFIC LAB.
LOS ALAMOS, BOX 1663, NEW MEXICO 87544
- 2) EXPERIMENTAL TECHNIQUE: A
DATA REDUCTION TECHNIQUE: B STANDARD MATERIAL 2024 AL ALLOY WITH
 $US = 5.460 + 1.318 \cdot UP$ $\rho_{H00} = 2.7850/CC$
AND GRUNEISEN GAMMA = 2.22

TABLE I



24-2(G-6)---2

BENZENE

C6H6

 $T_0 = 16-32 \text{ DEG. CENTIGRADE}$ $\rho_0 = 1.133-1.155 \text{ CC/G}$ $C_0 = 1.35-1.28 \text{ KM/SEC.}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBARS, DENSITY IN G/CC. AND TEMPERATURE IN DEG. CENTIGRADE.

TABLE

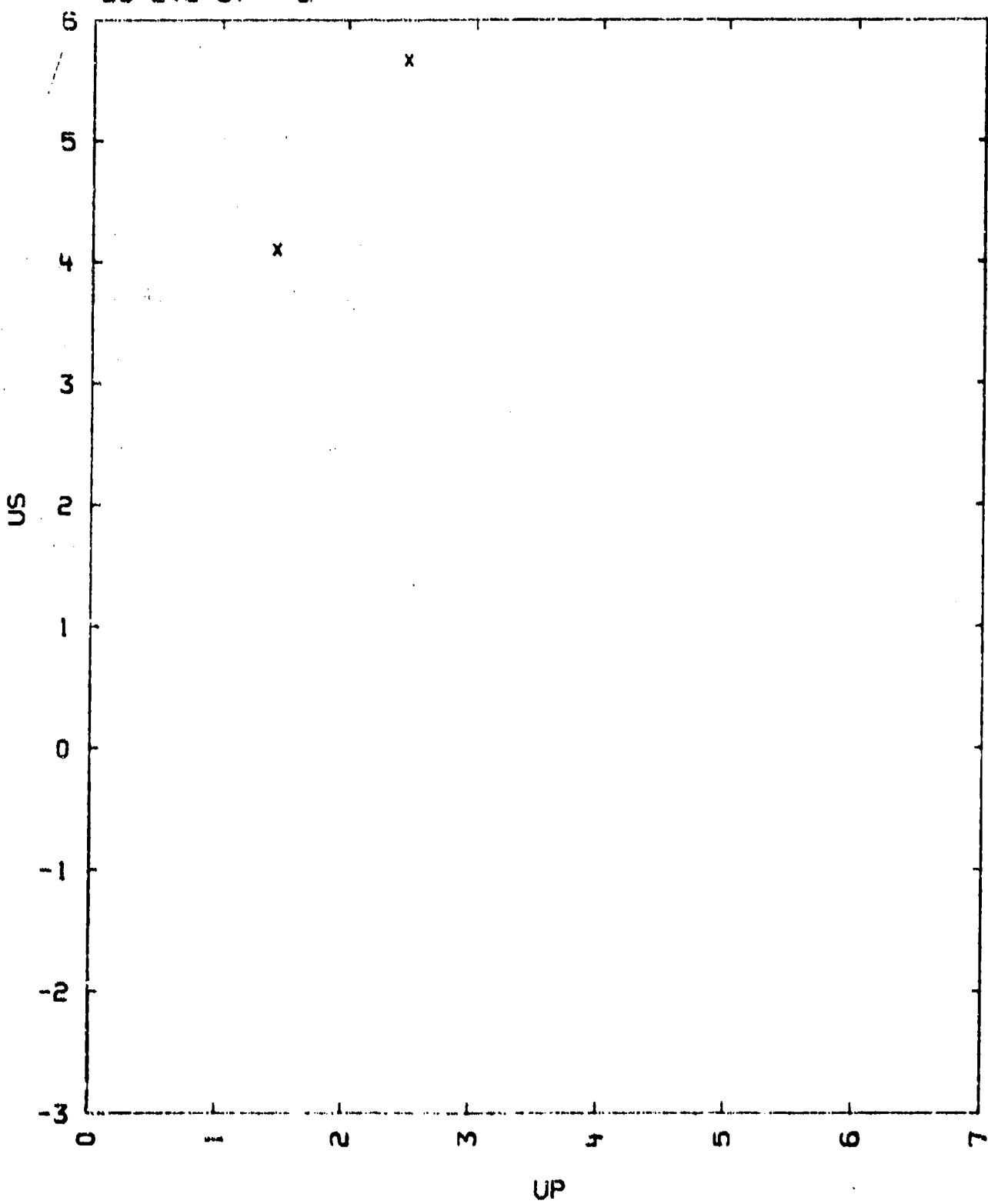
T_0	ρ_{00}	U_S	U_P	P	V/V_0
32	0.8658	5.66	2.470	121.0	0.564
16	0.8826	4.10	1.448	52.4	0.647
$U_S = 1.89 + 1.53 \cdot U_P \text{ KM/SEC}$					

COMMENTS:

- 1) SOURCE: WALSH J. M. AND RICE M. H.
JOURNAL OF CHEMICAL PHYSICS, VOL. 26, P. 815 (1957)
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION TECHNIQUE B
STANDARD MATERIAL 24ST ALUMINUM
- 3) THE VALUES FOR C_0 HERE DETERMINED BY INTERPOLATING THE DATA POINTS
OBTAINED FROM THE AMERICAN INSTITUTE OF PHYSICS HANDBOOK, (MCGRAW-HILL BOOK CO., N. Y., 1963) 2ND ED.

TABLE I

BENZENE
23-2(6-6)---2



25-215-141--1

HEXANE

C6-H14

$T_0 = 19-32 \text{ DEG. CENTIGRADE}$
 $\rho_0 = 1.471-1.499 \text{ G/CC.}$

$C_0 = 1.083 \text{ KM/SEC.}$
 $\text{AT } 20 \text{ DEG. CENTIGRADE}$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBARS, DENSITY IN G/CC AND TEMPERATURE IN DEG. CENTIGRADE.

TABLE

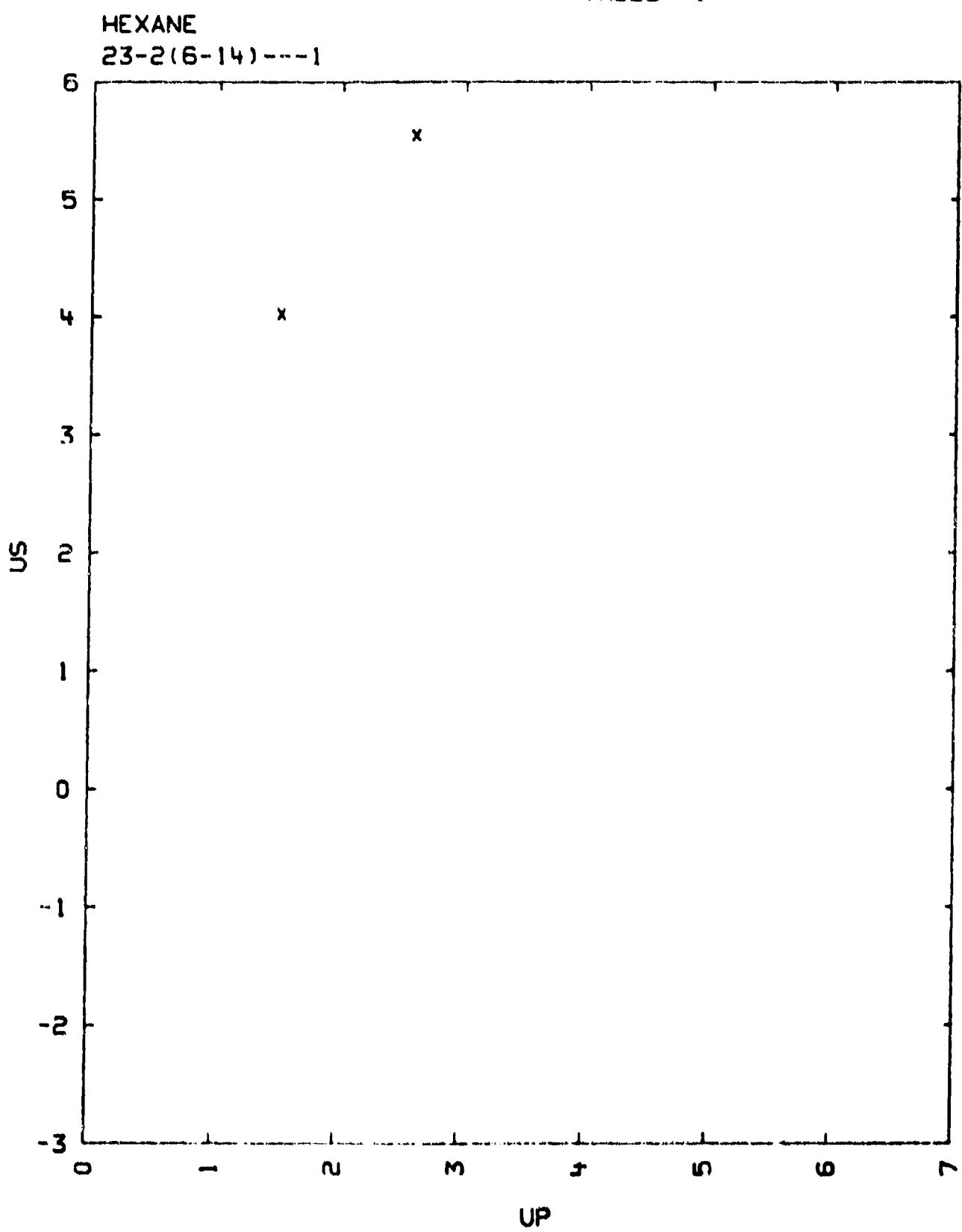
T	ρ_0	US	UP	P	V/V ₀
32	0.6571	5.54	2.590	95.7	0.533
19	0.6798	4.02	1.517	41.5	0.622

$$\text{US} = 1.07 + 1.42 \cdot \text{UP} \text{ KM/SEC}$$

COMMENTS:

- 1) SOURCE: WALSH J. M. AND RICE M. H.
JOURNAL OF CHEMICAL PHYSICS, VOL. 26, P. 815 (1957)
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION TECHNIQUE B
STANDARD MATERIAL 245T ALUMINUM
- 3) C0 AT 20 DEG. CENTIGRADE WAS OBTAINED FROM THE AMERICAN INSTITUTE OF PHYSICS HANDBOOK, (MCGRAW-HILL BOOK CO., N. Y., 1963) 2ND ED.

TABLE I



23-2(6-14)---2

HEXANE

C₁H₃)-(C₁H₂)₄-C₁H₃)T0 = 25-26
V01 = 1.525-1.527 CC/C.

CO(20 DEG.C.) = 1.083 KM/SEC

THE TABLE LISTS T IN DEG C., RHO0 IN G/CC, VELOCITIES IN KM/SEC AND P IN KBARS. RI IS REFRACTIVE INDEX. AL IS 2024 ALUMINUM

TABLE

SAMPLE							DRIVER	
T0	RHO0	US	UP	P	V/V0	RI	UFS	MAT
25.	0.6558	4.17	1.52	41.5	0.635	1.643	1.77	AL
26.	0.6549	3.92	1.56	40.0	0.602	1.684	1.82	AL
20.	0.6603				0.0	1.00	1.375	

US -

COMMENTS:

1) SOURCE: AHRENS T.J. AND RUDERMAN M.H.
J. APPL. PHYS. V.37 P.4758 (1966)

2) EXPERIMENTAL TECHNIQUE: D AND C1

DATA REDUCTION METHOD : B

3) V01 AND RHO0 WERE CALCULATED USING

RHO0(T)=0.6777 + .6496E 3*T - 1.084E-6*T^2 + .164E-9*T^3 G/CC
(LANDOLT BORNSTEIN, ZAHLWERTE UND FUNKTIONEN (SPRINGER VERLAG, N.Y.
1971) V.2 PARTI P.635 AND RHO0(20)=0.6603 TO ADJUST FIRST COEFF.4) CO IS FROM L. BERGMAN, DLR ULTRASCHALL (S. HIRZL VERLAG, STUTTGART
1954)

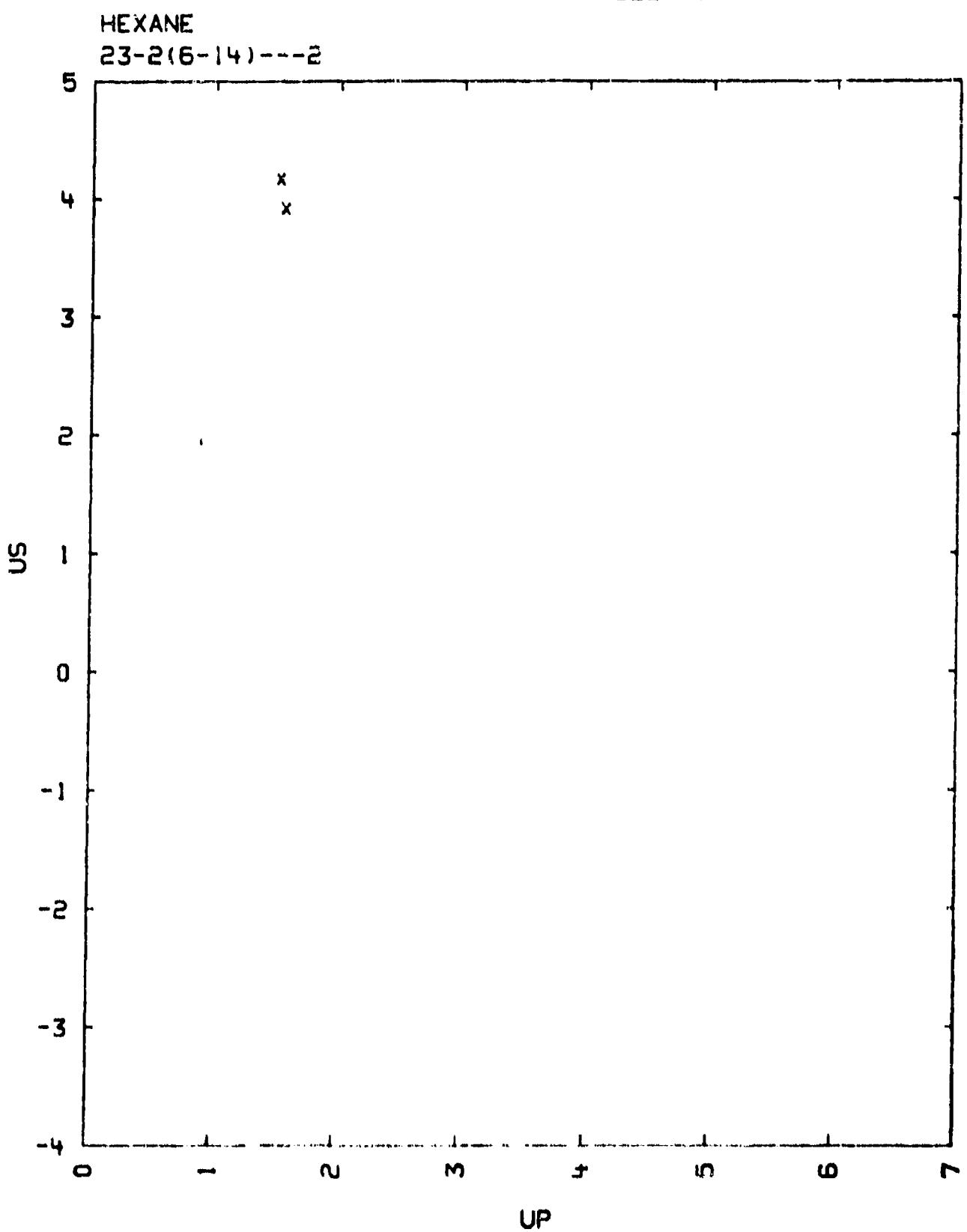
5) UNCERTAINTIES IN US 1-1.5 PERCENT

UP 2.5 - MAXIMUM

RI 1.3 -

6) ISOTHERMAL COMPRESSIBILITY 199E-6 PER ATMOSPHERE. (LANDOLT BORNSTEIN)

TABLE I



23-2(B-B)---

POLYSTYRENE

(C₆-H₅-C(H)-CH₂)N + (C₈-H₈)N

$$V_0 = 0.952 \text{ CC}/\text{O}$$

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN MM/MICROSEC, AND PRESSURE IN KILOBARS.

TABLE

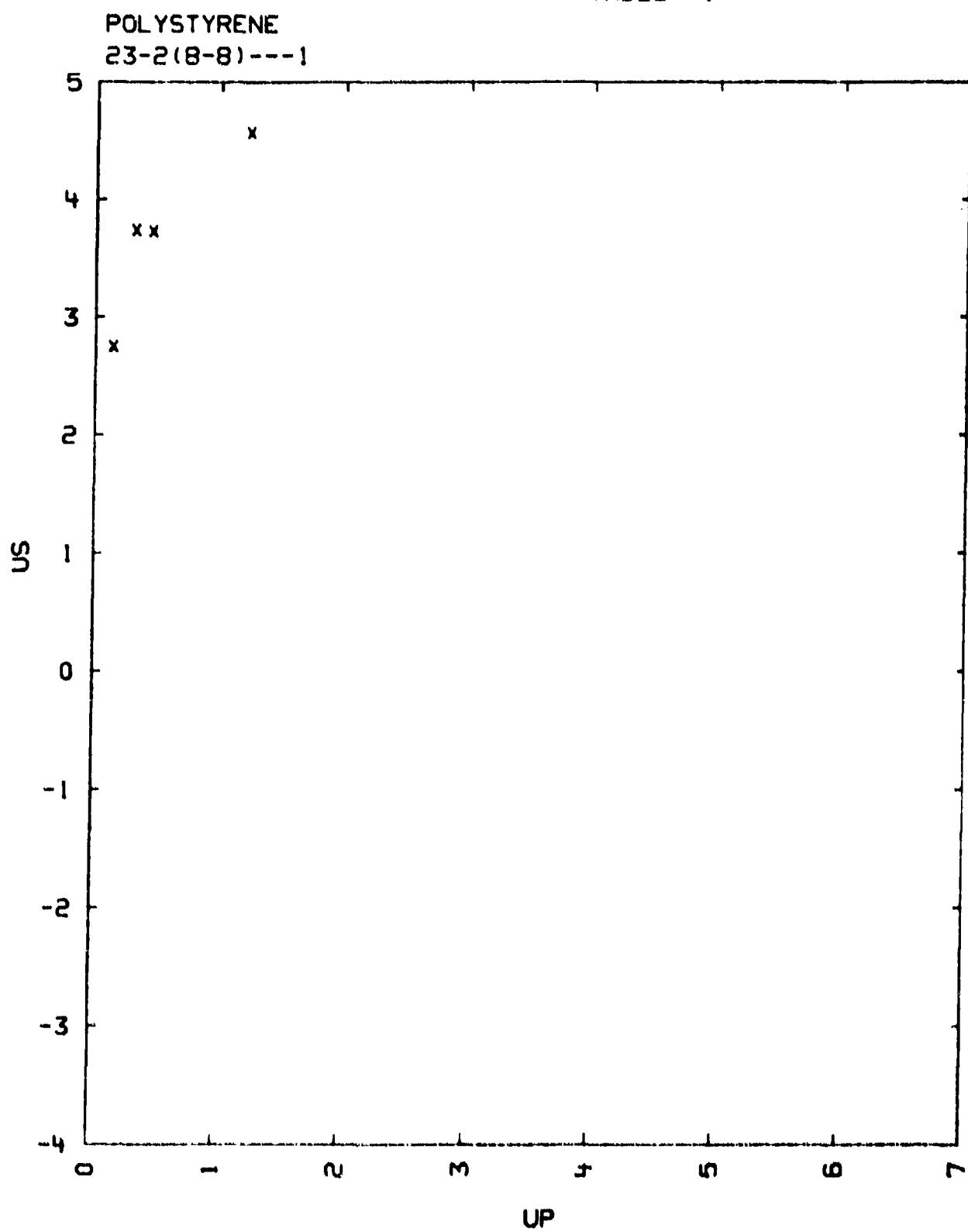
RHO0	US	UP	P	V/V0
1.05	2.74	.140	4.07	.9489
-	3.73	.320	12.5	.9142
-	3.72	.460	17.9	.8764
-	4.56	1.24	59.5	.7281

$$US = 2.62 + 1.60 UP \text{ MM/MICROSEC}$$

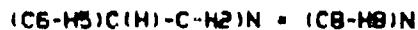
COMMENTS:

- 1) SOURCE: WAGNER, M.H., HALDORF, H.F., AND LOUIE, N.A.
REPORT NO. AFSC-TDR-62-66, VOL. I
WORK DONE AT DOWNEY, CALIFORNIA.
- 2) EXPERIMENTAL TECHNIQUE A
DATA REDUCTION TECHNIQUE D
IN THE TABLE UP = (1/2)US.
- 3) ACCURACY IS LIMITED BECAUSE ASSEMBLY DIMENSIONS ALLOW RELATIVELY
LARGE DEVIATION FROM ONE-DIMENSIONALITY.

TABLE I



23-2(B-B)---2
POLYSTYRENE



$$V_0 = 0.952 \text{ CC/G}$$

IN THE TABLE BELOW DENSITY IS GIVEN IN G/CC. VELOCITY IN KM/SEC AND PRESSURE IN KILOBARS

TABLE I

RHO0	US	UP	P	V/V0
1.05	3.91	0.92	37.7	0.785
-	5.26	1.73	93.5	0.671
-	5.35	1.81	102	0.662
-	5.85	2.15	132	0.632
-	6.12	2.29	147	0.626
-	6.37	2.38	159	0.626
-	6.46	2.48	168	0.616
-	6.73	2.73	193	0.592
-	6.87	3.00	216	0.563
-	7.15	3.32	249	0.536
-	7.17	3.39	255	0.527
-	7.26	3.49	266	0.519
-	7.28	3.40	260	0.533
-	7.31	3.45	265	0.528
-	7.31	3.52	270	0.519
-	7.34	3.46	267	0.529

US = 2.40 + 1.637 UP FROM UP = 0.9 TO 2.5 KM/SEC.
SIGMA US = 0.049 KM/SEC

TABLE II

RHO0	US	UP	P	V/V0
1.05	3.38	0.57	20.2	0.851
-	3.59	0.70	26.4	0.805
-	3.87	0.87	35.3	0.775
-	3.93	0.89	36.3	0.776
-	3.95	0.89	36.5	0.777
-	3.96	0.90	37.4	0.773
-	3.97	0.89	36.7	0.778
-	4.34	1.11	50.6	0.744
-	4.42	1.31	60.8	0.704
-	4.47	1.22	57.3	0.727
-	4.80	1.43	72.1	0.702

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POLYSTYRENE

RHO0	US	UP	P	V/V0
-	5.09	1.46	78.0	0.713
-	5.16	1.62	87.8	0.688
-	5.69	2.01	120	0.647
-	5.72	1.98	118	0.654
-	5.80	2.05	125	0.648
-	5.82	2.05	125	0.648
-	6.03	2.13	135	0.647
-	6.16	2.23	144	0.638
-	6.24	2.28	149	0.635
-	6.36	2.40	160	0.623
-	6.58	2.48	171	0.623
-	6.73	2.92	206	0.586
-	6.87	3.01	217	0.562

US = $2.47 + 1.643 \text{ UP}$ KM/SEC. FROM UP = 0.5 TO 2.5 KM/SEC
 SIGMA US = 0.077 KM/SEC.

THE LEAST SQUARE FIT ON TABLE I AND II COMBINED YIELDS
 US = $2.48 + 1.63 \text{ UP}$ KM/SEC. FROM UP = 0.5 TO 2.5 KM/SEC

SIGMA US = 0.08

US = $3.96 + 0.98 \text{ UP}$ KM/SEC. FROM UP = 2.7 TO 3.6 KM/SEC

SIGMA US = 0.044

COMMENTS:

- 1) SOURCE: HAUVER G. E. AND MELANI A.
B.R.L. REPORT NO. 1259 (1964)
BALLISTIC RES. LABS., ABERDEEN PROVING GROUNDS, MD.
- 2) EXPERIMENTAL TECHNIQUE B, C1 (TABLE I), H (TABLE II)
DATA REDUCTION METHOD B
- 3) AN APPARENT DISCONTINUITY IN THE US VS. UP CURVE SUGGESTS A TRANSITION AT 180 KB WHICH IS SUPPORTED BY A RAPID CHANGE IN THE POLARIZATION SIGNAL ABOVE THIS PRESSURE.
- 4) ALL DATA CORRECTED FOR SHOCK WAVE TILT

TABLE I

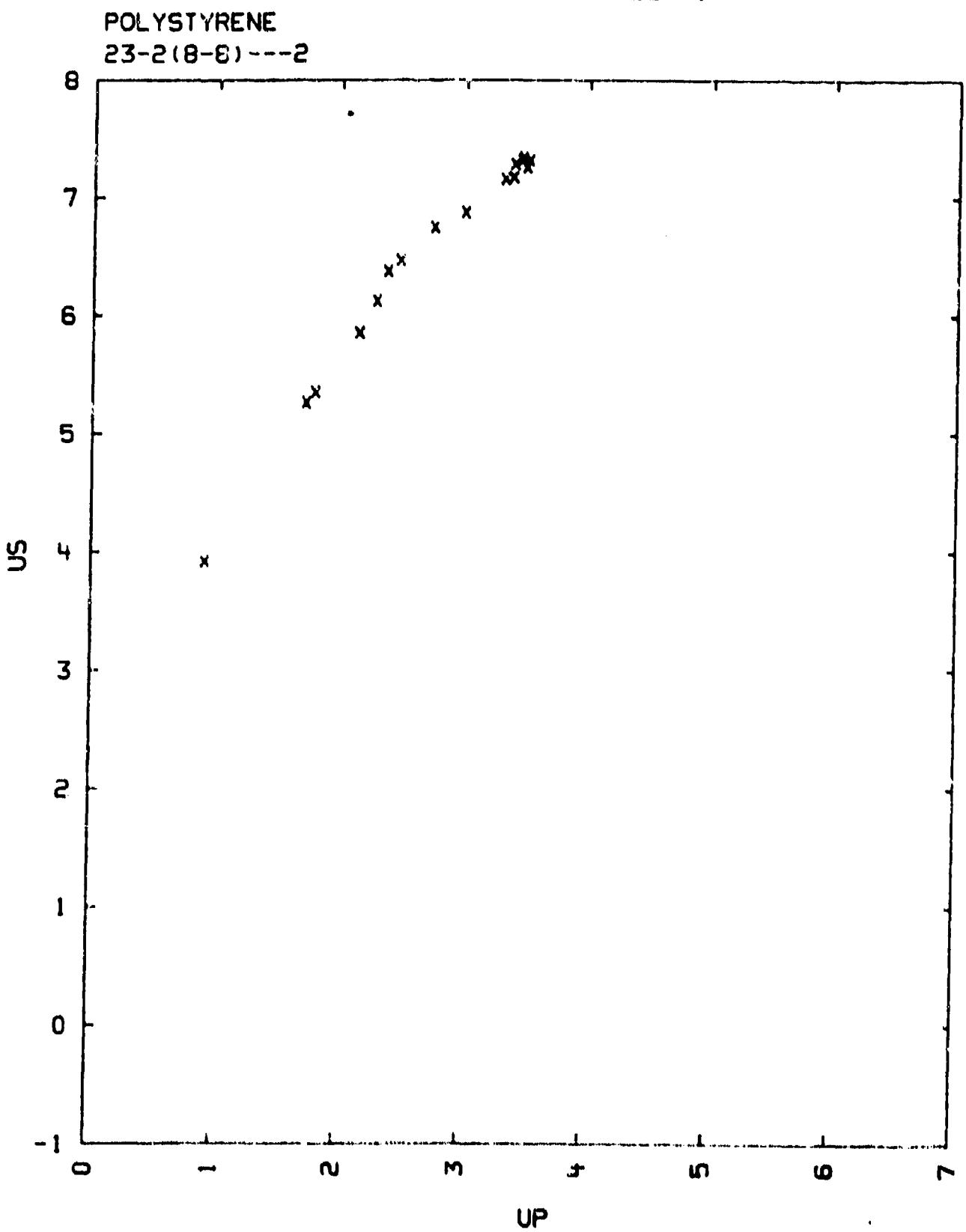
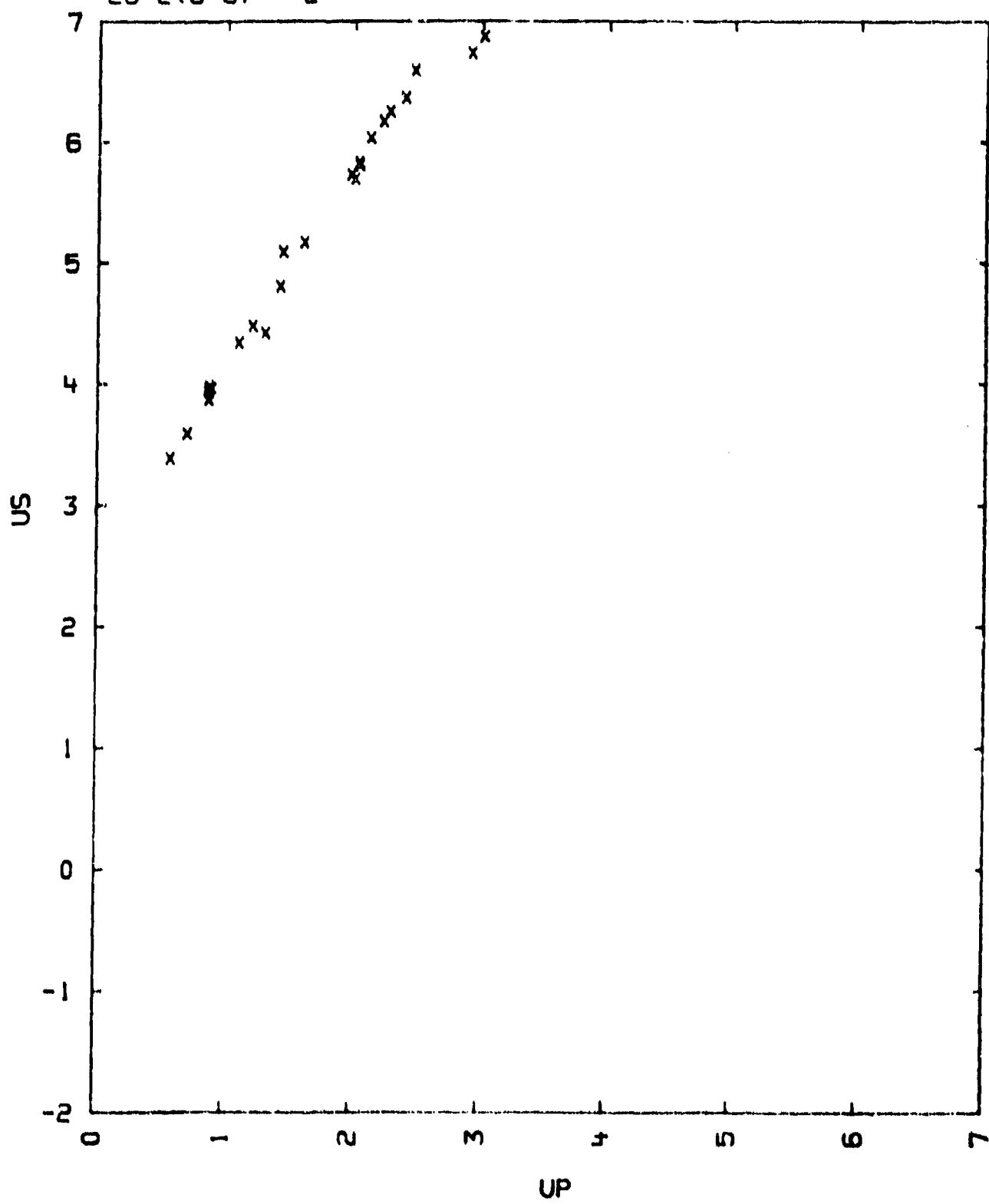


TABLE II

POLYSTYRENE
23-2(8-8)---2



23-2(θ-θ)---3

POLYSTYRENE

(C₆-H₅-C(H)-CH₂)N + (C₈-H₈)NV_D = 0.8542 CC/G.

IN THE TABLE BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBARS AND DENSITY IN G/CC.

TABLE

-----SAMPLE----- STANDARD-----

RHO0	US	UP	P	V/V0	UFS (PLEXIGLASS)	UFS (ALUMINUM ALLOY)
1.048	5.841	2.335	143.0	0.600	4.600	
-	6.038	2.310	146	0.617	4.600	
-	5.952	2.265	141	0.619	4.500	
-	6.082	2.330	148	0.617	4.660	
-	5.636	2.027	119	0.640	3.990	
-	5.592	2.020	118	0.639	3.960	
-	5.793	2.130	129	0.632	4.220	
-	5.793	2.165	132	0.626	4.280	
-	6.203	2.135	139	0.656	4.340	
-	6.038	2.125	134	0.648	4.280	
-	5.813	2.180	133	0.628	4.320	
-	5.875	2.140	132	0.636	4.260	
-	5.580	2.158	127	0.613		2.900
-	5.624	2.155	127	0.617		2.900
-	5.611	2.240	132	0.601		3.010
-	5.611	2.265	134	0.596		3.040
-	5.478	2.015	117	0.632		2.700
-	5.446	2.042	118	0.625		2.730
-	5.422	1.935	110	0.643		2.590
-	5.382	1.927	109.5	0.642		2.580
-	5.387	2.067	116	0.616		2.750
-	5.452	1.995	114	0.634		2.670
-	5.592	2.095	124	0.625		2.815
-	5.773	2.105	128	0.635		2.850
-	5.186	1.812	96	0.650		2.390
-	5.165	1.800	95	0.652		2.377
-	5.122	1.802	96.5	0.648		2.385
-	5.010	1.827	96	0.635		2.405
-	5.170	1.840	100	0.644		2.445
-	5.154	1.832	100	0.645		2.435
-	5.122	1.840	99.5	0.641		2.440
-	5.070	1.752	100	0.635		2.455
-	5.192	1.912	105	0.632		2.540
-	5.154	1.918	105	0.628		2.550
-	5.128	1.955	104	0.619		2.580
-	5.185	1.908	106	0.615		2.635
-	4.270	1.368	61	0.679		1.755
-	4.270	1.365	61	0.680		1.748
-	4.452	1.462	68	0.672		1.840
-	4.496	1.418	67	0.684		1.835

006/14/77

POLYSTYRENE

RHO0	US	UP	P	V/V0	UFS	URS
-	4.533	1.405	67	0.680		1.825
-	4.448	1.400	67	0.685		1.820
-	4.370	1.492	69	0.658		1.825
-	4.413	1.475	69.5	0.666		1.900
-	3.822	1.115	45	0.708		1.402
-	3.852	1.108	45	0.712		1.322
-	3.918	1.090	45	0.722		1.375
-	3.879	1.095	45	0.718		1.380
-	3.582	0.980	36.5	0.732		1.195
-	3.559	0.980	36.5	0.730		1.195
-	3.618	0.972	37	0.731		1.212
-	3.644	0.978	37.5	0.732		1.220
-	3.955	1.097	48	0.722		1.390
-	4.022	1.102	48.5	0.726		1.397
-	3.949	1.195	46	0.697		1.390
-	3.968	1.215	47	0.694		1.405
-	3.754	0.360	38	0.744		1.215
-	3.615	0.980	37.5	0.729		1.200
-	3.626	1.042	40	0.712		1.287
-	3.626	1.037	39.5	0.714		1.302

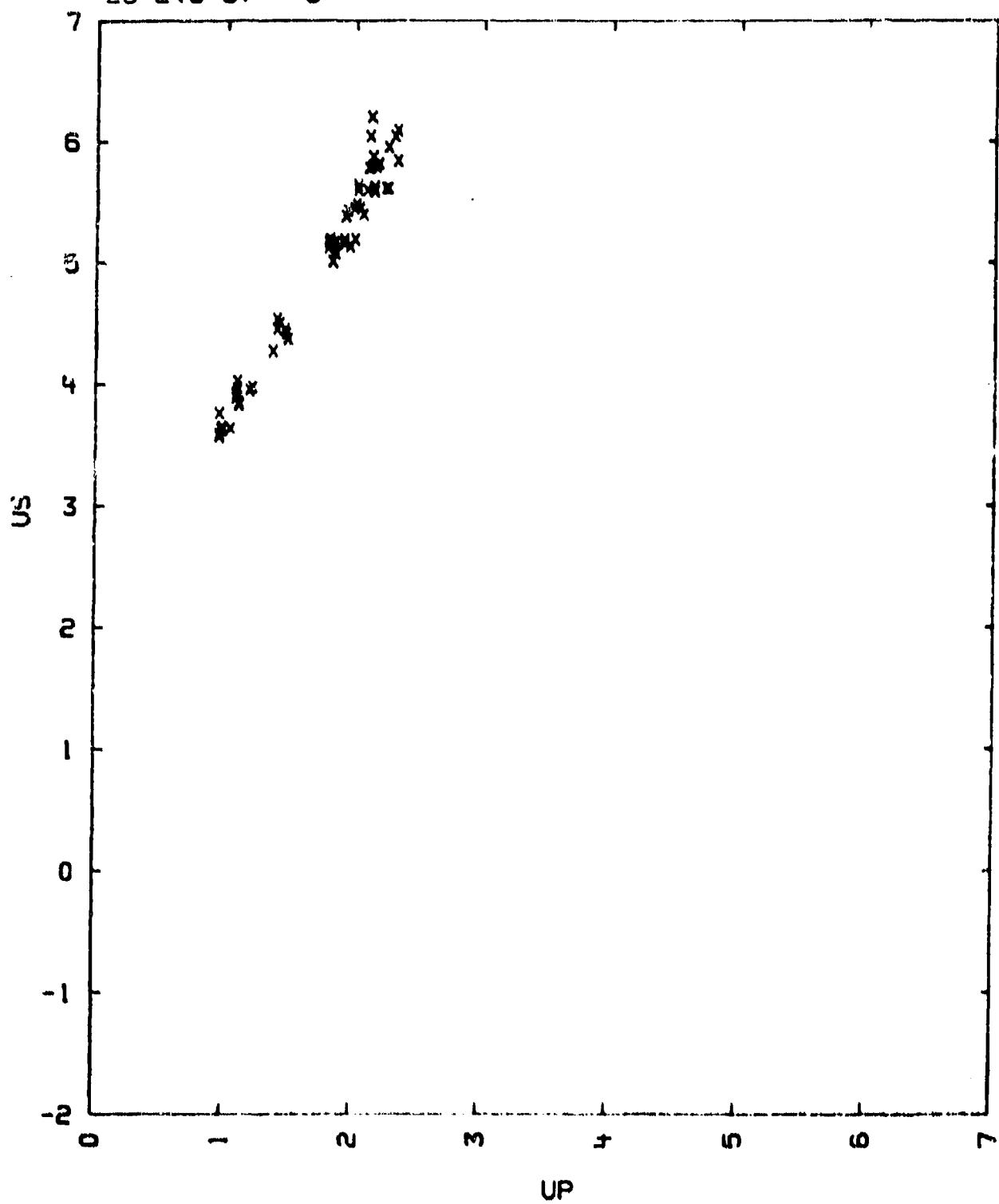
US = 1.902 + 1.769 UP KM/SEC. S10.US = 0.14 KM/SEC.

COMMENTS:

- 1) SOURCE: BERGER J. AND FAUCIGNON C.
PRIVATE COMMUNICATION (1964), B.P. NO. 7, SEVRAN, FRANCE
- 2) EXPERIMENTAL TECHNIQUE B
DATA REDUCTION TECHNIQUE B
STANDARD MATERIALS PLEXIGLASS AND ALUMINUM AUMG ALLOY
- 3) SAMPLE DIMENSIONS WERE: 2.0 CM DIAMETER
0.5 CM THICKNESS

TABLE I

POLYSTYRENE
23-2(8-8)---3



23-2(B-B)---4
POLYSTYRENE



$$V_0 = 0.958 \text{ CC}/\text{O}$$

IN THE TABLES BELOW, VELOCITIES ARE GIVEN IN KM/SEC., PRESSURE IN KILOBAR
AND DENSITY IN G/CC.

TABLE I

SAMPLE					STANDARD		
RHO ₀	US	UP	P	V/V ₀	MATERIAL	US(ST)	
1.044	4.35	1.27	58.	0.7080	2024 AL	6.41	
1.044	4.51	1.29	61.	0.7140	2024 AL	6.44	
1.044	5.68	2.21	131.	0.6095	2024 AL	7.30	

$$US = 2.748 + 1.319 \cdot UP \text{ KM/SEC}$$

$$\text{SIGMA US} = 0.094 \text{ KM/SEC}$$

TABLE II

SAMPLE					STANDARD		
RHO ₀	US	UP	P	V/V ₀	MATERIAL	US(ST)	
0.174	1.81	1.59	5.	0.1215	2024 AL	6.41	
0.174	1.91	1.76	6.	0.0785	2024 AL	6.53	
0.174	2.11	1.85	7.	0.1232	2024 AL	6.59	
0.174	2.31	2.27	10.	0.0956	2024 AL	6.88	
0.174	2.49	2.29	10.	0.0803	2024 AL	6.90	
0.174	3.48	2.97	18.	0.1466	2024 AL	7.38	
0.174	3.44	3.03	18.	0.1192	2024 AL	7.42	
0.174	3.33	3.04	18.	0.0871	2024 AL	7.43	

$$US = -0.069 + 1.151 \cdot UP \text{ KM/SEC}$$

$$\text{SIGMA US} = 0.083 \text{ KM/SEC}$$

TABLE III

SAMPLE					STANDARD		
RHO ₀	US	UP	P	V/V ₀	MATERIAL	US(ST)	
0.063	3.33	3.10	7.	0.0691	2024 AL	7.42	
0.063	2.81	3.28	8.	0.1391	2024 AL	7.54	
0.063	4.37	3.63	10.	0.1693	2024 AL	7.78	
0.063	5.66	4.84	17.	0.1449	2024 AL	8.58	
0.063	6.57	5.92	23.	0.1598	2024 AL	9.05	
0.063	6.69	5.73	24.	0.1439	2024 AL	9.19	

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POLYSTYRENE

RHO0	US	UP	P	V/V0	MATERIAL US(ST)
0.063	7.52	6.21	29.	0.1742	2024 AL 9.51
0.063	9.51	6.62	40.	0.3039	2024 AL 9.81
0.063	9.22	6.84	40.	0.2581	2024 AL 9.95
0.063	8.94	7.29	41.	0.1848	2024 AL 10.23

$$US = -1.096 + 1.443 \cdot UP \text{ KM/SEC}$$

$$\Sigma \text{IGMA US} = 0.515 \text{ KM/SEC}$$

TABLE IV

-----SAMPLE----- -----STANDARD-----

RHO0	US	UP	P	V/V0	MATERIAL US(ST)
0.032	4.04	3.30	4.	0.1832	2024 AL 5.74
0.032	4.52	3.66	5.	0.1903	2024 AL 7.78
0.032	6.36	4.89	10.	0.2311	2024 AL 8.59
0.032	7.05	5.59	13.	0.2071	2024 AL 9.05
0.032	6.46	5.81	12.	0.1606	2024 AL 9.19
0.032	8.21	6.30	17.	0.2326	2024 AL 9.51
0.031	7.78	6.78	16.	0.1285	2024 AL 9.81
0.032	10.72	6.95	24.	0.3517	2024 AL 9.95
0.032	9.67	7.42	23.	0.2327	2024 AL 10.23

$$US = -7.786 + 1.418 \cdot UP \text{ KM/SEC}$$

$$\Sigma \text{IGMA US} = 0.837 \text{ KM/SEC}$$

THE POROUS DATA MAY BE REPRESENTED BY :

$$US = 2.72 + 103.7 \cdot (RHO - 1.265) / (1 \cdot UP)^{1.5} + 75.1 \cdot (RHO - 1.265)^{0.27} / (1 \cdot UP)^{0.3}$$

$$+ 1.430 \cdot UP + 0.831 \cdot UP(RHO - 1.265) \text{ KM/SEC}$$

$$\Sigma \text{IGMA US} = 0.15 \text{ KM/SEC}$$

COMMENTS:

- 1) SOURCE: MCQUEEN, R.G., MARCH, S.P., TAYLOR, J.W., FRITZ, J.M., AND CARTER, W.J.
THE EQUATION OF STATE OF SOLIDS FROM SHOCK WAVE STUDIES,
HIGH VELOCITY IMPACT PHENOMENA, KINSLOW (ED.), ACADEMIC
PRESS, NEW YORK, 1970, CHAPTER VII
- 2) EXPERIMENTAL TECHNIQUE: E
DATA REDUCTION TECHNIQUE: II (STANDARD BASE PLATE AS SHOWN)
- 3) V(DP/DE) = 1.18

TABLE I

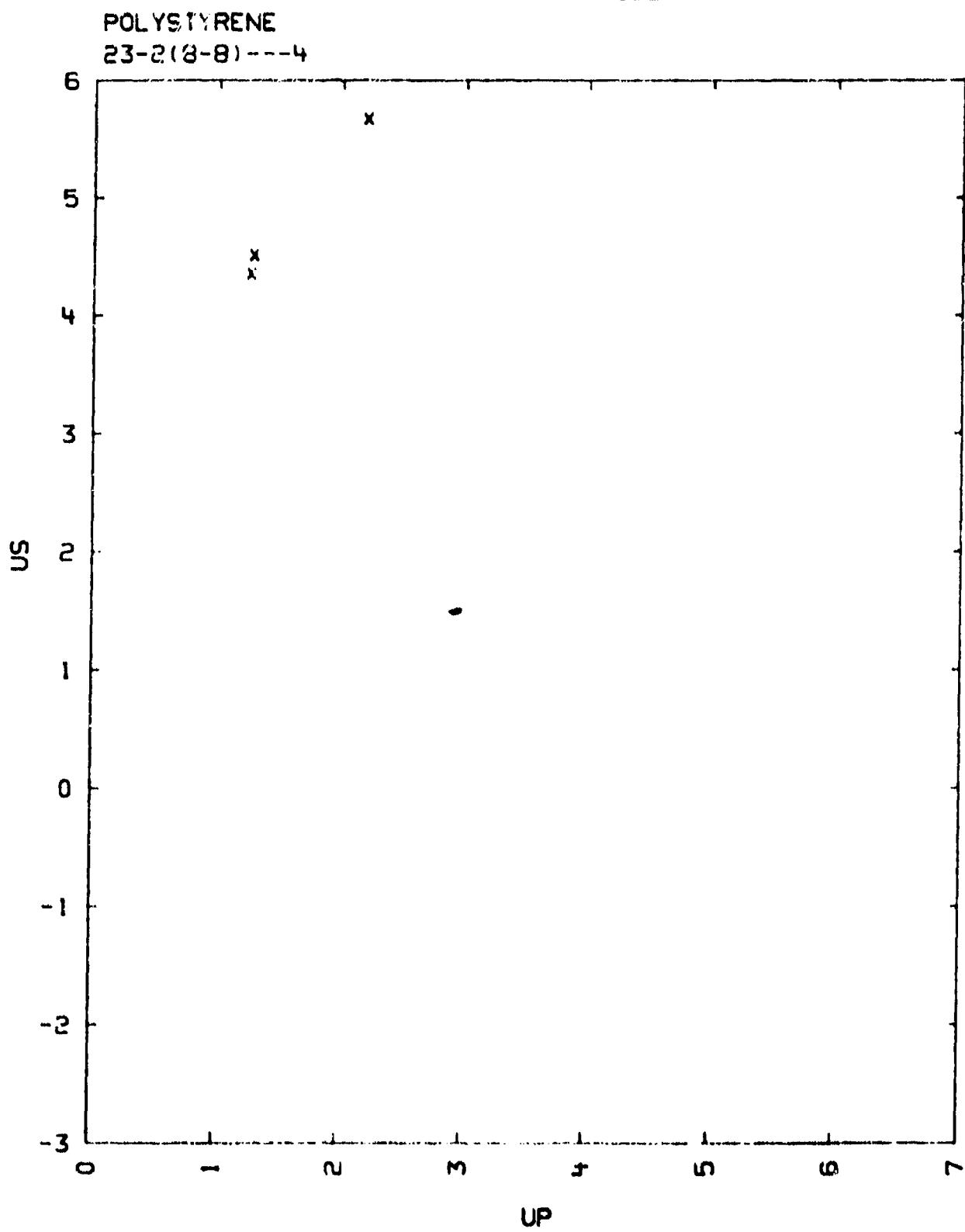


TABLE II

POLYSTYRENE
23-2(8-8)---4

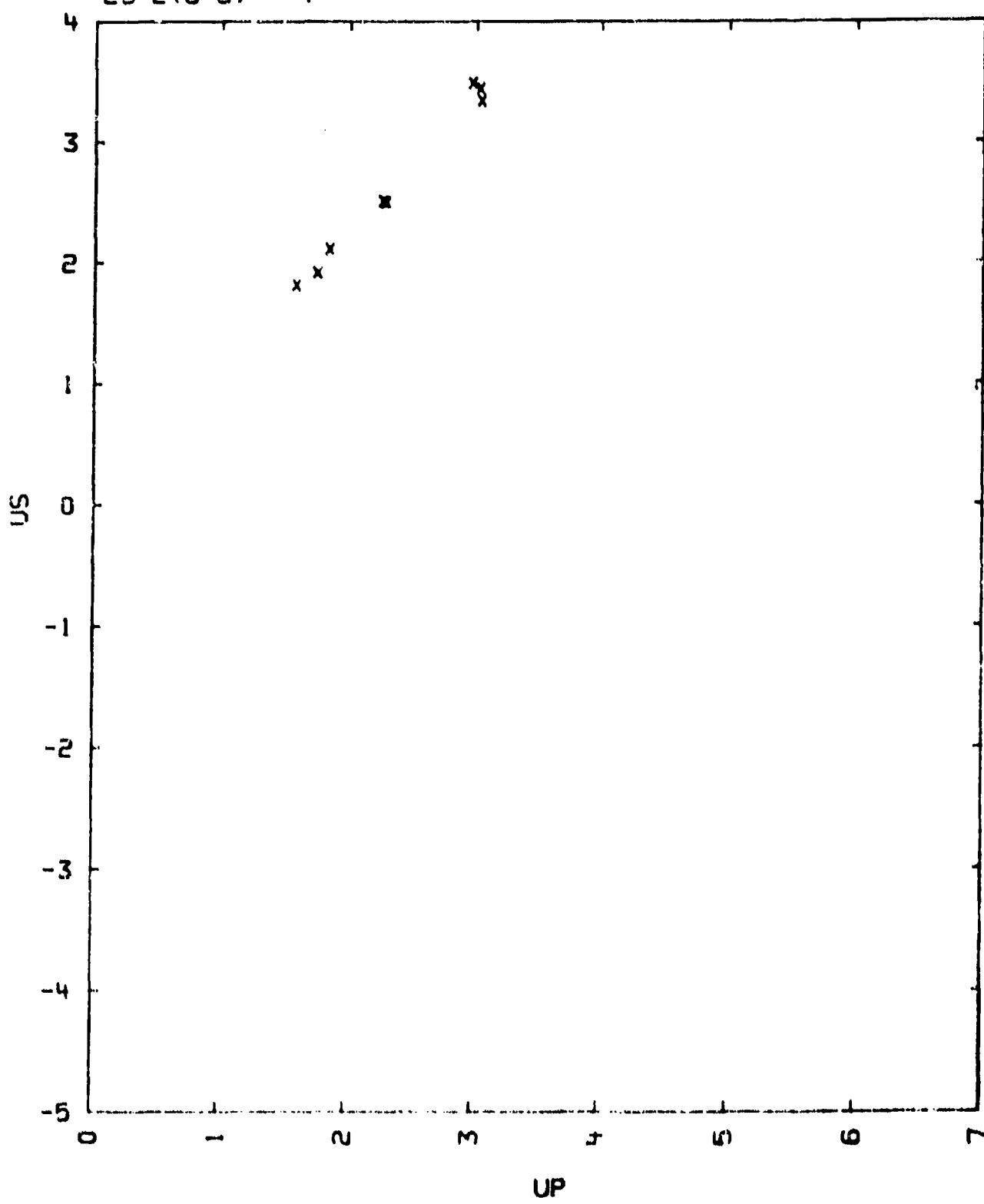


TABLE III

POLYSTYRENE
23-2(8-8)---4

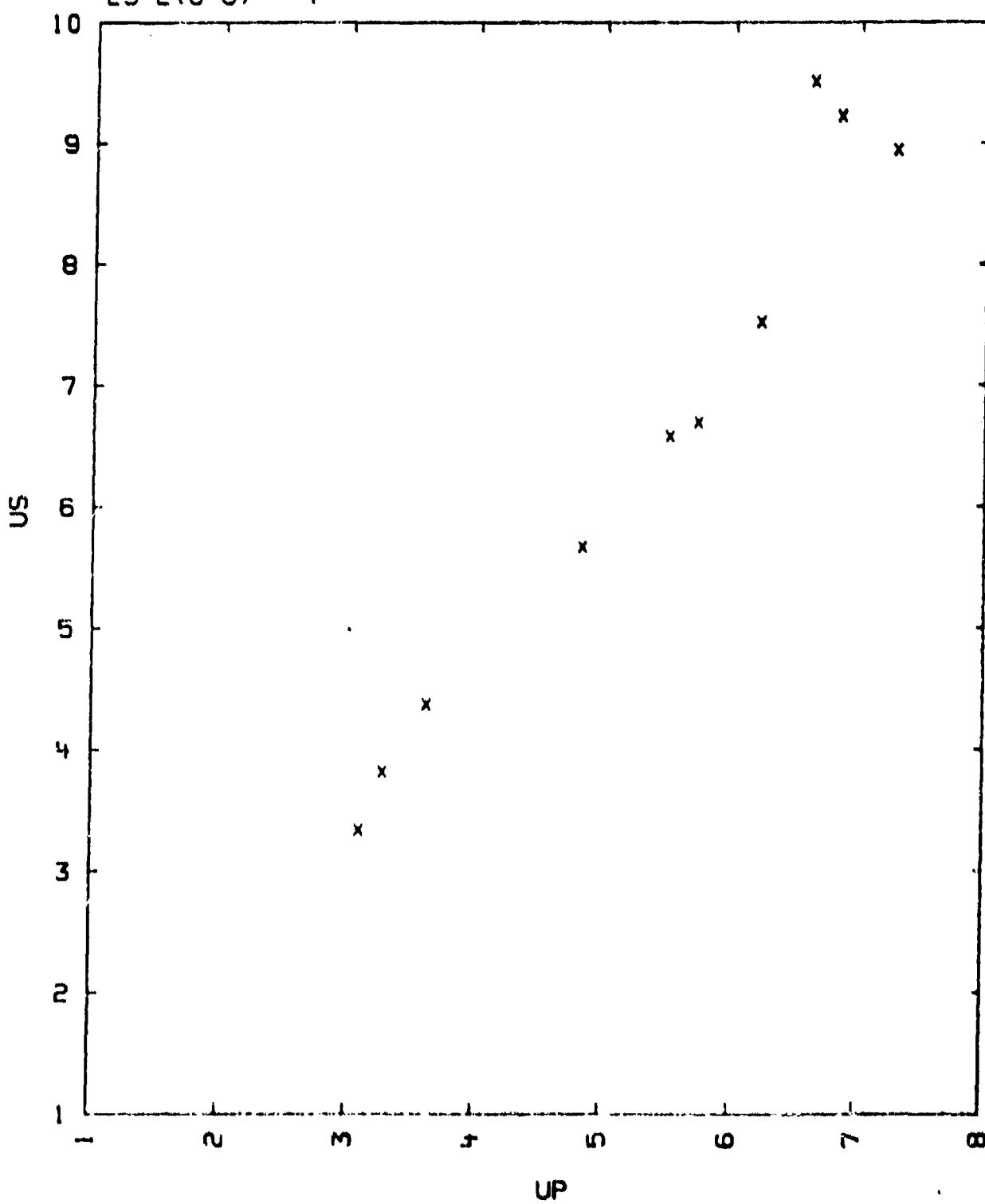
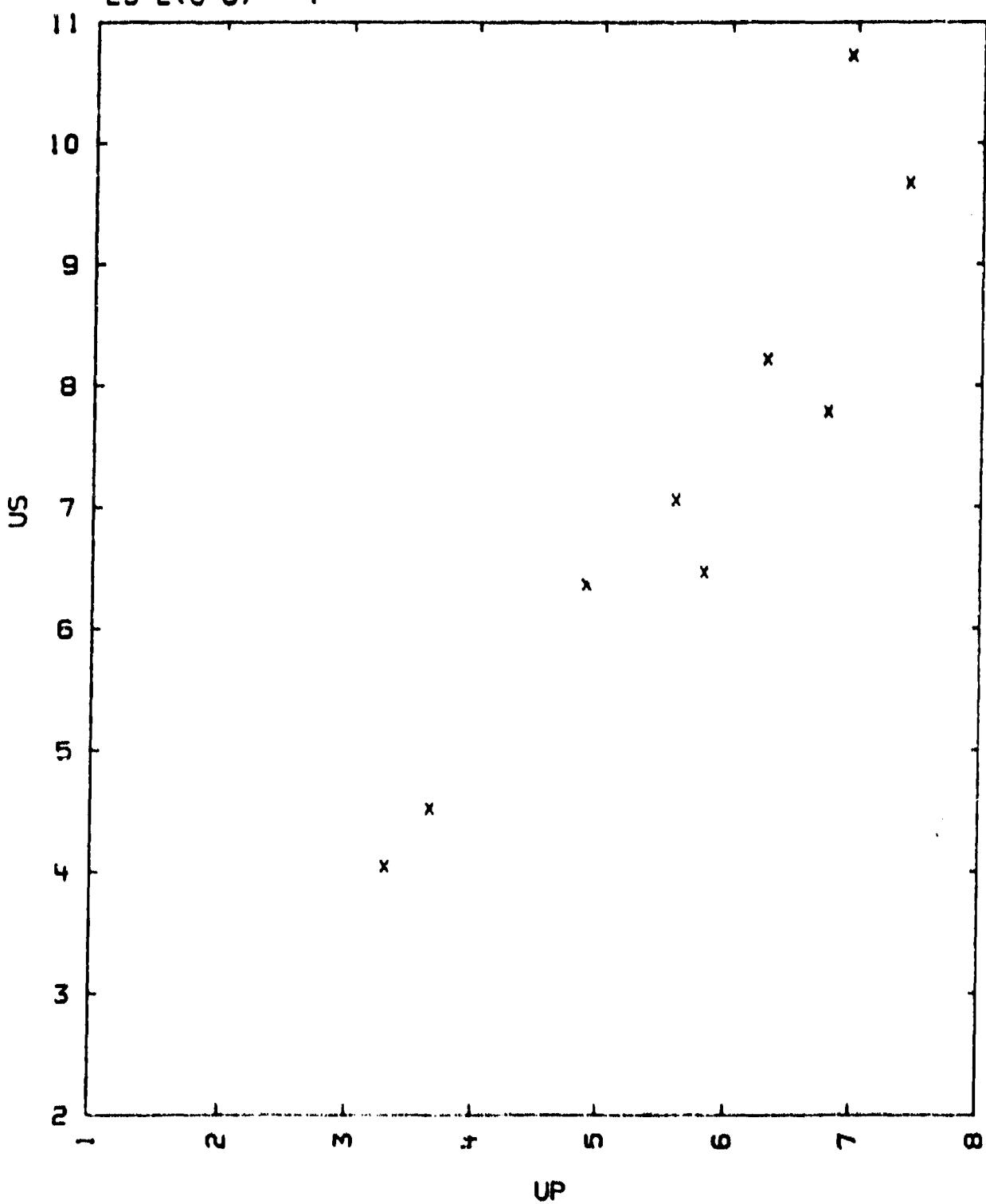


TABLE IV

POLYSTYRENE
23-2(8-8)---4



23-2(14-101---1
ANTHRACENE



$$V_0 = 0.8006 + 0R - 0.0006 \text{ CC}/\text{O}$$

$$V_{01} = 0.7968 \text{ CC}/\text{O}$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS.

TABLE

SAMPLE					STANDARD
RHO0	US	UP	P	V/V0	US(STD)
1.249	3.855	0.409	19.7	0.894	5.741
1.249	3.894	0.480	23.3	0.877	5.804
1.249	4.160	0.579	35.3	0.837	5.987
1.248	4.979	1.278	79.4	0.743	6.558
1.250	5.747	1.689	121.3	0.706	6.979
1.249	5.923	1.904	140.8	0.679	7.187
1.248	6.450	2.230	180.3	0.653	7.534
1.249	6.644	2.497	207.2	0.624	7.785
1.249	6.836	2.871	245.1	0.580	8.141
1.249	7.227	3.438	310.5	0.524	8.690
1.249	7.511	3.768	355.4	0.496	9.035
1.249	8.123	4.358	442.2	0.463	9.615
1.249	8.491	4.433	470.1	0.478	9.728
1.249	9.105	4.836	550.0	0.469	10.166

$$US = 3.21 + 1.445 \cdot UP \text{ KM/SEC.} \quad \text{SIG US} = 0.10 \text{ KM/SEC.}$$

FOR UP LESS THAN 2.3 KM/SEC

$$US = 6.722 + 0.0051(UP-2.343) + 0.3785(UP-2.343)^2 \text{ KM/SEC.}$$

$$\text{SIG US} = 0.23 \text{ KM/SEC.}$$

FOR UP BETWEEN 2.34 AND 5. KM/SEC

COMMENTS:

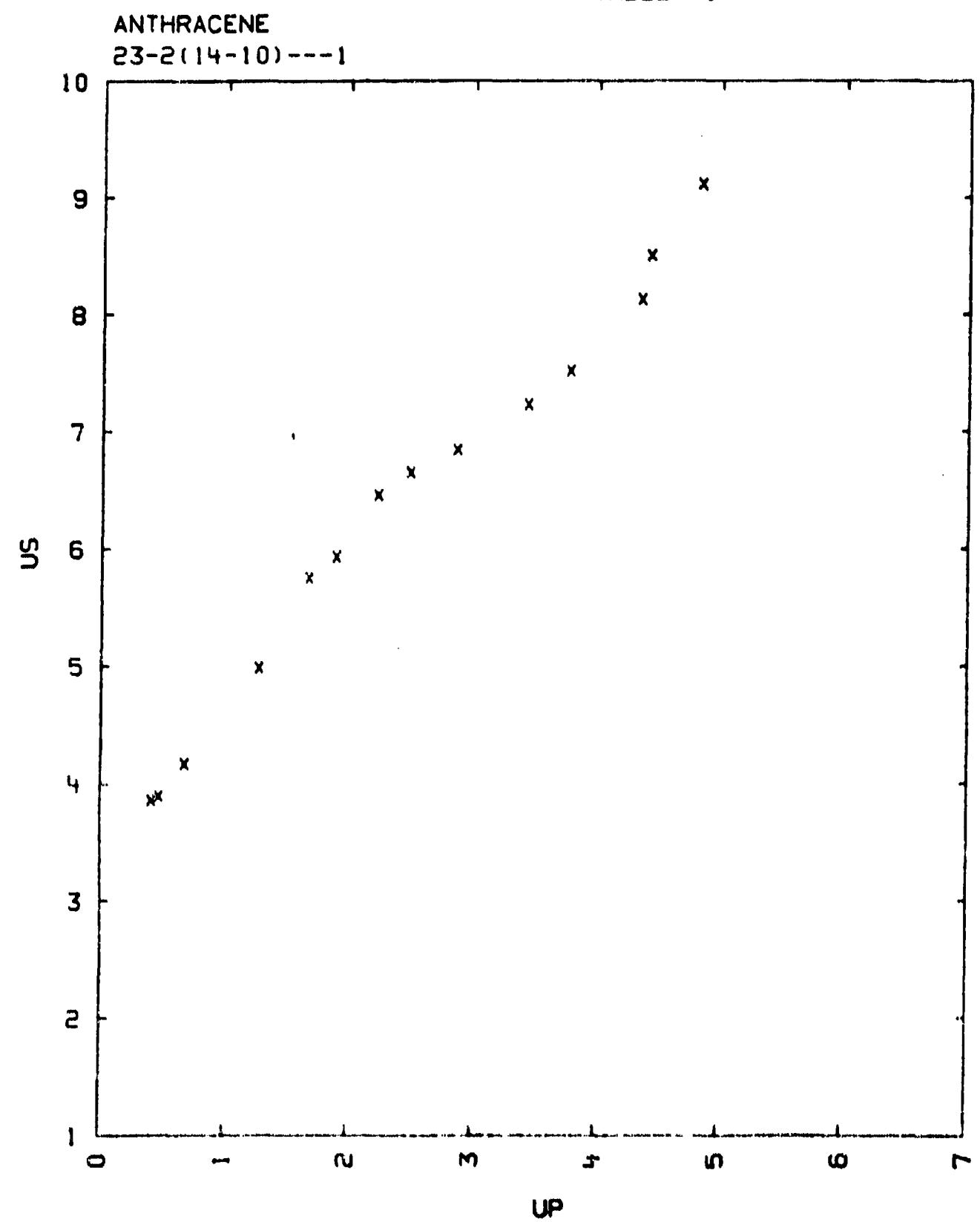
- 1) SOURCE: HARNES, R.
 PRIVATE COMMUNICATION (PRELIMINARY DATA)
 LOS ALAMOS SCIENTIFIC LABORATORY, LOS ALAMOS, NEW MEXICO, USA
- 2) EXPERIMENTAL TECHNIQUE B.
 DATA REDUCTION TECHNIQUE B.
 STANDARD MATERIAL 1100 ALUMINUM ALLOY: THE EQUATION FOR THE US-UP ALUMINUM STANDARD HUGONIOT RELATIONSHIP IS

$$US = 5.380 + 1.338 \cdot UP \text{ KM/SEC}$$
 WHERE $\rho_{00} = 2.712 \text{ G/CC.}$
- 3.1 V₀₁ WAS CALCULATED USING THE FOLLOWING LATTICE PARAMETERS: A = 0.423, B = 0.023 AND C = 0.544 ANGSTROMS AND THE ANGLE BETA = 103 DEG 30 MINUTES FOR A MONOCLINIC CELL. THESE PARAMETERS WERE OBTAINED

FROM A.C.A. MONOGRAPH 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION,
POLYCRYSTAL BOOK SERVICE, WASHINGTON D. C., 1883) 2ND. EDITION.

UOG/14/77

TABLE I



23-2(14-10)---2

PHENANTHRENE

 $C_6-H_4-(C-H)_2-C_6-H_4 + C_{14}-H_{10}$

$$V_0 = 0.8242 + OR - 0.0003 CC/0$$

$$V_{01} = 0.8173 CC/0$$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS.

TABLE

-----SAMPLE----- STANDARD					
RHO0	US	UP	P	V/V0	US(ST)
1.212	3.774	0.414	10.9	0.890	5.741
1.212	3.741	0.408	22.1	0.870	5.804
1.212	4.038	0.689	33.7	0.829	5.987
1.212	4.907	1.292	78.8	0.737	6.558
1.213	5.597	1.714	116.4	0.694	6.979
1.212	5.692	1.939	133.8	0.659	7.187
1.212	6.348	2.287	174.4	0.643	7.934
1.213	6.662	2.515	203.2	0.623	7.785
1.213	6.804	2.897	239.1	0.574	8.141
1.212	7.086	3.483	299.2	0.508	8.690
1.213	7.443	3.827	345.6	0.486	9.035
1.213	8.000	4.410	428.0	0.449	9.615
1.212	8.441	4.476	458.0	0.470	9.728
1.212	9.048	4.884	535.6	0.460	10.165

US = $3.097 + 1.417 \cdot UP$ KM/SEC. SIG US = 0.1 KM/SEC.
FOR UP LESS THAN 2.5 KM/SEC

US = $6.734 - 0.0478(UP-2.515) + 0.4302(UP-2.515)^{1/2}$. KM/SEC
SIG US = 0.24 KM/SEC
FOR UP BETWEEN 2.5 AND 5. KM/SEC

COMMENTS:

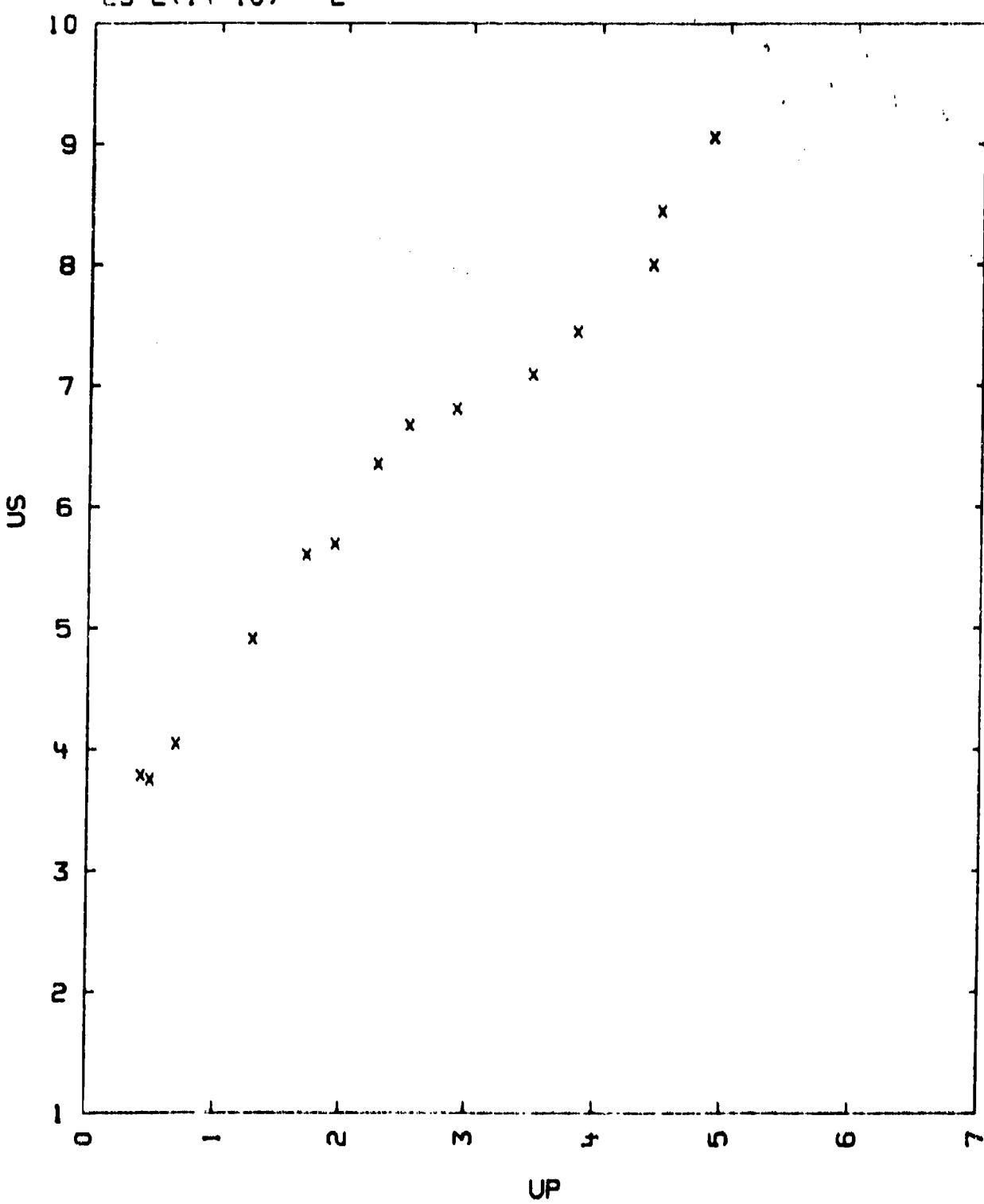
- 1) SOURCE: WARNE, R.
PRIVATE COMMUNICATION (PRELIMINARY DATA)
LOS ALAMOS SCIENTIFIC LAB., LOS ALAMOS, NEW MEXICO, USA.
- 2) EXPERIMENTAL TECHNIQUE A.
DATA REDUCTION TECHNIQUE B.
STANDARD MATERIAL 1100 ALUMINUM ALLOY: THE EQUATION FOR THE US-UP ALUMINUM STANDARD HUGONIOT RELATIONSHIP IS
 $US = 5.980 + 1.338 \cdot UP$ KM/SEC
WHERE $RHO0 = 2.712$ G/CC.
- 3) V01 HAS CALCULATED USING THE LATTICE CONSTANTS $A = 9.434$, $B = 6.141$ AND $C = 9.430$, WHERE THE ANGLE BETA = 97 DEG 53 MIN FOR A MONOCLINE CELL.

THE PARAMETERS WERE OBTAINED FROM A.C.A MONOGRAPH NUMBER 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION, POLYCRYSTAL BOOK SERVICE, WASHINGTON, D. C., 1983) 2ND EDITION.

U08/14/77

TABLE I

PHENANTHRENE
23-2(14-10)---2



23-2(16-10)---1
PYRENE (BENZO(DEF)PHENANTARENE)

C16-H10

$\rho_0 = 0.7844 + \text{OR} - 0.0001 \text{ g/cc}$

$\rho_{\text{f}} = 0.776 \text{ g/cc}$

IN THE TABLE BELOW, DENSITY IS GIVEN IN G/CC, VELOCITIES IN KM/SEC AND PRESSURE IN KILOBARS.

TABLE

SAMPLE					STANDARD
ρ_{H00}	US	UP	P	V/V_0	US(ST)
1.275	3.647	0.412	19.2	0.887	5.741
1.275	3.748	0.482	23.0	0.871	5.804
1.275	3.998	0.682	34.8	0.829	5.987
1.274	4.861	1.279	79.2	0.737	6.558
1.275	5.534	1.697	119.7	0.693	6.979
1.275	5.836	1.901	141.5	0.674	7.187
1.274	6.273	2.244	179.3	0.642	7.534
1.275	6.584	2.489	208.9	0.622	7.785
1.275	6.942	2.843	251.6	0.590	8.141
1.274	7.099	3.436	310.8	0.516	8.600
1.275	7.412	3.782	357.4	0.490	9.035
1.275	7.947	4.360	441.8	0.451	9.615
1.275	8.382	4.424	472.8	0.472	9.728
1.275	8.944	4.833	551.1	0.480	10.166

$US = 3.031 + 1.457 \cdot UP \text{ KM/SEC}, \quad S10.US = 0.05 \text{ KM/SEC}$
FOR UP LESS THAN 2.423 KM/SEC

$US = 6.856 - 0.1806(UP - 2.423) + 0.4325(UP - 2.423)^2,$
 $S10.US = 0.31 \text{ KM/SEC},$
FOR UP BETWEEN 2.4 AND 5. KM/SEC

COMMENTS:

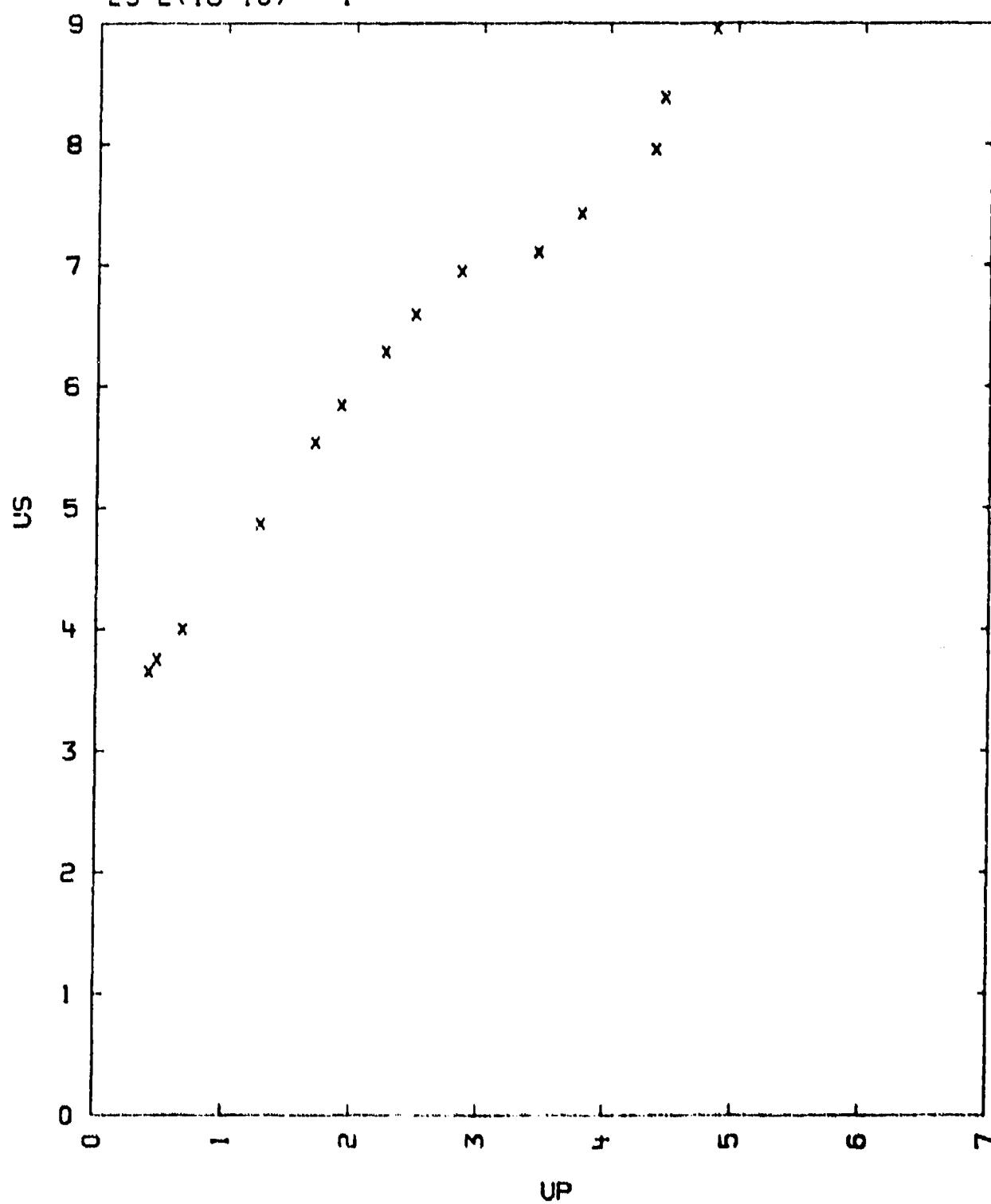
- 1) SOURCE: WARNE, R.
PRIVATE COMMUNICATION (PRELIMINARY DATA)
LOS ALAMOS SCIENTIFIC LAB., LOS ALAMOS, NEW MEXICO, USA.
- 2) EXPERIMENTAL TECHNIQUE B.
DATA REDUCTION TECHNIQUE B.
STANDARD MATERIAL 1100 ALUMINUM ALLOY: THE EQUATION FOR THE US-UP
ALUMINUM STANDARD HUGONIOT
RELATIONSHIP IS
 $US = 5.580 + 1.338 \cdot UP \text{ KM/SEC.}$
WHERE $\rho_{\text{H00}} = 2.712 \text{ g/cc.}$
- 3) ρ_{f} WAS CALCULATED USING THE LATTICE CONSTANTS $A = 1.363 + \text{OR} - 0.005$,
 $B = 9.26 + \text{OR} - 0.03$ AND $C = 9.39 + \text{OR} - 0.10$ ANGSTROMS, WHERE THE ANGLE
BETA = 100.2 DEG. FOR A MONOCLINIC CELL.

THE PARAMETERS WERE OBTAINED FROM A.C.A. MONOGRAPH 5 (AMERICAN CRYSTALLOGRAPHIC ASSOCIATION, POLYCRYSTAL BOOK SERVICE, WASHINGTON D.C., 1963) 2ND. EDITION.

TABLE I

PYRENE (BENZO(DEF)PHENANTARENE)

23-2(16-10)---I



EDIT TEST

BOX V72 PLTR

TV80LIB DD80 OUTPUT..... 12:46:34U 06/14

49 FRAMES PLOTTED

UNCL

BOX V72 PLTR

15:48:48 06/14/77U

XEROX+FILM

EDIT TEST

BOX V72 PLTR

TV80LIB DD80 OUTPUT..... 13:16:19U 06/14

EDIT TEST

BOX V72 PLTR

TV80LIB DD80 OUTPUT..... 13:16:19U 06/1

UNCL

BOX V72 PLTR

15:46:52 06/14/77U

XEROX+FILM

EDIT TEST

BOX V72 PLTR

TV80LIB DD80 OUTPUT..... 12:35:47U 06/14

EDIT TEST

BOX V72 PLTR

TV80LIB DD80 OUTPUT..... 12:35:47U 06/14